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NOVEMBER/DECEMBER 1996

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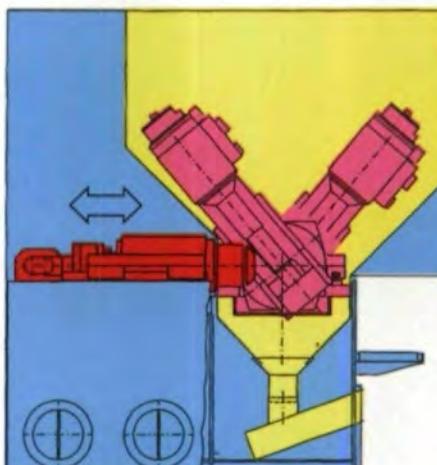
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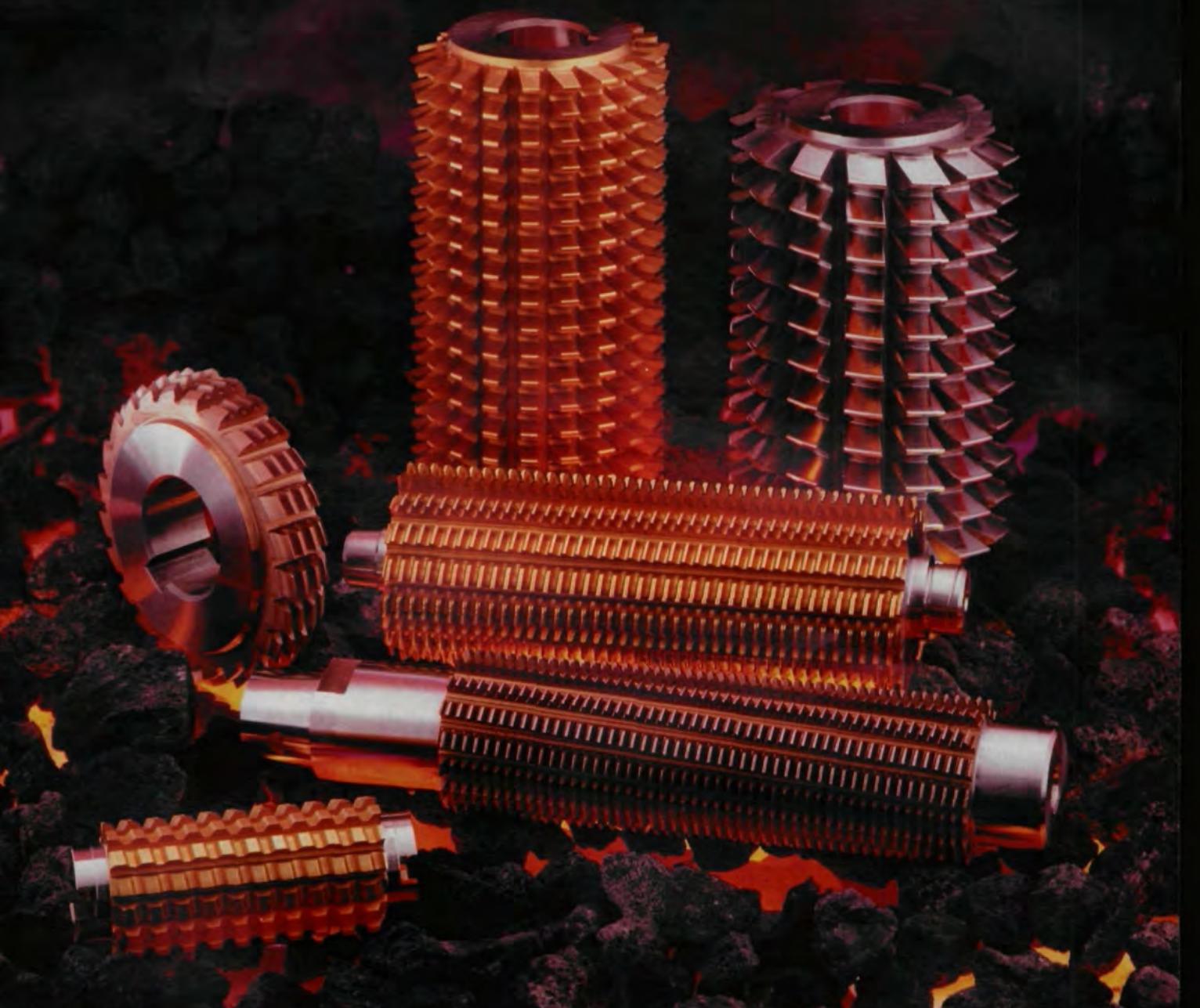
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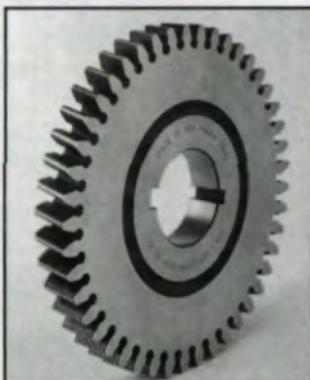
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NOVEMBER/DECEMBER 1996

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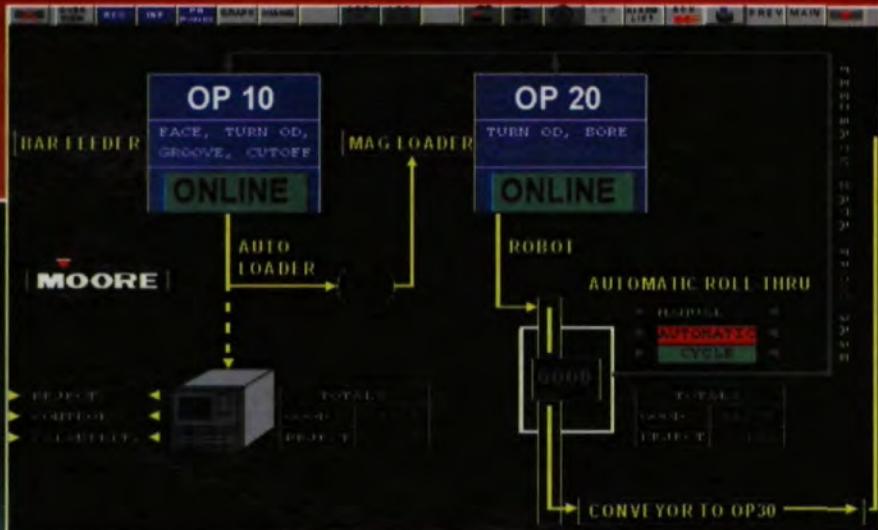
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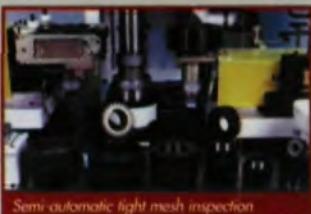
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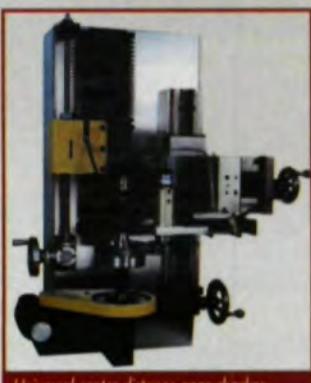
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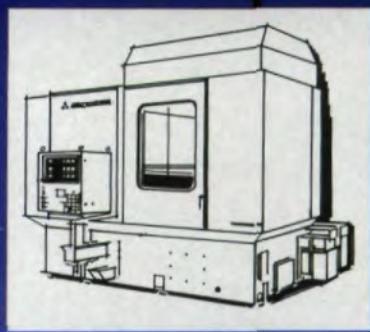
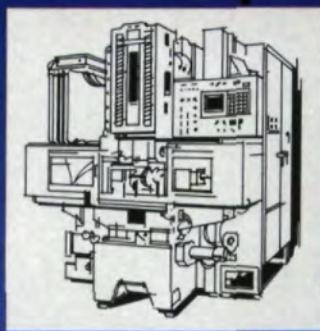
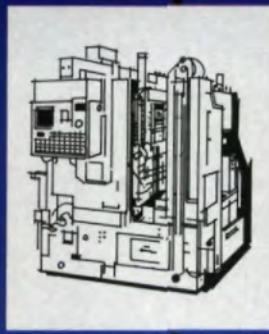
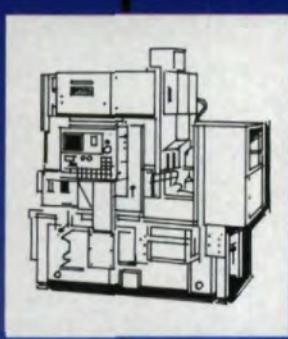
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Just back from IMTS and once again, I'm struck by the enormous vitality and strength of the manufacturing sector of the U.S. economy. It has made a phoenix-like rise from the grave dug for it by pundits in the '80s and has come back more robust and competitive than ever.

True, it's not our father's factory floor on display at the show, but in most ways it's a lot better than he ever dreamed it could be. It's a lot cleaner and there's a heightened awareness of safety and health issues. Production is faster, more organized and at the same time more flexible. The new applications and processes would amaze Dad (they amaze me). The companies have a real global reach now, and the faces to be seen are from every corner of the planet. Doesn't look much like a dying sector of the economy to me.

IMTS itself gets bigger and better every two years. It now takes up all three buildings at McCormick Place, and "doing" the entire show requires the training and stamina of a triathlete. To counter the inevitable information overload caused by a show this size, the addition of "pavilions," including the one for gear machinery, are especially welcome. It was a real treat to have most major industry players all conveniently located in the North Building, where valuable

time could be spent looking at machinery and talking to the experts rather than walking through miles of other booths.

The "hot" news at the Gear Generating Pavilion was the agreement in principal between Gleason and Pfauter (see our story on p. 16). The details of this agreement have yet to be worked out, but this is a story to watch over the next few months.

Industry trends continue much the same as they were at Gear Expo last November: Dry hobbing, faster speeds and feeds, more flexible manufacturing, and the growing presence of Windows-based software for all kinds of gear applications. The other good news is the reappearance of cheerful, smiling faces among the sales staffs. Business is very good for almost everyone, a welcome change from a few years ago, when popular wisdom had our industry on life support.

Meanwhile, back at the office . . . Our own newest ventures, The Gear Industry Home Page™, our electronic buyers guide for gear machinery, tooling and accessories, and *Gear Technology* online, are both off to a strong start. We have had over 3000 "hits," or page requests, originating everywhere from Malta to Malaysia in both August and September. Reports from advertisers on The Gear Industry Home Page™ are also positive.



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We've now introduced our direct response forms, which allow Internet explorers to request information online. Advertisers get specific information, such as names, addresses and job titles, about inquirers, much as they would from people who fill out "bingo card" forms in print magazines.

Like everyone else on the Internet, we're learning to use this new medium as we go along. Some important facts we've discovered so far are these.

1. While the Internet doesn't make for a "paperless" office, it can radically reduce the amount of paper (and the

expense of printing) you incur to reach your customers. The print bill alone for even a simple one- or two-page brochure can run to thousands of dollars even before you mail it. The same information disseminated on the Internet costs the amount of time it takes to generate the copy and get it up on line. And you have no mailing costs at all.

2. The Internet is an infinitely flexible medium for spreading the word about your company. Changes to your information can be made in a matter of minutes, at little or no additional cost. You never have to store the extra copies of anything or throw away

hundreds of out-of-date (and expensive) versions of your literature.

3. The Internet can put you in touch with people you never dreamed would be interested in your product, ones you wouldn't necessarily find by renting a mailing list. The very public nature of this medium means that people from everywhere can check out your site with the ease of a few mouse clicks. True, you may attract some "tire kickers" this way, but you also can establish contacts with potential customers you never knew were there.

4. The people who use the Internet most right now are what marketers call "early adapters." They like new technology, and they're eager to use it. This attitude doesn't just apply to the Internet. They're just as interested in your newest products and services. They're the kind of potential buyers you want to attract.

As late as this summer, I was an Internet skeptic and let my staff talk me into this venture with some reluctance. Now that I've seen how the Internet works and the power it has to convey information about products and services quickly and inexpensively anywhere in the world, I've become a convert. The success of our own Internet ventures has convinced me that as time goes on, more and more of our business will be conducted in cyberspace. People and companies who establish their presence early and who learn how to market their companies and products on the Net will have an advantage over the competition.

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Standard Issues

Like making law and sausages, standards development is an important, but messy process.

Nancy Bartels

Standards are not unlike gears themselves: mundane, but complex, ubiquitous and absolutely vital. Standards are a *lingua franca*, providing a common language with reference points for evaluating product reliability and performance for manufacturers and users. The standards development process provides a scientific forum for discussion of product design, materials and applications, which can lead to product improvement. Standards can also be a powerful marketing tool for either penetrating

new markets or protecting established ones.

No wonder then that their development and publication is an important part of the work of major technical societies, including AGMA. AGMA's input into gear standards development here and overseas causes ripples that reach all the way to the floors of the tiniest gear shops.

Because of the globalization of manufacturing, interest in developing common international standards has grown. AGMA plays an important role in this development. In addition to developing

national standards, it serves as the secretariat for work on international gear standards. Working through ANSI, the American National Standards Institute, it is responsible for processing documents as they are developed. It also oversees and arranges the various committee meetings, organizes ballots, supervises editing, handles logistics, distributes reports of meetings, etc.

Fig. 1 shows the relationship of the various national standards bodies. In reality, the process of developing common standards is not nearly so tidy. Different company and national interests, various interpretations and understandings about what is important, differing personalities and agendas on the part of the delegates, all have to be factored into the equation.

An Ever-Receding Horizon

In truth, developing all universal gear standards may not be possible, at least in the foreseeable future. For example, until U.S. gear buyers accept metric units, if they ever do, two sets of measurements will be used.

AGMA continues to develop its own standards for use in the U.S. Its goal is to harmonize its standards with those of ISO, but at the same time, parallel development continues. At present, AGMA has standards regarding some issues that ISO does not cover. ISO's 18 standards

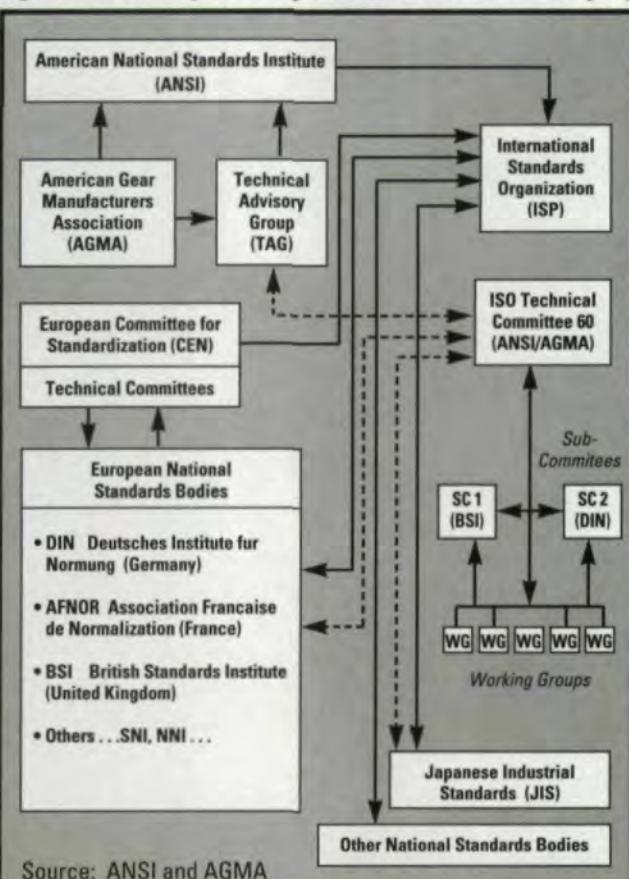
cover rating nomenclature, tooling and geometry, while AGMA's 58 standards also cover materials, enclosed drives, lubrication and other issues.

At the same time, AGMA closely evaluates ISO gear standards development and decides whether to incorporate its work into AGMA standards. It also sends delegates to ISO standards meetings to ensure that the U.S. has input into ISO standards development.

According to AGMA Technical Director, Bill Bradley, the goal of AGMA and ISO is to have good international standards that everyone can use. The approach to this goal is an incremental one. Standard by standard and meeting by meeting, AGMA and the other national standards-making organizations are working to bring their various standards closer and closer together.

Consensus by Compromise

According to Bradley, some of the issues that make international standards development an exercise in the fine art of compromise are the varying formulas used for determining gear performance and design, differences in understanding what these formulas mean and how they are to be implemented, differing national and company interests and different cultural expectations.



Source: ANSI and AGMA

CURRENT AGMA STANDARDS PROJECTS

STANDARD/INFO SHEET	AGMA COMMITTEE	DOCUMENT NAME
903-AXX	7c	Scoring Design Guide—Aerospace Gears
912-AXX	3a	Mechanisms of Gear Tooth Failures
913-AXX	3a	Profile Shift (Addendum Modification)
916-DXX	3b	Fine-Pitch, On-Center Face Gears
917-BXX	3b	Design Manual; Parallel Shaft Fine-Pitch Gearing
920-AXX	3c	Plastic Gearing Materials
921-AXX	7g	Guide for Wind Turbine Drives
922-CXX	6e	Load Classification & Service Factors; Flex Couplings
923-AXX	5c	Gear Material Grade Specifications
924-AXX	5c	Metallurgical Practice for Ind. Carburized Gearing
925-AXX	5a	Lubrication Effects on Distress (Scuffing, etc.)
926-BXX	7c	Procedure for Carburized Aerospace Gears
927-AXX	5a	Gear Tooth Load Distribution Calculations
928-AXX	4b	Inspection Data Electronic Interchange Protocol
929-AXX	5b	Calculation for Bevel Gear Topland Tooth . . .
930-AXX	3d	Load Capacity of Powder Metal Gears
931-AXX	4c	Calibration Alignment
1002-BXX	4a	Gear Cutting Tools, Fine- and Coarse-Pitch Hobs
1006-AXX	3c	Tooth Proportions for Plastic Gears
1106-AXX	3c	Metric Tooth Proportions for Plastic Gears
2003-BXX	5b	Rating Pitting Resistance & Bending Strength, Bevels
2009-AXX	4b	Classification & Inspection of Bevel Gears
2011-AXX	6a1	Wormgear Tolerance & Inspection Methods
2113-AXX	4c	Measuring Machine Calibration—Alignment
6001-DXX	5e	Design of Components of Enclosed Drives
6007-AXX	3c	Test Methods for Plastic Gears
6008-AXX	3d	Powder Metallurgy Gears
6009-AXX	6c	Gearmotor, Shaft Mount & Screw Conveyor Drives
6010-FXX	6b	Spur, Helical, Herringbone & Bevel Enclosed Drives
6011-HXX	7b	Specification for High-Speed Helical Gear Units
6025-DXX	4d	Vibration Enclosed Helical & Sprial Bevel Drives
6030-DXX	6a2	Design of Industrial Double-Enveloping Wormgears
6033-BXX	7a	Standard Marine Gear Units, Materials
6110-FXX	6b	Spur, Helical, Herringbone & Bevel Enclosed Drives
9001-BXX	6e	Lubrication for Flexible Couplings
9004-AXX	6e	Flexible Coupling Mass Properties
9008-BXX	6e	Dimensions for Gear Coupling Flanges
9009-DXX	6e	Nomenclature for Flexible Couplings
9102-AXX	6e	Metric Bores & Keyways for Flexible Couplings

Take the case of developing a formula for applying load to gear teeth as an example. There are a number of ways to do this. Which way should go into the standard? Should two or three ways be put in and let the user decide which to use, or should one be specified? If so, which one? Or should a new formula that incorporates the best of all of them be developed?

All of these issues—and similar ones for every standard—have to be hammered out.

One of the most obvious cultural differences that must be worked around is the reluctance of the U.S. to adopt the metric system. ISO

wants—and needs to have—standards stated in metric. But it's not enough to convert measurements from one system to the other. ISO would prefer to have standards in "hard" metric; that is, developed in metric from the ground up. Such standards for gears are easier to work with if tooling is already set up in metric increments.

On the other hand, many U.S. companies are still oriented toward working in inches and feet, and it does not seem likely that the U.S. will abandon the old pound-inch measurement system any time soon. Given that fact, AGMA standards will

have to accommodate both measurement systems for some time to come.

Another important difference that affects the way standards development shakes out is the manufacturing orientation of AGMA and other U.S. standards. "Standards development should be a market-driven process. There should be a market need for a given standard before it's developed," says Bill Bradley. "Standards are no good unless they are usable in a contract."

AGMA's standards tend to reflect the "state of the market," lagging behind the "state of the art." Typically, they rely on simple empirical equa-

tions in contrast to others, such as the DIN standards, which tend to include more complex equations based on element-by-element lab testing of ideal gears. Advocates of the DIN methods point out the advantages of a strong theoretical basis, while AGMA's supporters stress ease of use and years of successful applications over a wide range of sizes and configurations. Finding a common ground between these positions is a slow process.

A factor which is of less importance to Europeans, but which is crucial to U.S. standards, is the issue of product liability. In the U.S., standards have to be very explicit about



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GEAR STANDARDS

their applicability, the range of their application, etc. Language like "... is outside the scope of this standard," is frequently found in U.S. standards. The less litigious nature of European countries makes that language unnecessary in ISO standards.

Corporate & National Interests

AGMA has long been encouraging manufacturers to get more involved in standards development by sending delegates to standards committee meetings. "They should be involved," says Bradley, "because they're the ones who know what the markets have been asking for. They have the field experience to say what's realistic."

But this involvement can impede compromise. Obviously, individual companies have specific interests they want protected. However, as time goes on, and American manufacturers become more globally oriented, the need for compromise becomes more apparent and looking beyond narrow self-interest becomes easier.

The same is true of various national interests. The way standards are written can, intentionally or not, favor practices in one country over those of another. Overcoming this national interest in the push for a common benefit is one more element that has to be accommodated in the process.

Perhaps surprisingly, this obstacle is not as big as it might be. "There's not as much nationalism or company protectionism as you might think," says Bradley. "People on the committees tend to think more about the technical aspects of the prob-

lem. We've all learned to develop a consensus."

A Knowledge Bank

In the midst of all this jockeying for position and accommodating a variety of interests, one important function of gear standards making tends to get lost: that of providing a repository of gear knowledge. The professionals who serve on the standards committees bring a wealth of theoretical and practical experience to the table. In the process of hammering out the final form of the standards, much of this knowledge gets preserved and transmitted. If gear standards served no other function, this would be a vital one.

"The U.S. gear industry is old and is consolidating," says Bradley. "There are fewer good, experienced gear engineers, and we need all of them to work on standards in order to keep up their quality. If one waits for others to do the standards development, they will! For the U.S. to continue to be truly competitive, we must participate and take a leadership role in developing industry standards."

The 9000 Series Controversy

At present, the standards that are getting the most attention are the 9000 series of quality standards. AGMA does not have a comparable set of standards and has no official position on whether these standards should be adopted by individual companies. ISO 9000 series standards can be applied to the entire manufacturing process, but AGMA is interested only in gear standards. It does not write quality method standards.

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GEAR STANDARDS

However, these standards have caused a good deal of controversy. Many people both in the U.S. and Europe feel that the ISO 9000 standards were never intended to be vehicles for third-party certification, but rather were meant to be used internally by companies for their own evaluation purposes. The development of a lucrative third-party certification industry, the concerns of smaller companies about the high cost of qualification, and the debates about the qualifications of registrars and consultants have led some to reconsider the entire ISO 9000 certification process.

The advent of the Big Three automakers' QS-9000 program has only complicated the issue. This program is not a product of the original ISO 9000 series, but a separate set of quality standards which is now being demanded by Ford, GM and Chrysler. The pros and cons of this program and its effect on the ISO 9000 series are the subject of still more debate.

AGMA's Overall Goal

The development of common standards may seem glacially slow at times, but progress is definitely being made. At any given time, AGMA has between twenty and twenty-five active committees at work on one and sometimes two or more standards. (See the attached list of current AGMA projects.) In addition, some committees are working on information sheets, which contain material that is not included in standards, but is useful or needed to apply standards effectively.

AGMA's goal is to bring AGMA and ISO standards into harmonization as soon as the gear industry will accept a single standard, but progress is slow and tedious. It takes two to three years to revise or develop a standard, depending on how active a committee is. And committees are all made up of volunteer members.

The Best of Times; The Worst of Times

Ironically, times like these, when business is good, can be one of the worst times for standards development. Some companies are too busy to let valuable employees have time away from the office to attend standards committee meetings. On the other hand, when business is poor, companies can't afford to let employees attend. Willingness and commitment on the part of both individuals and their employers are crucial to the success of the various standards committees.

International standards development may be a bit like making law and sausages—a messy process whose result is not necessarily to everyone's liking. But it is an important one. As business becomes more and more global, the push to harmonize standards, although it may come in fits and starts, will certainly continue. ☀

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For more information about AGMA, please circle 202.

TECHNICAL CALENDAR

NORTON TOOLROOM SCHOOLROOM

The Norton Company offers this course in various cities around the country during the weeks of **Nov. 10 and 17**. The course is a one-day seminar focusing on how to select and use grinding wheels for optimum efficiency and results. It will cover grinding theory, bonded abrasive basics, wheel selection, dressing, superabrasives, mounting and truing and grinding wheel safety. Contact Norton at 508-795-5000 or fax 508-795-2688 for more information.

EDUCATION SYSTEMS WORKSHOP, INC.

Steel Mill Gearing Symposium, Sharaton Station Square Hotel, Pittsburgh, PA. Held **Nov. 13-14**, this course will cover steel mill drive systems using the gear units as reference points. The use of gear standards, optimum gear tooth modification metallurgy and drive lubrication for all types and geared drive systems for steel mills will be discussed. The course should be of particular interest to maintenance personnel, operators, engineers, metallurgists and researchers, as well as manufacturers of drive components, mill builders, service personnel and consultants. Contact ESW at 219-865-1318 for more information.

SME AUTOFACT '96

Conference and exhibition will be held **Nov. 12-14** at Cobo Center, Detroit, MI. Autofact '96 is billed as the industry's premier conference and exposition for products and processes for design engineering in manufacturing. Exhibits and seminars on a variety of subjects of interest to design and process engineers and managers, including CAD/CAM, EDM, rapid prototyping, systems and communications and factory automation. Contact SME at 800-733-4763, 313-271-1500 or fax 313-271-2861 for more information, or check the SME web site, <http://www.sme.org>.

AGMA GEAR SCHOOL

This final session of the year will be held at Richard J. Daley College, Chicago, IL from **Nov. 18-22**. The course is designed for employees with at least six months' experience in setup or machine operation, and it covers setup, gear inspection, gear calculations and basic gearing principles. Call Susan Fentress at AGMA, 703-684-0211 or fax 703-684-0242 for more information.

SPC AND METROLOGY FOR GEAR MANUFACTURING

Two-day course in SPC will be held **Jan. 21-22, 1997**, and a one-day mini-course in Understanding Gear Metrology will take place on **Jan. 23, 1997**. Both courses will be held in Indianapolis, IN, and are sponsored by SME. For more information, contact Cherrie Bacon at SME Headquarters, 313-371-1500, x 358 or e-mail: bacoche@sme.org. Information is also available on the SME web site, <http://www.sme.org>. ☀

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New Gear Developments at IMTS

The International Manufacturing Technology Show provided one of the biggest ever marketplaces for buying and selling gear-making equipment, with 121,601 attendees, making it the largest IMTS ever. The show took place September 4–11 at McCormick Place in Chicago, IL.

The gear industry made a strong presence at the show, with the introduction of the Gear Pavilion at IMTS. The new focus area allowed visitors to find most of the companies who sell gear manufacturing machinery all in one place.

Several key gear industry companies made announcements or introduced new machines that should have an impact on gear manufacturing for many years to come.

Gleason to Acquire Pfauter Group

Gleason Corporation shocked the gear industry just before the show opened by announcing that it had reached an agreement in principle to acquire all assets of the Hermann Pfauter Group, based in Ludwigsburg, Germany.

The purchase will include Pfauter's gear machinery manufacturing operations in Germany, Italy and the United States as well as the company's 76% interest in Pfauter-Maag Cutting Tools, L.P., located in Loves Park, IL. The Pfauter Group employs about 1,050 worldwide and had combined sales of \$175 million in 1995.

According to Gleason and Pfauter management, the entire deal took place over the last few weeks before IMTS and was kept under tight wraps so an announcement could be made at the show.

"Pfauter has long been recognized as a leading supplier of cylindrical gear production equipment, as Gleason has for bevel gear production equipment. The combination of our two companies will create an excellent strategic fit that will expand our product line, substantially enhance our ability to provide our customers fast and effective solutions to their gear processing needs and offer significant benefits from combining technology, production capabilities and distribution channels," said James S. Gleason, chairman and president of Gleason Corporation.

Mitsubishi Debuts 3-in-1 Gear Center

A unique machine that combines hobbing, deburring and rolling in one machining center was demonstrated for the first time at IMTS by Mitsubishi Machine Tools USA.

The GT06R is aimed directly at automotive manufacturers—it can produce one AGMA Class 10 gear every 10–15 seconds. One machine and one operator can produce gears that leave the machine ready for heat treating.

The machine has a maximum hob speed of 4,000 rpm and a maximum table speed of 750 rpm. It measures 13.2 feet by 11.5 feet. Also available is a GT06S model, which replaces the rolling function with a shaving function to finish the gears.

Fellows Introduces Direct-Driven Shaper

The new FS180 Mark III CNC Hydrostroke gear shaper features six servo-driven axes of motion for higher-speed cutting cycles. In addition, the machine is being introduced at a lower price than that of the previous model.

The manufacturer claims the machine may reduce cutting cycle times by as much as 35% with speeds up to 2,000 strokes per minute. It handles pitch diameters up to 7" and face widths up to 1 1/4", which makes it appropriate for automotive transmission applications.

Gleason Knowledge System Demonstrated



The Gleason Works introduced a new software system for its PHOENIX 125GH CNC hobbing machine. The software, installed on a personal computer, provides the machine operator with setup, startup, operational, troubleshooting and maintenance information.

The system combines the knowledge of Gleason's technical experts to include complete fault diagnostics with suggested remedies, a complete set of replacement parts drawings, animated tutorials to explain key concepts and complex procedures and training modules to help the user get accustomed to the machine interface and control panels.

Bourn & Koch Redefines Small Footprint

The Model 25H hobbing machine demonstrated by Bourn & Koch Machine Tool Company is a 4-axis CNC hobber for 1" maximum diameter and 4" maximum face width gears.

The machine is almost a desktop model, occupying a 30" x 30" space on the floor. It includes auto hob shift, double cut and crowning capabilities and can use carbide or HSS hobs.

Star Cutter Introduces Tool & Cutter Grinder

Elk Rapids Engineering, a subsidiary of Star Cutter Company, demonstrated its new UTG-300 CNC five-axis tool and cutter grinder, which includes Windows-format software for sharpening hobs, shaper cutters, broaches, end mills, taper fluted tools and Maag-style cutters.

Pfauter-Maag Introduces Shaving Cutter Line



Pfauter-Maag Cutting Tools, L.P. announced that it has begun offering a complete line of shaving cutters, including standard, underpass, plunge and diagonal-type cutters in a range of sizes and accuracy capabilities.


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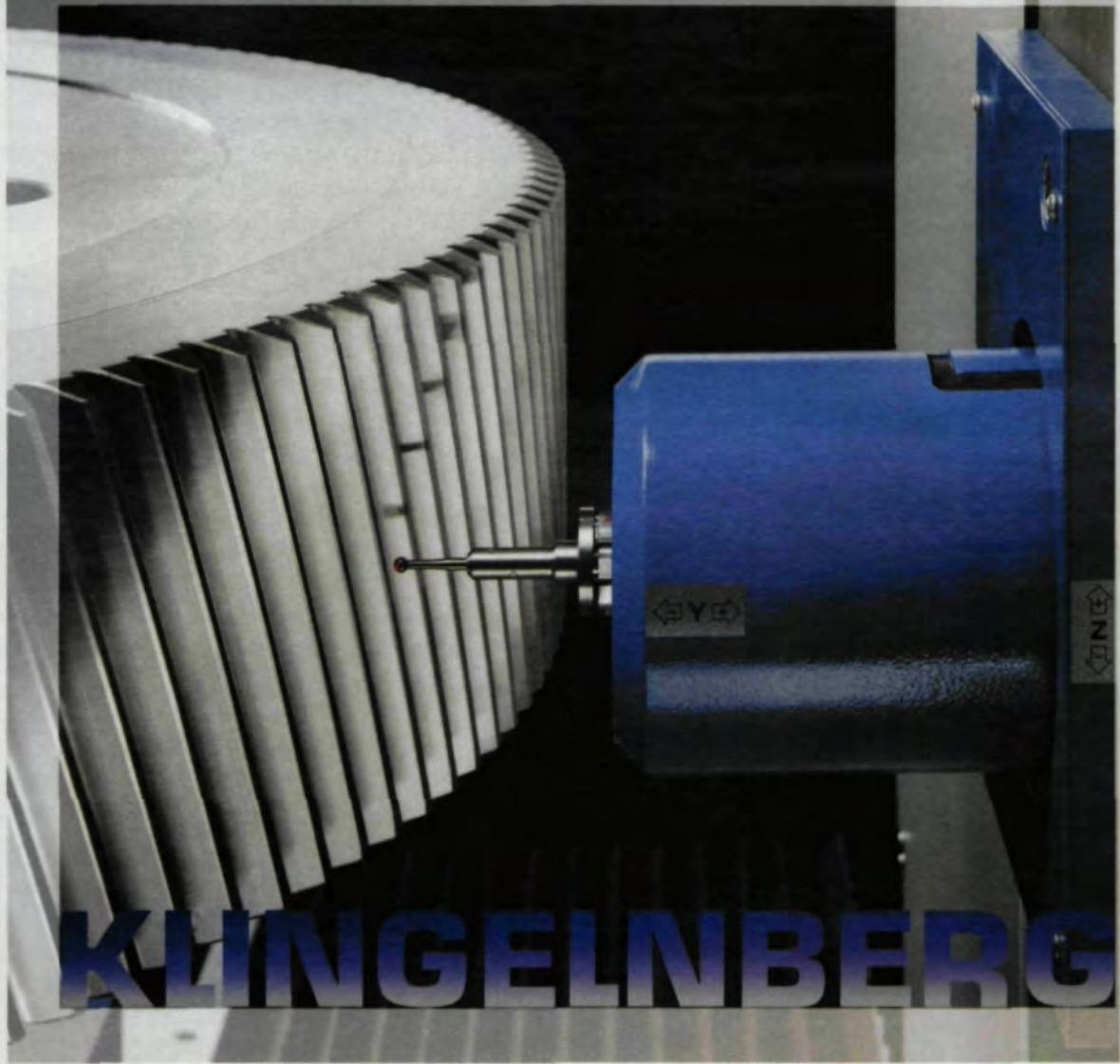
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The Advantages of Ion Nitriding Gears

This process can eliminate the need for expensive post-heat treatment operations.

Robert Lamont, Jr. & A. Bruce Craven

When it comes to setting the standard for gear making, the auto industry often sets the pace. Thus when automakers went to grinding after hardening to assure precision, so did the machine shops that specialize in gearing. But in custom manufacturing of gears in small piece counts, post-heat treat grinding can grind away profits too.

One alternative that has yet to be fully exploited by the gearing industry is ion nitriding. General Motors' Allison Division has ion nitrided 4140 steel diesel engine gears, Ford has used the process for certain models, and perhaps a dozen commercial heat treaters around the United States provide ion nitriding services to machine shops. Here—from the perspective of a custom gear shop and a heat treater—are some of the advantages that ion nitriding offers gear makers.

Advantages of Ion Nitriding

For any manufacturing operation, grinding adds not only time and labor, but also an element of risk. Grinding has become a routine part of gear making, primarily because the heat treating processes that harden load-bearing parts such as gear teeth also introduce thermal stresses that cause distortion. But unlike induction hardening, a commonly used surface hardening process in which gear teeth are hardened tooth-by-tooth or one at a time, ion nitriding introduces favorable compressive stresses.

Ion nitriding is performed in a precision-sealed vacuum furnace. After the air is evacuated (to less than 100 ppm of air), a small partial pressure of hydrogen and nitrogen gas is bled into the chamber, and the vacuum is maintained at about 5 torr (atmospheric pressure is 760 torr). Then, energizing the parts to a negative (approximately 500 volt) potential initiates an electrical plasma of gaseous ions. The positively charged ions are attracted to the part, subsequently reacting with the alloy elements of the steel part to form nitrides. The nitriding temperature is significantly lower than that of induction hardening or carburizing—specifically, 950°F. Moreover, with ion nitriding, there is no need for a liquid quench, eliminating another source of adverse stresses and distortion. Eliminating most heat treat-induced distortion is critical for any manufacturer, particularly smaller machine shops with limited equipment for secondary operations such as grinding and straightening.

Practical Applications

How do these theoretical advantages translate into everyday practice? At Atch-Mont Gear, a good customer requested a Class 10 gear with hardened teeth. A Class 10 gear is not that hard to machine, but typical practice for a 4140 gear (either annealed or pre-heat treated) would have been to induction harden the *gear teeth only* for better wear characteristics. The distortion introduced by induction hardening or carburizing lowers the class number (or precision) because of the high process temperature (in excess of 1600°F) and subsequent quench. Lacking the ability to grind all types and sizes of gears, Atch-Mont's only option for returning the gear to the required precision appeared to be sending the piece out for tooth grinding. This was cost prohibitive.

Fortunately, Atch-Mont has had some customers who requested gas nitriding with ammonia, so the company was familiar with nitriding's low-distortion benefits. Solar Atmospheres, a commercial heat treater specializing in vacuum processing, suggested the piece would be a good candidate

Table 1 — Case Depth

Steel Grade	Typical	Practical Maximum
1045	.001" – .002"	.002"
4140	.010" – .012"	.025"
4340	.008" – .010"	.015"
A-2, D-2, H-13	.008" – .012"	.015"
400 Series S/S	.004" – .006"	.010"
300 Series S/S PH S/S (17-4, 17-7, etc.)	.003" – .004"	.005"

for ion nitriding. Atch-Mont told the customer it couldn't guarantee Class 10, but could ion nitride and lap the gear teeth if necessary. The results were successful.

Ion Nitriding Worm and Pinion Shafts

Worm and pinion shafts are also good candidates for ion nitriding. Parts that are usually made from 8620 steel and carburized, or from 0.4 carbon medium alloy carbon steel and induction hardened need to be rough machined with extra material on the journals. This allows for finish machining to overcome the distortion resulting from carburizing or induction hardening. With ion nitriding, this is not a requirement.

Worm gears—typically made from 8620, 4615 or 1045 steel—have a tendency to unravel when carburized or induction hardened (because of the higher temperature process), which means they have to be ground afterwards to make them straight and true with respect to the bore (or centerline). At Atch-Mont, engineers found that by making the gears of pre-heat treated 4140 steel and ion nitriding them, nearly the same hardness could be achieved. Herringbone gears will respond with the same positive results.

At Solar Atmospheres, gears in the 10–12" diameter range are commonly ion nitrided, and gears of up to 30" in diameter can be accommodated. Gear materials most commonly ion nitrided are the medium alloys—the 4000 and 5000 series steels and, occasionally, the 6000 series steels. Stainless steel, which is very hard to gas nitride without mechanical or chemical surface treatments prior to processing, can be ion nitrided, although not as easily as the medium alloys. (The high percentage of chromium and nickel develops very hard surface nitrides that saturate the metallurgical structure quickly, making the ultimate case depths shallower than the alloy steels.)

Ion nitriding introduces minimum growth on the order of .0001—.0002" per side and requires less processing time than gas nitriding. But the real advantage for a machine shop is the reduced number of machining steps coupled with the quick turnaround, which results in faster manufacture. It can also give manufacturers more material selection choices. The resultant benefits are moderate surface hardness gains with deep case depths in medium alloy steels, high surface hardness with shallow case depths in stainless steels and high surface hardness with modest case depths in tool steels.

Masking

With ion nitriding, workpieces may have to be masked to insure that surface hardening occurs only where it is supposed to. Sometimes this is

relatively easy; i.e., gears can be stacked, permitting nitriding of the teeth with just the topmost pieces requiring a mask to cover the face and bore. But even when individual pieces have to be masked with a stop-off paint—a time-consuming but effective process—Atch-Mont Gear feels it's well worth it to "get the gear we want."

Currently, ion nitriding is used for gears up to 30" or 36" in diameter. In fact, the authors believe it is technically feasible to produce ion nitrided gears that would compete with many carburized gear applications. Most ion nitriding heat treating shops do not have the equipment capability to handle the 30" or larger gears.

One of the factors contributing to the relative scarcity of ion nitriding is the high cost of the machinery required. As interest and demand increases, however, the large capital outlay is being overshadowed by the business potential, and companies like Solar Atmospheres are looking to this area for expansion.

It is this heavy investment in equipment, as well as a lack of education as to the potential of ion nitriding, that the authors believe have kept the process from taking off in the United States as it has in Germany and other European countries. In addition, equipment problems when ion nitriding was first introduced in this country created the image of an unreliable process that has stuck in the minds of some engineers. While this is no longer a valid objection, it is true that ion nitriding furnace operators must be carefully trained, as the process is more technically challenging than gas nitriding.

These factors need not concern custom gear makers or tool and die shops, however, since there are commercial heat treaters who have expertise in developing processes even for runs of one or two parts. With ion nitriding's ability to eliminate many secondary operations and to turn jobs around relatively quickly, it's a process worthy of the machinist's consideration. ◎



Fig. 1 — A load of gears before (left) and after ion nitriding.



Fig. 2 — Parts as loaded for ion nitriding on the furnace hearth plate.

Robert Lamont, Jr.

is the former president of and a consultant for Atch-Mont Gear Inc. of Ivyland, PA.

A. Bruce Craven

is Vice President, Engineering, of Solar Atmospheres, Inc., Souderton, PA, a commercial vacuum heat treating company.

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If you found this article of interest and/or useful, please circle 203.

For more information about Atch-Mont Gear Inc., circle 204.

For more information about Solar Atmospheres, Inc., circle 205.

Dry Hobbing Saves Automaker Money, Improves Gear Quality

Dry hobbing delivers a breakthrough in productivity, economy, cycle times, tool life and part quality.

David Arnesen

It takes confidence to be the first to invest in new manufacturing technology. But the payback can be significant. That has been the experience at the Ford Motor Company's Transmission & Chassis Division plant at Indianapolis, IN, which boasts the world's first production application of dry hobbing.

Beginning in July 1994, Ford began installing Liebherr LC 82 CNC hobbing machines to hob steering pinions (SAE

1045, 22 Rc). According to Ford manufacturing engineers, dry hobbing with carbide cutters has reduced machining costs by 44%, shortened cycle time by 48% and increased tool life by a factor of 6. So far.

Goal No. 1: Improve Pinion Quality

The task at Ford's Indianapolis plant was to improve gear quality—surface finish and pitch diameter runout—and meet increased production demands. After determining that existing hobbing

machines using standard coated HSS hobs with coolant were incapable of meeting the plant's targets, the engineers investigated new technology.

After extensive research and subsequent testing at Ford, carbide hobbing without coolant showed the most promise in meeting quality goals and offered the additional potential of greatly extended tool life and lower maintenance costs. During test cutting of the steel pinions, the process demonstrated a Cpk of 3.0, and tool life was far longer than was achieved with any steel hob. The process testing was completed using carbide hobs on a Liebherr CNC hobbing machine specifically designed for carbide dry hobbing.

More Speed, Greater Horsepower

To properly utilize the advantages of carbide, a hobbing machine must be capable of increased speeds and greater horsepower than is typical of conventional machines. The Liebherr machine table can achieve speeds up to 450 rpm; the hob head is equipped with a heavy duty drive that permits speeds up to 3,000 rpm with drive power to 18 kW (25 hp), several times that of the conventional hobbing machines at Ford.

The combination of carbide hobs with maximum diameter of 90 mm (3.6") and the new machines, which have cutter spindle speeds of 2,000 rpm, enabled hobbing at 850 sfpm, much greater than the capability of conventional production machines.

The higher cutting speed reduced machining times to approximately 22 seconds from 42 seconds previously with HSS. A workpiece load/unload mechanism built into the hobber and closely coordinated with workpiece



Courtesy of Liebherr-America

View of the pinion, hob and tailstock in the Liebherr LC 82. The workpiece load/unload mechanism built into the hobber, closely coordinated with workpiece clamping, reduced Ford's chip-to-chip time to about 4 seconds.

clamping reduced Ford's chip-to-chip time to about 4 seconds.

Because the pinions are held rigidly in place during machining by hydraulic gateways driven by cams, part movement or deflection is prevented, and the potential for runout, feed scalloping and chatter marks is reduced. The result is that surface finish improved to between .5 and .75 Ra from 1.1 to 1.5 Ra.

In the first year of production, Ford Indianapolis immediately achieved significant gains in tool life, more than offsetting the higher initial cost for carbide cutters. Because heat is the main factor affecting tool life, the engineers made several further changes to allow the cutter to run even cooler. These included different coatings, recently developed carbide materials and hob geometry.

To reduce heat build-up at the edge of the cutter and increase the shearing action, the rake angle was increased to 5°. The number of gashes was reduced to 12 from 15, allowing more room for chip evacuation.

Documented Benefits

Data from the Ford experience clearly points to the benefits of dry hobbing. According to Ford manufacturing engineers, tool life improved to 252,000 pinions per hob (14 regrinds) using dry carbide from 39,000 pinions per HSS hob (12 regrinds) on existing wet cutting machines. Machining cost fell by 44%. In addition, Ford found that the process is very stable, maintaining exceptional consistency well within the process capability specifications.

Increasing the cutting edge rake angle and changing the coating to TiAlN is now being tested, and Ford is now achieving up to 33,000 pinions per

regrind, with the potential of getting nearly 300,000 pinions per cutter.

The primary goal was to improve quality and production economy, but the plant also achieved a Ford 2000 environmental goal by eliminating the use of cutting oils and coolants. Operators like the rapid, coolant-free cycling. It's environmentally safer and cleaner with no cutting oils and mist.

A search for a better quality pinion at Ford Motor Company yielded a process

that not only produced a better surface finish, but reduced piece cost and cycle time. It also provided the additional advantage of coolant-free operation, saving costs and improving operator morale. ☀

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Dry hobbing produces Ford steering pinions in 48% less time, at 44% less cost and improved gear quality.

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BEVEL GEARS

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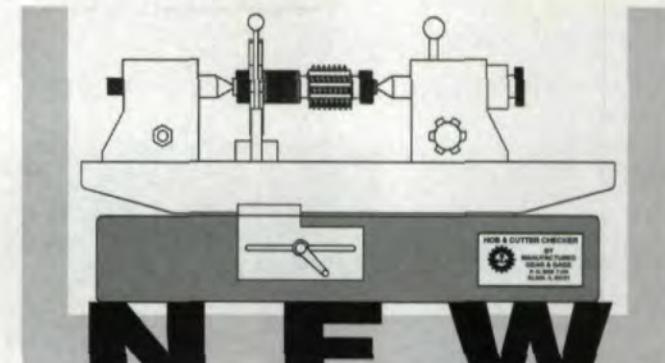
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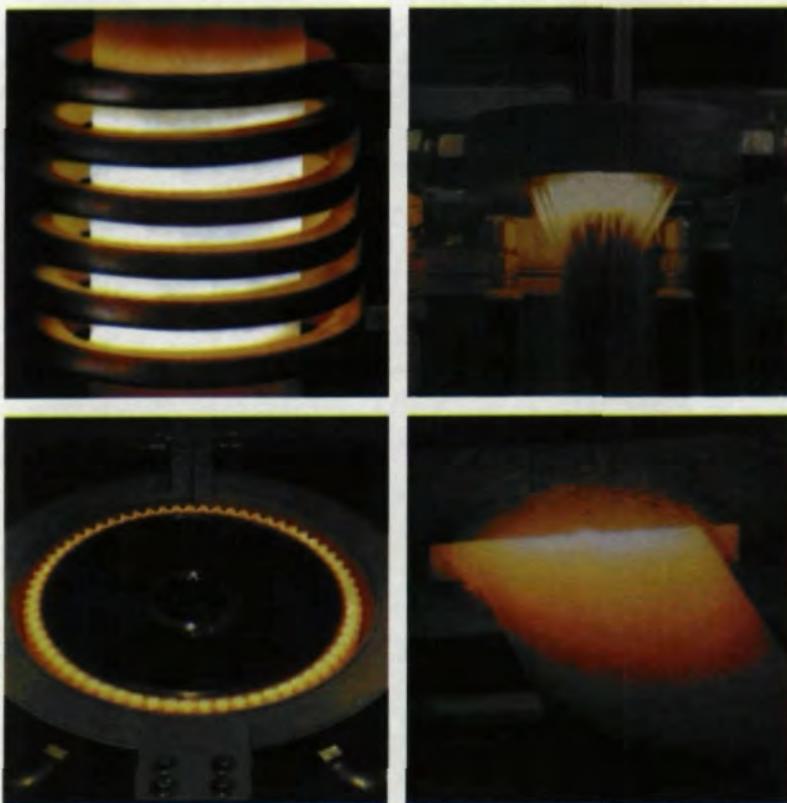
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Chamfering and Deburring External Parallel Axis Gears

Basavaraj Nyamagoudar

The chamfering and deburring operations on gear teeth have become more important as the automation of gear manufacturing lines in the automotive industry have steadily increased. Quieter gears require more accurate chamfers. This operation also translates into significant cost savings by avoiding costly rework operations. This article discusses the different types of chamfers on gear teeth and outlines manufacturing methods and guidelines to determine chamfer sizes and angles for the product and process engineer.

Why Chamfers?

Chamfers are needed in gears:

- To prevent nick and bump damage along the active tooth surface after the shaving or finishing operation;
- To prevent burrs and sharp edges which cause gear noise;
- To prevent the break-off of burrs and sharp edges during torque transfer when the gears have been assembled in boxes or transfer cases;
- For cosmetic reasons.

In the last few years, gear manufacturers have intensified their efforts to prevent or reduce nick and bump damage. Handling systems have ratchet conveyors, which prevent the gears from touching each other. Special baskets are used to protect the gears from accidental damage during heat treatment process. Operator training has stressed the careful handling of gears at every stage of production. In spite of all these steps, the problem still persists. The number of gears rejected because of nicks can range from 10–60% of a batch. Nicks modify lead or involute characteristics, causing meshing defects.

Chamfers significantly reduce noise while the gears mesh and effectively protect all vulnerable zones in the gear tooth.

Types of Chamfers

Four chamfers are shown in Fig. 1. Chamfer A is the tip chamfer along the lead produced by the

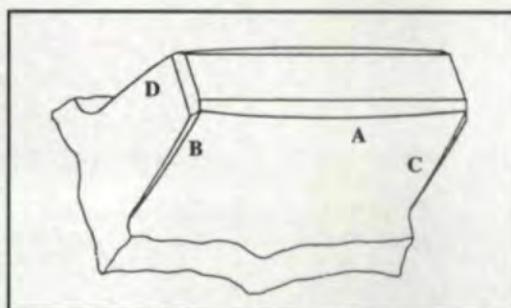


Fig. 1 — Types of chamfers on gear teeth.

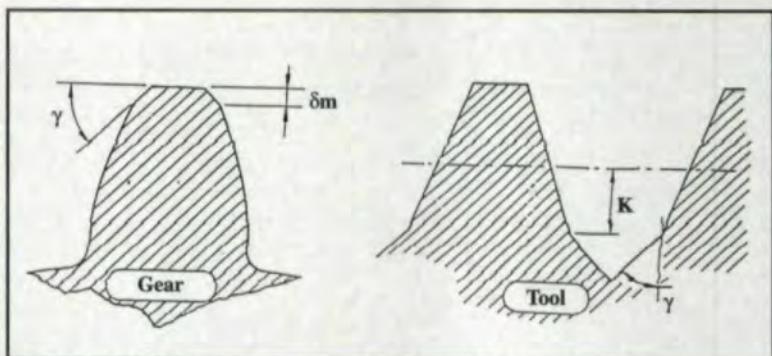


Fig. 2 — A) End of chamfer along lead; B) Basic rack of preshave tool.

preshape tool. B is the acute edge chamfer in cylindrical helical gears. C is the obtuse edge chamfer in cylindrical helical gears produced by cutting, grinding or rolling operations. D is the tip chamfer on end faces produced during the turning of blanks.

The tip chamfer along the lead is generally executed while cutting the gear with either a hob or a shaper cutter which has a modified tooth profile called semi-topping. The size of the chamfer depends on the gear's diametral pitch (the module). Generally it is

$$\delta_m = 0.10\text{--}0.15 \text{ mm}$$

$$\gamma = 30\text{--}40^\circ$$

See Fig. 2 for details.

It is difficult to maintain the size of the tip chamfer, since it is related to the tolerances of the outside diameters and gear tooth thickness. For example, gears with normal diametral pitches up

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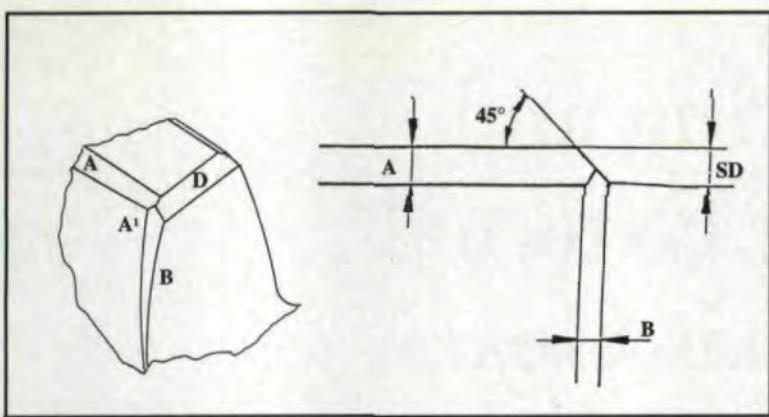


Fig. 3 — Gear tooth with edge chamfer and both tip chamfers.

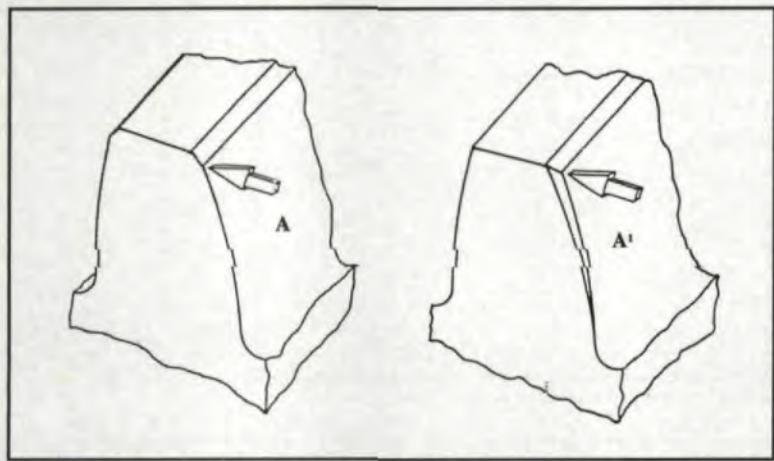


Fig. 4 — Gear tooth with tip chamfer and tip chamfer along lead and edge chamfer.

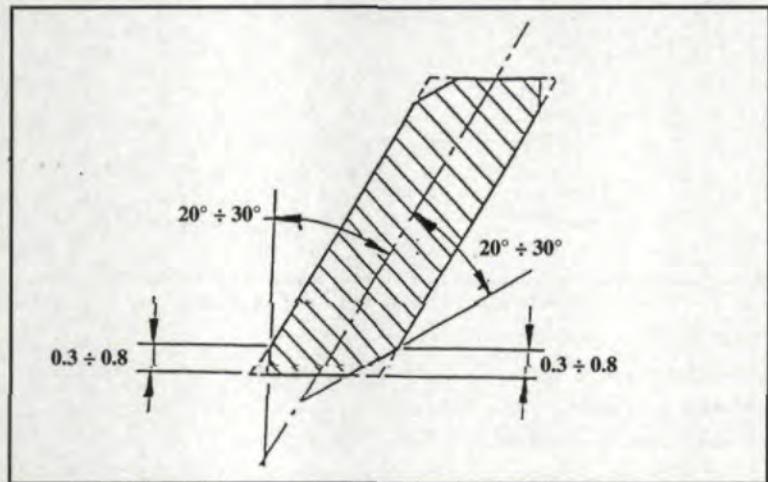


Fig. 5 — Chamfer angles must be set with exposed points as far away from the ends of the tooth as possible.

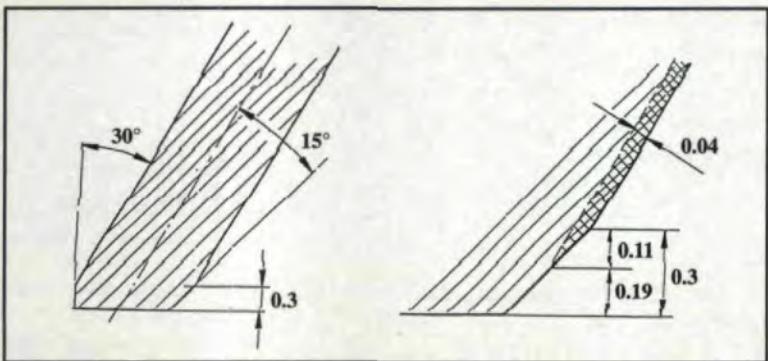


Fig. 6 — Shaving reduces the size of the chamfer to some extent.

to 8–10 (module 2.5–3.0) have an O.D. tolerance of roughly 0.008" (0.2 mm) and a variation of 0.004" per side (0.1 mm/side). The cutting tolerance on tooth thickness may be $\pm 0.0008"$ (0.02 mm), which affects the cutting tool position. The chamfer will have the following variation:

$$\delta_m = \frac{(0.0008)}{\tan \alpha_n}$$

where α_n = normal pressure angle

When $\alpha_n = 14^{\circ}30'$, $\Delta\delta_m = 0.003"$ (0.077 mm).

When $\alpha_n = 20^{\circ}$, $\Delta\delta_m = 0.002"$ (0.055 mm).

This variation is close to 50% of the nominal value of the chamfer size. This becomes much more significant when we are dealing with gears with a normal diametral pitch (NDP) of more than 20 (or module less than 1.25). The tolerances of the O.D. and the tooth thickness exceed the chamfer's nominal value. It then becomes necessary to cut the gears with "topping" tools, which simultaneously cut the teeth and the O.D.

Sometimes when it is necessary to use as much active profile as possible because tip chamfers reduce the working diameter and the line of action, gear designs do not allow tip chamfers. In some rare instances, only a few tenths of a millimeter make up the meshing continuity. Such constraints must be resolved during the early stage of a transmission design, and the designer must make accommodations for tip chamfer.

The chamfer "D" on end faces is required for assembly purposes and for smoother meshing. The chamfer "D," which is put on the gear during turning, can actually cause more nicks than it prevents. Usually the project engineer requires an end tip chamfer without paying too much attention to its size. From Fig. 3, it can be seen that as chamfer "D" is increased, chamfers "A" and "B" provide less protection. Therefore, it should be made as small as possible and never larger than the value

$$S_d = 0.5(a + b)$$

Another reason favoring reduction of the end tip chamfer to a minimum is the presence of hobbing and shaping burrs in this area. These burrs are not removed by the usual deburring tools and may be difficult to remove if they are large. Smaller burrs usually disappear during heat treatment or shot peening. If the chamfer "D" is large and has a heavy burr, sometimes it is necessary to employ an additional deburring tool.

From Fig. 4, it is clear that in the absence of an edge chamfer, point A is more exposed to nicking. With an edge chamfer, the most exposed point, A', is shifted towards the inside and is therefore less prone to nicks. The tip chamfer is rendered

useless unless there is an edge chamfer. Edge chamfer dimensions do not have the constraints of tip chamfers, since they are made after the gear teeth are cut. Their dimensions are to some extent independent of gear tooth tolerances. Chamfer sizes range from 0.012" (0.3 mm) to 0.030" (0.8 mm). The angles need to be set so that the exposed points are as far away from the ends of the tooth as possible (see Fig. 5). As the helix angle increases, the chamfer angle (related to the tooth axis) decreases to less than 20°. For example, a 30° helix angle will lead to a 15° chamfer angle. There is some reduction in the chamfer size while shaving (Fig. 6). During this process, 0.0015" (0.04 mm) of stock is removed from each flank. If the original chamfer size was 0.012" (0.3 mm), the chamfer size after shaving would be

$$\delta_m = 0.3 - \frac{(0.04)\sin 45^\circ}{\sin 15^\circ} = 0.19 \text{ mm or } 0.0075"$$

Therefore, it is necessary to start with a larger size chamfer, maybe 0.024–0.030" (0.6–0.8 mm). The chamfer should be made without finishing with a step. Sometimes it is better to chamfer the root fillet even if this area is not susceptible to nicking. Fig. 7 shows the correct procedure for chamfering.

Production Methods

Edge chamfers can be produced by three different methods.

A cutting operation. There are two cutting methods. The machine may be designed to have a milling cutter and a gear train of CNC equipment to generate an involute. The milling cutter can be held steady with only one circular speed along its axis. In this case, the chamfer is uniform and parallel to the involute. This method produces a good chamfer, and there is no need for any additional deburring operations. On the other hand, milling is a costly operation, and it is difficult to chamfer gears lying adjacent to a shoulder using this technique. Cycle times are long in this method because of indexing, and tool life is poor.

A second way to cut a chamfer is to use a gear train or CNC equipment to index in conjunction with a cutter. The cutter has a reciprocating motion timed with the indexing motion. This type of operation usually produces the chamfer along a straight line. The advantage of this method is that no further deburring operation is required. Among the disadvantages is the fact that this method creates an uneven chamfer extending through the whole root. Sometimes burrs are left on the gear in the root area. Chamfering gears adjacent to a shoulder is also difficult with this method. Again, cycle times are long, and tool life is poor. This

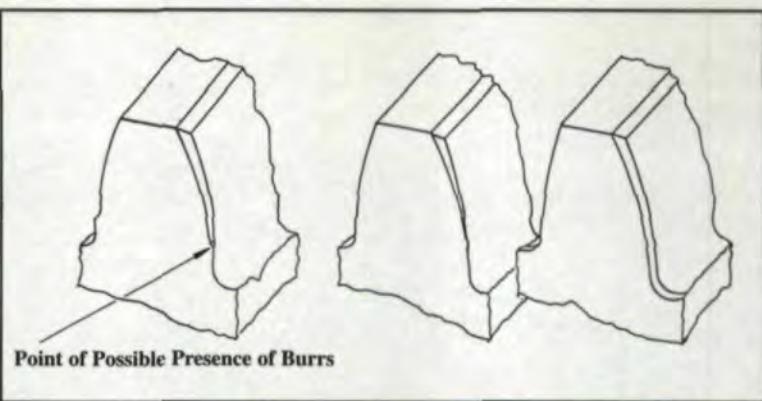


Fig. 7 — Correct chamfering procedure.

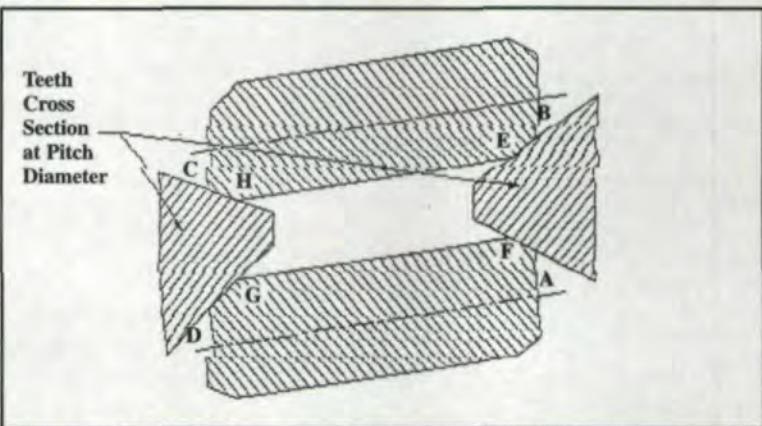


Fig. 8 — A cross section of gear and chamfering tool teeth in a rolling operation.

approach also requires a lot of operator assistance to maintain a good setup.

A grinding operation. In this method, a grinding wheel is used to produce the chamfers. The advantages are low cycle times and acceptable chamfers all around, but the grinding powder mixed with steel particles pollutes the atmosphere, creating Clean Air Act compliance problems and raising concerns about employee health and general environmental ethics. To counter the pollution effects, expensive filters and dust collectors are needed. Tiny burrs are created along the involute, and they need an extra cleaning operation like shot peen blast. A lot of operator assistance is required to maintain a good setup.

A rolling operation using special chamfer tools. This operation involves driving a chamfer tool in mesh with the gear under pressure. The pressure will plastically deform the material, producing the chamfer. Most of the material deformed plastically will flow out of the sides A, B, C and D (see Fig. 8). Tiny portions, about 0.0008" (0.02 mm), will rise up as tiny ridges inside the involutes E, F, G and H, and a very small portion will rise out of the tip chamfer (D) (Fig. 1) produced by a turning operation. Because of this, the operation must be followed by a finishing operation like shaving or grinding. It is not recommended for finished cut parts.

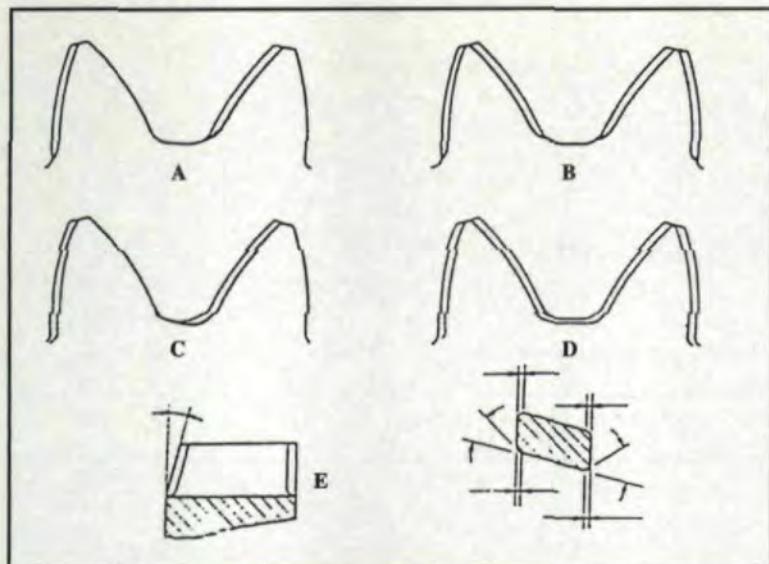


Fig. 9 — Types of edge chamfers.

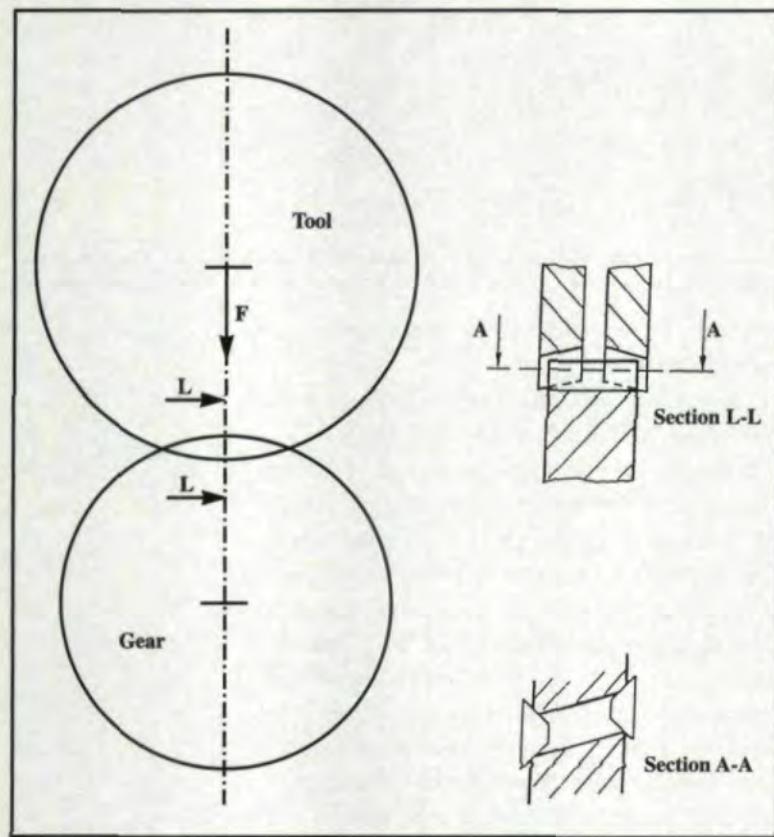


Fig. 10 — Schematic diagram of chamfer tool in mesh with gear.

The material raised along the surfaces A, B, C and D and the burrs produced during the cutting of the teeth are removed by a spring-loaded deburr tool. The chamfer and deburr operations must be carried out simultaneously to avoid pushing the burrs into the gear teeth after cutting. The chamfer tool will force the burrs out for a cleaner cut by the deburr tool. The material raised along the surface D can be minimized by designing the chamfer tool with an operating pressure angle that minimizes the sliding velocity toward the tip. A pair of burnishing tools can be added to the deburr tool group to remove the raised material along D.

The main advantage of this method is extremely long cutter life. It is quite common to chamfer more than 100,000 parts between resharpening. The machine cut cycle time is only 3–4 seconds, while the floor-to-floor cycle time varies from 7–15 seconds for pinion gears. Constant sizes of chamfer parallel to the involute and chamfering the root are possible. This method can chamfer/deburr any adjacent shoulder both on the gear side and the groove side.

Some stress points should be considered when producing edge chamfers by rolling. The plastic deformations of the material should produce residual stresses along the involute surface chamfer that would locally increase the surface stress limit and reduce the stress concentration factor, thus enhancing the overall resistance of the chamfered gear. It is essential to chamfer not only the acute angle called for on most drawings, but also the obtuse angle. This gives better protection from nicks and bumps and ensures homogeneous behavior of both the flanks of the gear under load because of the residual stress.

For simplest applications, the tool used on chamfering and deburring machines consists of a set of chamfering tools and a set of skiving tools to deburr lateral surfaces. Because of the force between the tool's springs and the gear's width once it enters into the tools, the two deburring tools will spread open. Chamfering and deburring tools run free on their own quills and self-center themselves on the center line of the gear, thus assuring symmetrical chamfers and complete removal of burrs.

The tool group on a one-head machine in the simplest form consists of one set of chamfer bevel gears and one set of cutter discs mounted together as a gang. The workpiece drives the complete tool group, since it is in mesh with the chamfering tool.

The various types of chamfers that can be achieved on either spur or helical gears cover the whole range usually required for any cylindrical gears. Examples of feasible chamfers include a) chamfering only on one flank without the root; b) chamfering both flanks without the root; c) chamfering one flank and part of the root; d) chamfering the complete profile; e) chamfering inclined faces (see Fig. 9).

Each problem can be evaluated individually and tooling engineered to suit specific applications. Cluster gears can be chamfered and deburred with machines having multiheads with two working stations. To work different gears on the same machine, the tools can be designed to keep a constant center distance between the workpiece and the tool in order to reduce the changeover time.

Chamfering Tools

Chamfering tools are engineered to generate the chamfer on the edges of the gear teeth. The chamfer is made by the rolling action of chamfering tools. In effect two bevel gears mate with the work gear only along the corner edges of its teeth. The force "F," provided by a pneumatic cylinder, represents the thrust necessary for rolling (see Fig. 10). Because of their bevel gear shape and balanced application (one pair of identical tools symmetrically coupled), opposed axial stresses are generated during rolling. As the tool group is free to move axially, it centers itself on the centerline of the gear width.

If the two tools are off center as in Fig. 11A, after the tool group is engaged, the gear will move axially until the forces are balanced. The final position is shown in Fig. 11B. This makes the chamfers symmetrical. These tools will work either spur or helical gears.

Fig. 12 describes a chamfering tool tooth. Besides being tapered, the teeth have an involute form enabling them to mesh with the gear and roll on its corners.

The angle of the tooth flanks of the chamfering tool depends on the gear helix angle and the angle of chamfers to be generated (Fig. 13).

β_1 and β_2 = chamfer angle required by part print drawing.

β = gear helix angle.

γ_1 and γ_2 = flank angle on the chamfering tool teeth.

$\gamma_1 = \beta + \beta_1$, and $\gamma_2 = \beta_2 - \beta$.

In order to have the chamfers correctly executed, the chamfering discs must be in such a position that the axes of the chamfer tools have the same helix angle as the gear (phasing along helix angle).

Special Cases

When a shoulder or radius is present on the side face of the gear, the chamfering operation cannot be completed all along the profile. The chamfer must end at least 0.012" (0.3 mm) before a step or a radius begins. In cases where the gear has an angled side face, it is necessary to engineer tools with properly modified pressure angles.

Chamfer Tool Resharpening

The chamfering tools are able to produce many thousands of pieces before resharpening. The chamfering tool teeth are not truly resharpened. Rather, the position of the chamfering disc is changed with respect to the gear so that afterward chamfers will be generated by a new area of the chamfer tool teeth that is not worn yet.

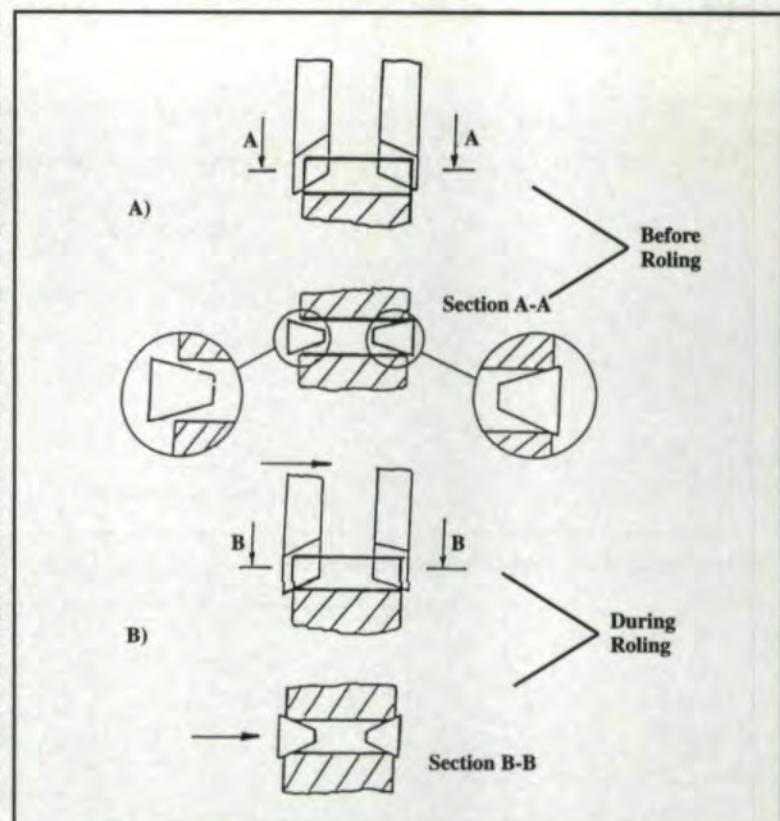


Fig. 11 — A) Nonsymmetrical chamfer tools; B) Symmetrical chamfer tools.

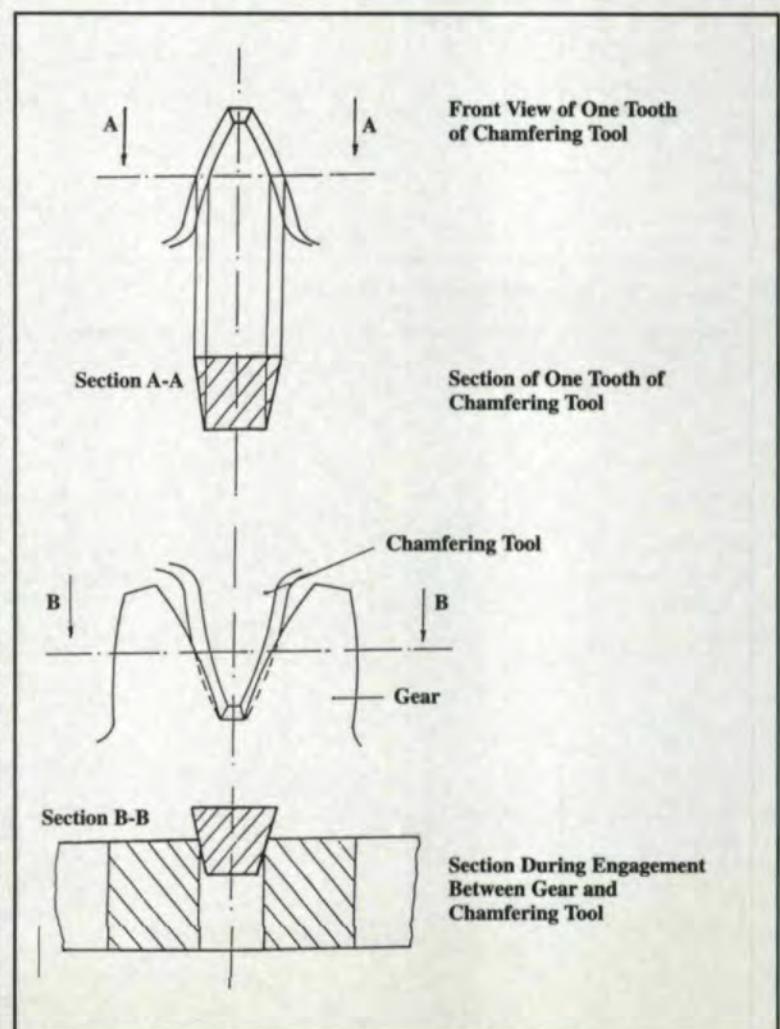


Fig. 12 — Gear tooth and chamfering tool tooth sections.

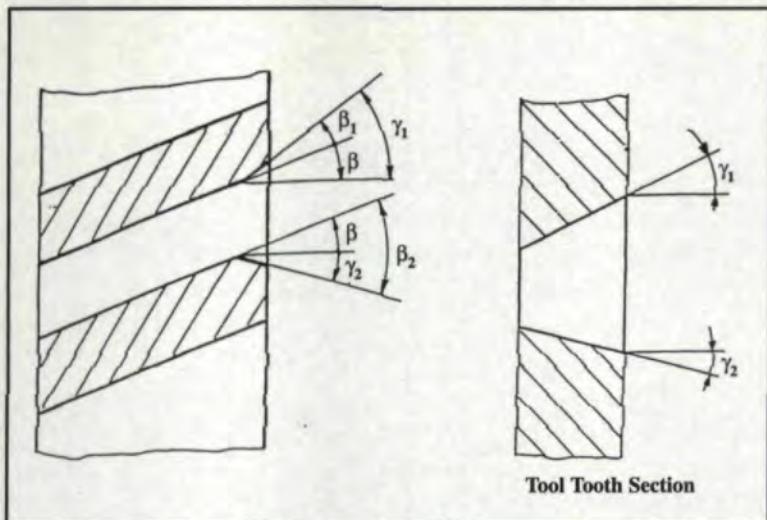


Fig. 13 — Section view of deburring tools in mesh with gear.

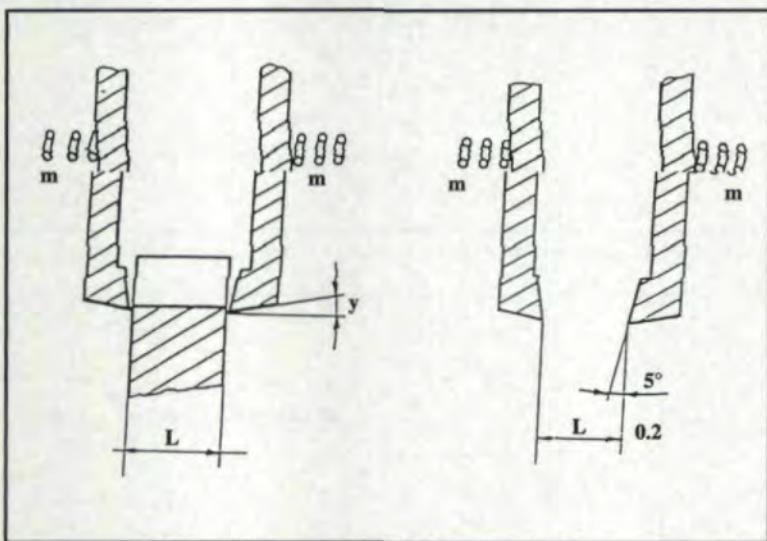


Fig. 14 — “R” type deburring tool in mesh with gear.

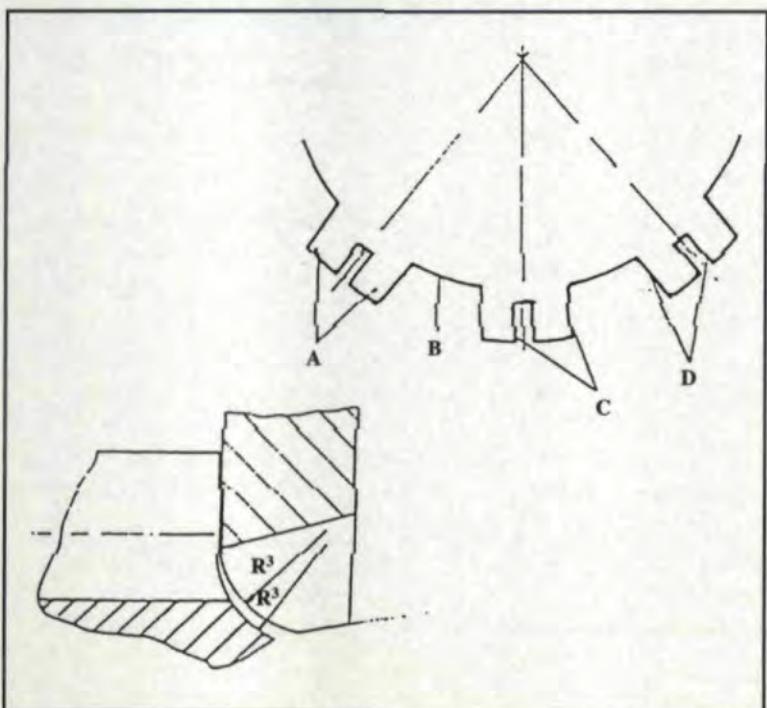


Fig. 15 — Cross sectional view of deburring tool.

Each chamfering disc can be utilized three or four times. When the chamfers no longer have a constant size from one gear tooth to another when the rolling stress rises, or when each single chamfer is no longer uniform along the profile, it is time to grind the chamfering discs in such a way that a new rolling area will contact with the edges of the gear teeth.

Deburr Tools

Deburring tools are large diameter discs whose external rims are ground to the rake angles necessary for cutting action. The distance between the two discs is not constant because they can move axially either under the action of the springs (“m” shown in Fig. 14) or as a consequence of the self-centering with the gear to be deburred.

In the rest position, the spring pressure on the deburring discs brings their separation distance to a minimal value, which is about 0.008" (0.2 mm) less than the minimum gear width. If the distance between the discs were fixed, the discs themselves would hit the outside diameter of the workpiece, chipping it when discs are plunge-fed towards the workpiece. To avoid this, the cutting edge of each disc is provided with a tapered lead-in whose size is large enough to avoid hitting the outside diameter of the gear to be deburred. The first contact must occur between the lead-in surface and the workpiece outside diameter.

The deburring discs are rotated by the workpiece itself, and the burrs are removed through a true skiving action on the gear lateral faces. Generally 100,000 pieces or more in some cases can be deburred before resharpening the tool. The tool life between resharpenings depends upon a number of factors. They are

- The hardness and machinability of workpiece material;
- The thickness of burrs and the size of the requested chamfer;
- The length of the deburred area (workpiece whole depth);
- The presence of steps, radii or shoulders, which may interfere with the tool cutting edge;
- The correct resharpening and assembly of the tool group.

Special Cases

For gears with shoulders or radii, special types of deburring tools are designed for a correct action of the deburring discs in order to avoid the interference. To deburr a gear with a radius (see Fig. 15), a special type of deburring tool known as an “R” type tool is used. Due to the spring loading action, the burrs are uniformly and cleanly skived off the surface by the tool following the profile of the gear. The same tool also performs the debur-

ring of the straight portion. The radius form protuberances A are alternated with the cutting edges B, which work the straight portion of surface S like a standard deburring tool. Protuberances A remove burrs from the radii by means of the true cutting action of the cutting edges C or D according to the direction of rotation. Portion B skives the straight faces as far as .008" (0.2 mm) to 0.012" (0.3 mm) above radius R^3 .

When the surface to be deburred is tapered, specially tapered deburring tools with many inclined slots are used to generate an adequate number of sharp cutting edges. During helical gear cutting with either a hob or with a shaper cutter, burrs are usually left on the acute edge (where the tool comes out of the gear). The relative traverse movement between the deburring tool and the gear must push the burr toward the tooth and not toward the space.

Deburring Tool Sharpening

Wear can be removed by grinding either surface E or surface H (see Fig. 16A). Stock size removed must be 0.008" (0.2 mm) or its multiples in the direction of the disc's axis. The disc thickness reduction is compensated for by shifting the spacers.

With no gear between the tools, the discs are in the conditions shown in Fig. 16B. The springs push the disc and the spacer against the shoulder flange. When the gear enters the discs, it forces the discs apart, thus moving the tool from the shoulder flange and creating a gap approximately 0.004" (0.1 mm) between flange and spacers (see Fig. 17). After resharpening the gap will not be the same. In order to return to the initial conditions, a space 0.008" (0.2 mm) thick will have to be shifted from position 1 to position 2 as shown in Fig. 18. After every resharpening, it is necessary to check the lead in chamfer size so that it lies outside of the gear when the tool contacts the gear. *

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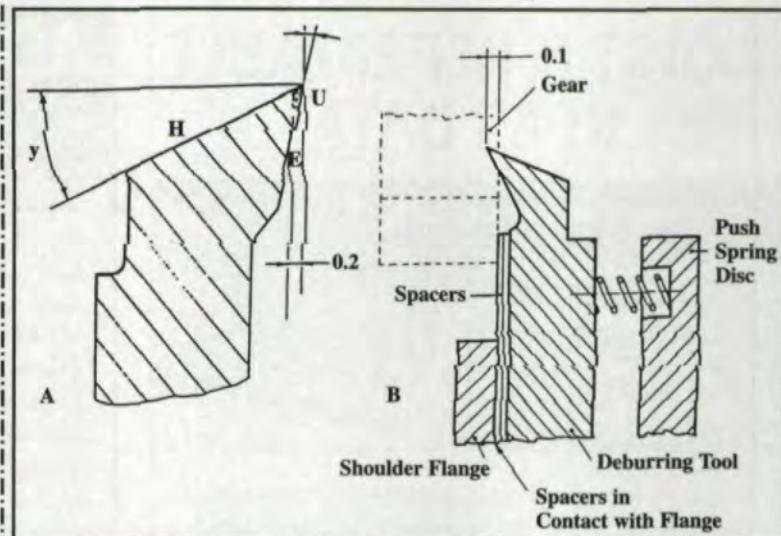


Fig. 16 — Principle of deburring tool operation.

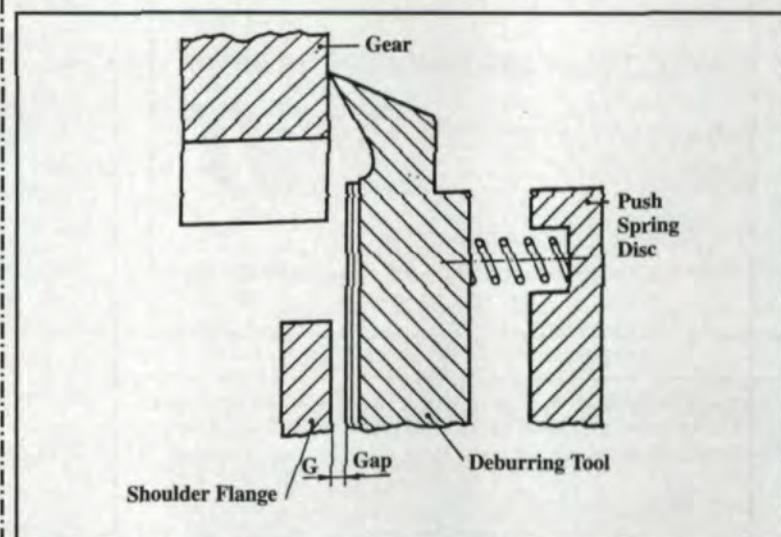


Fig. 17 — Cross sectional view of deburring tool with spacers and springs.

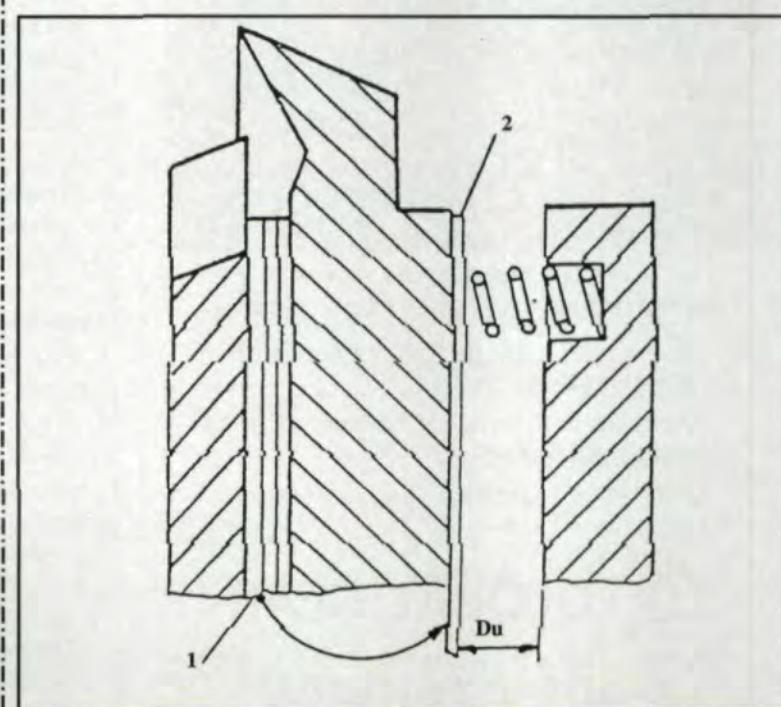


Fig. 18 — Position shift after resharpening.

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Axicom Technologies	Modern Industries Inc.	Spline Gauges Ltd.	Precision Engineering Services	Aerocom Industries Inc.	
Best Engineering Co.	National Metrology	Sussex Gear Company	Philadelphia Gear — GSD	Akron Gear & Engineering	
C-Dot Engineering	Philadelphia Gear — GSD	Trogetec Inc.	Power Eng. & Mfg. Ltd.	Alpha Precision Inc.	
Chicago Gear Works	Power Eng. & Mfg. Ltd.	Universal Technical Systems	Precision Gear Co.	American Pfauter L.P.	
Ciateq A.C.	Reilly Engineering Inc.	Van Gerpen-Reece Eng.	Precision Gear Inc.	American Stress Technologies	
Dabko Industries Inc.	Robotronix	Von Ruden Mfg.	Pro-Gear Co. Inc.	American Sykes Co.	
Dayton Gear & Tool	Technimet Corp.	Wedin Int'l. Inc.	Process Industries	Aplus Engineering Inc.	
Drive Systems Technology	Trogetec Inc.	Westech Gear	The Purdy Corp.	Ashot Ashkelon Indust.	
Dynamic Metal Treating	Wes-Tex Gear Inc.	Winzeler Gear	Qualcast Corp.	Ashot U.S.A. Inc.	
Engranes Industriales Rivera	Westech Gear	Wohlert Corp.	Reef Gear Mfg.	Axicon Technologies	
Fairfield Mfg. Co.	Xtek Inc.	Xtek Inc.	Riley Gear Corp.	Best Engineering Inc.	
Gary P. Mowers, P.C.	Gear Design	Gear Engineering	Riverside Spline & Gear	Boeing Precision Gear	
The Gleason Works	A. W. Sadler Machine	A. W. Sadler Machine	Robotronix	Bourn & Koch	
Guy Crader Consulting	ABA-PGT Inc.	ABA-PGT Inc.	Southern Gear & Machine	Machine Tool	
GW Plastics	Advance Gear & Machine Corp.	Advance Gear & Machine	RD Industries	Brighton Industries	
Hy-Mech Systems Inc.	Akron Gear & Engineering	Aplus Engineering Inc.	Reef Gear Mfg.	Brown & Sharpe Mfg.	
I.S.P.J.A.E.	Aplus Engineering Inc.	Applied Mechaniques	Riley Gear Corp.	Cincinnati Gear	
Impact Strategies	Applied Mechaniques	Ashot Ashkelon Indust.	Robotronix	Columbia Gear Corp.	
Intech Corp.	Ashot U.S.A. Inc.	Axicon Technologies	Southern Gear & Machine	D.I.G.I.T.	
Jack Dustman & Assoc.	BestMetal Corp.	BestMetal Corp.	Machine	Dayton Gear & Tool	
James Reid Gear Services	C-Dot Engineering	Brown & Sharpe Mfg.	SU America	Disston Precision Inc.	
Management & Engineering Tech.	Caterpillar Industrial Products Inc.	C-Dot Engineering	Tifco Gage & Gear	Dynamic Metal Treating	
Manufactured Gear & Gage	Ciateq A.C.	Ciateq A.C.	USACH Technologies	Engranes Industriales Rivera	
McGinty Gear	Cincinnati Gear	Cincinnati Gear	Viking Air Tools	Equitable Engineering	
Milburn Engineering	CMD (UK) Ltd.	CMD (UK) Ltd.	Wedin Int'l. Inc.	Euro-Tech Corporation	
Milford Gear Works	Cone Drive Operations	Cone Drive Operations	Westech Gear	Fairfield Mfg. Co.	
Moore Machine & Gear	Contour Hardening Inc.	Contour Hardening Inc.	Winzeler Gear	Forest City Gear Co.	
NCADT	Cunningham Industries	Cunningham Industries	Wohlert Corp.	Fuller Company	
NASA Lewis Research Center	Dayton Gear & Tool	Dayton Gear & Tool	Xtek Inc.	Gary P. Mowers, P.C.	
Ontario Drive & Gear	Deco-Technologies	Deco-Technologies	Grinding	GEARCOA	
Pfauter Maag Tools, L.P.	DMS Inc.	DMS Inc.	Advance Gear & Machine Corp.	Gear Motions	
Power Eng. & Mfg. Ltd.	Drive Systems Technology	Drive Systems Technology	AeroCom Industries Inc.	The Gear Works Seattle	
Precision Engineering Services	Dynamic Tool Grinding Service	Dynamic Tool Grinding Service	Akron Gear & Engineering	Gears & Drive Systems	
Profile Engineering	EMCO Gears	EMCO Gears	American Pfauter L.P.	The Gleason Works	
Reilly Engineering Inc.	Engranes Industriales Rivera	Engranes Industriales Rivera	Aplus Engineering Inc.	Harder Precision Components	
Sales Consultants	Engrante de Mexico	Engrante de Mexico	Ashot Ashkelon Indust.	Highway Machine Co.	
SBR Consulting	Equitable Engineering	Equitable Engineering	Ashot U.S.A. Inc.	Interstate Tool Corp.	
Society of Manufacturing Engineers	Fairfield Mfg. Co.	Fairfield Mfg. Co.	Axicon Technologies	Invo Spline Inc.	
Engranes Industriales Rivera	Fairlane Gear Inc.	Fairlane Gear Inc.	Boeing Precision Gear	Jack Dustman & Assoc.	
Fairfield Mfg. Co.	Gary P. Mowers, P.C.	Gary P. Mowers, P.C.	Brighton Industries	Krautkramer Branson	
Robotronix	The Gear Works Seattle	The Gear Works Seattle	Caterpillar Industrial Products Inc.	Lawler Gear Corp.	
Ty Miles Inc.	Gearesearch Assoc.	Gearesearch Assoc.	Caterpillar Industrial Products Inc.	M&M Precision Systems	
U.S. Tech Corp.	General Electric	General Electric	Fairfield Mfg. Co.	Mahr Corp.	
Van Gerpen-Reece Eng.	Generated Gear & Machine	Generated Gear & Machine	Fellows Corp.	Manufactured Gear & Gage	
Welin Int'l. Inc.	The Gleason Works	The Gleason Works	Foot-Jones/Illinois Gear	Merit Gear Corp.	
Wes-Tex Gear Inc.	Guy Crader Consulting	Guy Crader Consulting	FPM Heat Treating	Midwest Gear	
Westech Gear	GW Plastics	GW Plastics	Gary P. Mowers, P.C.	Modern Industries Inc.	
Winzeler Gear	Harder Precision Components	Harder Precision Components	Gear Motions	Moore Machine & Gear	
Cryogenics	Highway Machine Co.	Highway Machine Co.	Federal Gear Corp.	National Metrology	
Boeing Precision Gear	Holroyd Machine Tools	Holroyd Machine Tools	Fender Gear Corporation	National Broach & Machine Co.	
Fairfield Mfg. Co.	Hy-Mech Systems Inc.	Hy-Mech Systems Inc.	Franke Gear Works	NCADT	
Robotronix	I.S.P.J.A.E.	I.S.P.J.A.E.	General Electric	Niagara Gear Corp.	
Fault Analysis	InSCO Corp.	InSCO Corp.	The Gleason Works	Patterson Gear & Machine	
Akron Gear & Engineering	ITW Spiroid	ITW Spiroid	Guy Crader Consulting	Perry Technology Corp.	
Applied Mechaniques	Labeco	Labeco	GW Plastics	Philadelphia Gear — GSD	
Ashot Ashkelon Indust.	McGinty Gear	McGinty Gear	Harder Precision	Power Eng. & Mfg. Ltd.	
Aston Metallurgical Services	Milburn Engineering	Milburn Engineering	Components	Precision Gage Co.	
Splines Gauges Ltd.	Milford Gear Works	Milford Gear Works	Highway Machine Co.	Precision Gear Inc.	
Sussex Gear Company	Moore Machine & Gear	Moore Machine & Gear	Holroyd Machine Tools	Precision Gears Inc.	
Swiglo Metallurgical Consulting	O'Neill Gear	O'Neill Gear	Hy-Mech Systems Inc.	Process Industries	
Trogetec Inc.	Ontario Drive & Gear	Ontario Drive & Gear	I.S.P.J.A.E.	Profile Engineering	
Ty Miles Inc.	Power Eng. & Mfg. Ltd.	Power Eng. & Mfg. Ltd.	InSCO Corp.	The Purdy Corp.	
U.S. Tech Corp.	Precision Engineering Services	Precision Engineering Services	Intech Corp.	Qualcast Corp.	
Van Gerpen-Reece Eng.	Holroyd Machine Tools	Holroyd Machine Tools	Labeco	Progressive Engineering	
Welin Int'l. Inc.	Hy-Mech Systems Inc.	Hy-Mech Systems Inc.	M&M Precision Systems	Qualcast Corp.	
Wes-Tex Gear Inc.	I.S.P.J.A.E.	I.S.P.J.A.E.	Milburn Engineering	Robotronix	
Westech Gear	InSCO Corp.	InSCO Corp.	Milford Gear Works	Robotronix	
Winzeler Gear	ITW Spiroid	ITW Spiroid	Midwest Gear	Tocco Inc.	
Cryogenics	Labeco	Labeco	Modern Industries Inc.	U. S. Axle Inc.	
Boeing Precision Gear	McGinty Gear	McGinty Gear	Midwest Gear		
Fairfield Mfg. Co.	Milburn Engineering	Milburn Engineering	Reef Gear Mfg.		
Robotronix	Milford Gear Works	Milford Gear Works	Riley Gear Mfg.		
Fault Analysis	Moore Machine & Gear	Moore Machine & Gear			
Akron Gear & Engineering	O'Neill Gear	O'Neill Gear			
Applied Mechaniques	Ontario Drive & Gear	Ontario Drive & Gear			
Ashot Ashkelon Indust.	Power Eng. & Mfg. Ltd.	Power Eng. & Mfg. Ltd.			
Aston Metallurgical Services	Precision Engineering Services	Precision Engineering Services			

PRODUCTS & SERVICES INDEX

Riverside Spline & Gear
Roto-Technology Inc.
 Schafer Gear Works
 Scott Machine Tool Co.
 Southern Gear &
 Machine
 Spline Gauges Ltd.
 Tifco Gage & Gear
 Trogetec Inc.
 UBM Corp.
 Ultron Incorporated
 Viking Air Tools
 Wedin Intl. Inc.
 Westech Gear
 Winzeler Gear

Shot Peening

Ashot Ashkelon Indust.
 Ashot U.S.A. Inc.
 Boeing Precision Gear
 Cincinnati Gear
 Columbia Gear Corp.
 Dayton Gear & Tool
 Fairfield Mfg. Co.
 Harder Precision
 Components
 Patterson Gear &
 Machine
 Progressive Technologies
 RD Industries

Tool Coating

American Pfauter L.P.
 Balzers Tool Coating
 Best Engineering Co.
 Diamond Black Tech
 Dynamic Metal Treating
 Eltech Inc.
 General Magnaplate
 LMT-Fette Inc.
 Multi-Arc Inc.
 Reid Tool Service Inc.
 Richter Precision Inc.
Star Cutter Co.
 Wohlert Corp.

Other Services

American Metal
 Treating — Induction
 Hardening
 Ascent Drafting Service
 — Drafting Services
 ASM International —
 Training, Education,
 Books
 Aston Metallurgical
 Services —
 Metallurgical Testing
 Becker Gearmeisters
 Inc. — Machine
 Calibration
 Capital Associates
 International —
 Machinery Leasing &
 Financing
 Clifford-Jacobs Forging
 Co. — Forging
 Detroit Flame
 Hardening — Flame
 Hardening
 Elmass North America
 Inc. — Broaching &
 Keyseating Services
 Eltech Inc. — Hob
 Sharpening
 Fairlane Gear Inc. —
 Noise Evaluation
 General Magnaplate
 Corp. — Protective
 Coatings
 Hane Industrial Training
 — Gear School
Holroyd Machine Tools
 — Complete
 Manufacture

Hy-Mech Systems Inc.
 — Training Seminars,
 Gear & Hydraulic
 Product Design
 Impact Strategies Inc. —
 Engineering/Market-
 ing/Consulting for the
 Metalworking & Heat
 Treating Industries
 Intech Corp. —
 Durability
 Calculations
 International Financial
 Services —
 Machinery &
 Equipment Financing
 James Reid Gear
 Services —
 Productivity &
 Quality Improvement
Koro Sharpening
 Service — HSS &
 Carbide Hob
 Sharpening
 McGinty Gear — Spline
 Design
 Metlab — Carburizing,
 Nitriding
 Mikrofinish — Wear
 Enhancement
 Mitts & Merrill, L.P. —
 Keyway Machining
 Modern Industries Inc.
 — Metallurgical
 Evaluation
 Modified Gear & Spline
 — Crown Grinding
 Morrison Knudsen —
 Engineering Consultants
 National Metrology —
 Machinery
 Calibration
 NCADT — Condition-
 Based Maintenance
 Paulo Products Co. —
 Metallurgical Support
 & Services
 Precision Engineering
 Services —
 Probabilistic Error
 Analysis
 Progressive Tool Co. —
 Wire EDM
 Spline Gauges Ltd. —
 Plotting & Analysis of
 Gear Stresses
 Stearns Financial —
 Machinery Financing
 Sussex Gear Company
 Inc. — Gearbox &
 Actuator Design
 Technimet Corp. —
 Materials Selection &
 Testing
 Tri-Wire Inc. — Wire
 EDM
 Trogetec — Custom
 Design & Software

GEAR SOFTWARE

Custom

Ace World Company
American Pfauter L.P.
 American Sykes Co.
 Aplus Engineering Inc.
 C-Dot Engineering
 Ciateq A.C.
 Gearesearch Assoc.
 Gearsoft Design
 Hoglund Technology
 I.S.P.J.A.E.
Mahr Corp.
 Metal Powder Industries
 Federation

Metscope Corp.
Moore Products Co.
 NASA Lewis Research
 Center
 PC Enterprises
 R.H. Software
Roto-Technology Inc.
 Scott Machine Tool Co.
 Software Engineering
 Service
 Trogetec Inc.
 Universal Technical
 Systems
 User Solutions Inc.
 Van Gerpen-Reece Eng.

Gear Design

ABA-PGT Inc.
 Accu-Promp Inc.
 American Gear Mfgs.
 Assn.
 Bluegrass Precision
 Machinery
 C-Dot Engineering
 Ciateq A.C.
 Dabko Industries Inc.
 Designatronics
 Fairfield Mfg. Co.
 Gearesearch Assoc.
 Gearsoft Design
 Geartech
 The Gleason Works
 I.S.P.J.A.E.
 NASA Lewis Research
 PC Enterprises
 Software Engineering
 Service
 Trogetec Inc.
 Universal Technical
 Systems
 Van Gerpen-Reece Eng.

Gear Inspection

Alpha Precision Inc.
 American Machinery &
 Engineering
 American Stress
 Technologies
American Pfauter L.P.
 American Sykes Co.
 Bourn & Koch Machine
 Tool
 Brighton Industries
 Brown & Sharpe Mfg.
 Euro-Tech Corporation
 Gearesearch Assoc.
 The Gleason Works
 Krautkramer Branson
 M&M Precision
 Systems
 Metrscope Corp.
Moore Products Co.
 NCADT
 PC Enterprises
 Precision Gage Co.
 R.H. Software
Roto-Technology Inc.
 Scott Machine Tool Co.
 Software Engineering
 Service
 Trogetec Inc.
 Universal Technical
 Systems

Shop Management

American Pfauter L.P.
 JobBOSS Software Inc.
 Metrscope Corp.
 R.H. Software
 Scott Machine Tool Co.
 U.S. Tech Corp.
 User Solutions Inc.

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CIRCLE 161

PRODUCTS & SERVICES INDEX

Other Software

Bourn & Koch — Gear Manufacturing Software
Drive Systems Technology — Software Available Through Seminars Engis — "Diaform" Proprietary Software Euro-Tech Corporation — Spline Inspection Gearsearch Assoc. — Gear Scoring Analysis Hognlund Technology Corp. — Gear Manufacturing Software JobBOSS Software Inc. — Business Management & Shop Floor Control for Gear Shops Krautkramer Branson — Inspection Data Management Meccanica Nova Corp. — Grinding Machine Software Metal Powder Industries Fed. — Powder Metal Design Software Normac Inc. — Gear Grinding Software U.S. Tech Corp. — CNC Control, Asset Management Software Van Gerpen-Reece Eng. — Tooling Re-Use

GEAR TOOLING & GEAR ACCESSORIES

Abrasives

Abrasive Technology American Pfauter L.P. American Sykes Co. Bates Technologies Inc. Best Engineering Co. Bluegrass Precision Machinery Cincinnati Milacron Clipper Diamond Tool Dianamic Abrasives Engis Corp. Ernst Winter & Son Inc. GMI Lapmaster Intl. Meccanica Nova Corp. Meister Grinding Tech. P. F. Markey Inc. Redin Corp. Rex-Cut Products Inc. Sidney Diamond Tool Star Cutter Co. Sunnen Products Co. W. E. Litwin Assoc. Wendt Dunnington

Broaching Tools

American Sykes Co. Apex Broach & Machine Barit International Best Engineering Co. Brighton Industries Colonial Tool Group Detroit Broach Co. Elmass North America General Broach & Engineering Jack Dustman & Assoc. LMT-Fette Inc. National Broach & Machine Co. The Ohio Broach & Machine

P. F. Markey Inc.

Parker Industries Inc.

Ply-Mar Tool Co. Reid Tool Service Inc. Trogetec Inc. Ty Miles Inc.

Chamfering Tools

American Pfauter L.P. American Sykes Co. Best Engineering Co. The Gleason Works GMI Jack Dustman & Assoc. P. F. Markey Inc. Ply-Mar Tool Co. Reid Tool Service Inc. Schenck Turner SU America

Deburring Tools

Ace World Company American Sykes Co. Best Engineering Co. The Gleason Works GMI Jack Dustman & Assoc. JRM International Inc. Liebherr-America P. F. Markey Inc. Progressive Technologies Redin Corp. Reid Tool Service Inc. Rex-Cut Products Inc. Schenck Turner SU America

EDM Tooling & Supplies

Agie USA Ltd. Bluegrass Precision Machinery Charmilles Technologies Current EDM, Inc. Esaco-Sparceton EDM Solutions Engemaq U.S.A. Hangsterfer's Labs Inc. Hitachi EDM Products KGM International/ Sodick EDM Koolant Koolers Inc. LeBlond Makino Machine Tool Co. Mecatool USA Ltd. Victel Machinery Inc. Xermac Inc.

Form Grinding Wheels

Abrasive Technology American Pfauter L.P. Best Engineering Co. Bluegrass Precision Machinery Brighton Industries Clipper Diamond Tool Engis Corp. Ernst Winter & Son Inc. Hognlund Technology Liebherr-America Meccanica Nova Corp. Meister Grinding Tech. P. F. Markey Inc. Sidney Diamond Tool Star Cutter Co. Wendt Dunnington

Hobs

Ace World Company American Pfauter L.P. American Sykes Co. Axicor Technologies Barit International Basic Incorporated Tool Group Best Engineering Co.

Eltech Inc.

Fellows Corp.

GMI Interstate Tool Corp. JRM International Inc. Koepfer America L.P. Kromhard Twist Drill Liebherr-America LMT-Fette Inc. Mitsubishi Machine Tool National Broach & Machine Co. P. F. Markey Inc.

Parker Industries Inc.

Pfauter-Maag Cutting Tools Ply-Mar Tool Co. Rebco Industrial Products Reid Tool Service Inc. Russell, Holbrook & Henderson

Star Cutter Co.

SU America Tifco Gage & Gear Trogetec Inc.

Keyseat Cutters

Best Engineering Co. Colonial Tool Group Elmass North America Interstate Tool Corp. LMT-Fette Inc. The Ohio Broach & Machine Co. P. F. Markey Inc. Reid Tool Service Inc. Star Cutter Co. W. E. Litwin Assoc.

Lapping Compounds

Cincinnati Milacron Engis Corp. Lapmaster Intl. Liebherr-America P. F. Markey Inc. Reid Tool Service Inc. Sidley Diamond Tool Wendi Dunnington

Lubricants/Coolants

Abrasive Technology Cincinnati Milacron D. A. Stuart Co. Engis Corp. Etna Products Inc. Fiske Brothers Refining Hangsterfer's Labs Inc. Houghton International Jack Dustman & Assoc. Kluber Lubrication North America Lapmaster Intl. Meccanica Nova Corp. Nye Lubricants Inc. P. F. Markey Inc. Sunnen Products Co. Texaco Lubricants Co.

Shaper Cutters

American Pfauter L.P. American Sykes Co. Barit International Best Engineering Co. Elmass North America Eltech Inc.

Fellows Corp.

GMI Interstate Tool Corp. JRM International Inc. Kromhard Twist Drill Liebherr-America Mitsubishi Machine Tool National Broach & Machine Co.

P. F. Markey Inc.

Parker Industries Inc.

Pfauter-Maag Cutting Tools Ply-Mar Tool Co. Rebco Industrial Products Reid Tool Service Inc. Russell, Holbrook & Henderson

Star Cutter Co.

SU America Tifco Gage & Gear Trogetec Inc.

Shaver Cutters

American Pfauter L.P. American Sykes Co. Barit International Best Engineering Co. Eltech Inc. Fellows Corp. The Gleason Works GMI JRM International Inc. LMT-Fette Inc. Mitsubishi Machine Tool

National Broach & Machine Co. P. F. Markey Inc. Parker Industries Inc. Pfauter-Maag Cutting Tools Ply-Mar Tool Co. Rebco Industrial Products Reid Tool Service Inc. Star Cutter Co. W. E. Litwin Assoc.

Spline Gages

Best Engineering Co. Colonial Tool Group Euro-Tech Corporation Invo Spine Inc. Jack Dustman & Assoc. JRM International Inc. M&M Precision Systems

Mahr Corp. The Ohio Broach & Machine Co. Parker Industries Perry Technology Ply-Mar Tool Co. Precision Gage Co. Reid Tool Service Inc. Russell, Holbrook & Henderson

Spline Gages Ltd. Tifco Gage & Gear Trogetec Inc.

Worm Milling Cutters

American Pfauter L.P. American Sykes Co. Barit International Best Engineering Co. GMI Interstate Tool Corp. JRM International Inc. Koepfer America L.P. LMT-Fette Inc. Parker Industries Inc. Pfauter-Maag Cutting Tools

Fellows Corp. Ply-Mar Tool Co. Rebco Industrial Products Reid Tool Service Inc. Russell, Holbrook & Henderson

Star Cutter Co.

Other Tooling & Accessories

A/W Systems Co. — Cutter Bodies & Blades ABA-PGT Inc. — Injection Molds for Gears

American Sykes Co. — Gear Hones, Rack Cutters

Barit International Corp. — Involute Form-Relieved Milling Cutters

Bates Technologies Inc. — Honing Stones & Tooling

Best Engineering Co. — Rack Cutters

Comtorgate Corp. — Hand-Held Dimensional Gages

Dianamic Abrasive — CBN & Diamond Grinding Wheels

Esgard, Inc. — Corrosion Prevention

Hangsterfer's Labs Inc. — Dielectric Fluid

Höfler Maschinenbau GmbH — Double-Tapered Grinding Wheels

Interstate Tool Corp. — Involute Gear Cutters

JRM International Inc. — Hydraulic Clamping

Koolant Koolers Inc. — Industrial Liquid Coolers/Chillers

Meccanica Nova Corp. — In- and Post-Process Machine Gages

Micromatic Textron — Spline Rolling Tools

Normac Inc. — CNC Grinding Wheel Dressers

Oberlin Filter Co. — Coolant Filtration & Media

P. F. Markey Inc. — Superabrasive Hones & Tools

S.L. Munson & Co. — Diamond Gear Dressers

Spline Gauges Ltd. — Powder Metal Gear & Spline Form Tool Sets

Sunnen Products Co. — Bore Gages

Tifco Gage & Gear — Composite Checkers

W. E. Litwin Assoc. — Hard Turning Tools

Wendt Dunnington — Diamond Profile Dressers & Dressing Equipment

GEAR WORKHOLDING & FIXTURING

Arbors

Alpha Precision Inc.

American Pfauter L.P.

American Sykes Co. Best Engineering Co.

Bluco Corp. Bluegrass Precision Machinery

Bourn & Koch Machine Tool

Drewco Corp.

Euro-Tech Corporation Fairlane Gear Inc. The Gear Works Seattle

The Gleason Works

Harder Precision Components

Invo Spine Inc. Jack Dustman & Assoc. JRM International Inc.

LeCount Inc.

M&M Precision Systems

Mahr Corp. Manufactured Gear & Gage

National Broach & Machine Co.

P. F. Markey Inc. Parker Industries Inc. Profile Engineering

Reid Tool Service Inc. Schunk Inc.

Spline Gauges Ltd. Tifco Gage & Gear Toolink Engineering Triangle Machine Tool

W. E. Litwin Assoc.

Chucks

Ajax Chuck Jaws Inc. Alpha Precision Inc.

American Pfauter L.P.

American Sykes Co. Best Engineering Co. Bluegrass Precision Machinery

Bourn & Koch Brighton Industries Drewco Corp.

Euro-Tech Corporation The Gleason Works Harder Precision Components

Invo Spine Inc. Jack Dustman & Assoc. Manufactured Gear & Gage

P. F. Markey Inc. Reid Tool Service Inc. Schunk Inc.

Star Cutter Co.

Toolink Engineering Triangle Machine Tool Trogetec Inc.

W. E. Litwin Assoc.

Modular Fixtures

Ace World Company Alpha Precision Inc.

American Pfauter L.P.

American Sykes Co. Bluco Corp. Bluegrass Precision Machinery

Drewco Corp. Jack Dustman & Assoc. JRM International Inc.

Liebherr-America

Meccanica Nova Corp. Moore Products Co.

P. F. Markey Inc. Paul W. Marino Gages Schunk Inc.

Scott Machine Tool Co. Sunnen Products Co.

Sytec Corp.

Triangle Machine Tool Trogetec Inc.

Viking Air Tools W. E. Litwin Assoc.

PRODUCTS & SERVICES INDEX

Toolholders

Alpha Precision Inc.
American Pfauter L.P.
 Best Engineering Co.
 Bluegrass Precision
 Machinery
 Brighton Industries
 Drewco Corp.
 Elmass North America
 Euro-Tech Corporation
The Gleason Works
 Interstate Tool Corp.
 Jack Dustman & Assoc.
 JRM International Inc.
 Mahr Corp.
 P. F. Markey Inc.
 Reid Tool Service Inc.
 Schunk Inc.
 Toolink Engineering
 Triangle Machine Tool
 Viking Air Tools
 W. E. Litwin Assoc.

Workholding Devices &

Other Fixturing

Bluco — Expanding
 Mandrels for
 Broaches
 Detroit Broach —
 Workholders for
 Broaches
 Eurotech Corp. —
 Compensating
 Washers for Hobs
 General Broach &
 Engineering —
 Workholders for
 Broaches
 Meccanica Nova Corp. —
 Custom Grinding Fix-
 turing & Workholding
Sytec Corp. — Pitch
 Line Work Holding
 Ty Miles Inc. — Broach
 Tooling Systems

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 Jed Heavy Industry-
 Korea
 American Machinery &
 Engineering —
 American Sykes,
 Apex Broach —
 Fellows, Höfler
 Grinders, Koepfer,
 M & M, Star Cutter,
 American Pfauter L.P.
 — Zeiss-Hofler,
 Hurth, Kapp

American Sykes Co. —
 James Technologies
 American Wera Inc. —
 Wera Werk, Hurth

Modul, Samag
 Ashot U.S.A. Inc. —
 Ashot Ashkelon
 Industries

Ataka Engineering Co.
 — Saikuni Mfg. Co.

Bazell Technologies —
 Microseparato

Bluegrass Precision
 Machinery —
 Mitsubishi

Brighton Industries
 Corp. — Normac Inc.

Commerical Gear &
 Sprocket —
 U.S. Tsubaki

Eltech Inc. —
 SU America Inc.,
 Niles

Engis Corp. —

Diaform Proprietary
 Euro-Tech Corporation —
 Fresco & Mytec
 Gear Group
 International —
 Katsa, Parkland,
 Tasowheel
 Harder Precision
 Components —
 H.P.C. Components
 Jack Dustman &
 Assoc. —
 American Broach
 JRM International Inc.
 Kesel, Saazor, Schrem
Liebherr-America —
 Liebherr, Lorenz,
 Oerlikon, Klingelberg
 Meccanica Nova Corp. —
 Meccanica Nova

Miller Industrial
 Services, Inc. —
 Ohio Broach &
 Machine, Tornos

Technologies, UVA
 Grinding Systems
 National Metrology —
 Metronics

Ontario Drive & Gear —
 KTR

Paul W. Marino Gages —
 Alufix, Koba

Precision Gage Co. —
 Vari-Roll gear testers

Reid Tool Service Inc. —
 Fellows Corp.

S.L. Munson & Co. —
 Dr. Kaiser Diamond
 Products

Southern Sales &
 Engineering —
 Horsburgh & Scott

Spline Gauges Ltd. —
 M & M Precision
 Systems Inc.

Toolink Engineering —
 König-mtm GmbH

V&R Associates —
 Hurth/Gould &
 Eberhardt

W. C. Divers & Associates
 — National Broach

W. E. Litwin Assoc. —
 Speedgrip Chuck

Professional Tool
 Grinding

Wakefield Group Inc. —
 Tocco, Acme

Manufacturing

TRAINING & EDUCATION

Colleges & Universities

Colorado School of
 Mines

I.S.P.J.A.E.
 Mississippi State Univ.

N. E. Wisconsin
 Technical College

NCADT

Purdue at Indianapolis

Gear Schools

American Gear

Manufacturers Assn.

American Pfauter L.P.

Aplus Engineering, Inc.

Best Engineering Co.

Boston Gear

Bourn & Koch Machine

Tool

Cone Drive Operations

Drive Systems Technology

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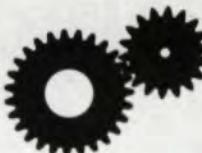
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Welcome to the 1996 *Gear Technology* Buyers Guide Company Index. This year we have more listings than ever to give you even better coverage of the industry.

Use this index to locate the complete contact information for each company listed in the Products and Services Directory. *Gear Technology* advertisers are shown in boldface type. To find the pages on which their ads appear, see the Advertisers Index on page 32.

While *Gear Technology* has made every effort to ensure that company names and addresses are correct, we cannot be held responsible for errors of fact or omission.

If your company is not listed, and you would like to be included in 1997, call 847-437-6604, fax 847-437-6618 or e-mail us at people@geartechnology.com, and we will add you to our mailing list.

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Esgard, Inc.
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Etna Products Inc.
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Euclid Heat Treating Co.
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Euro-Tech Corporation
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Falk Corp.
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Fayscott Co.
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Federal Gear Corp.
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Fellows Corp.
Precision Dr.
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FGT Gage & Systems Inc.
2624 S. 162nd St.
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Finishing Equipment Inc.
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Fiske Brothers Refining Co.
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Flender Corporation
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Fuji Univance Corp.
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Keller Machine Co.
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Keystone Powdered Metal Co.
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Koolant Koolers Inc.
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Koro Sharpening Service
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L + H Welding & Machine Co.
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Latrobe Steel Co.
Division of The Timken Co.
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Fax: 412-532-6316

Lawler Gear Corp.
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LeBlond Makino Machine Tool Co.
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18 Things You Should Know About SPC for Gears

Dr. Hans Bajaria

Statistical Process Control (SPC) and statistical methods in general are useful techniques for identifying and solving complex gear manufacturing consistency and performance problems. Complex problems are those that exist in spite of our best efforts and the application of state-of-the-art engineering knowledge.

Statistical methods approach these problems *results-backward* as opposed to *knowledge-forward*. For example, the knowledge-forward approach would seek consistencies in gear profile, lead, runout, etc., with the assumption that consistencies improve performance. The results-backward approach, on the other hand, will analyze the situations starting from assembly performance. It will then relate performance variation to specific gear characteristics.

In other words, we use our gear expertise in a knowledge-forward approach. When this fails to solve a problem, we should use the results-backward approach. Once critical gear characteristics are determined, we can begin attempting to achieve consistency.

Let us begin by describing six SPC fundamentals and six statistical applications for gear design and manufacturing. These will lead us to an effective sequence for applying statistical methods.

Six Fundamentals of SPC

SPC is only a subset of statistical methods helpful in analyzing complex problems. These methods can be a useful set of tools for carrying out investigations of our manufacturing processes. SPC can chart the output of any process to examine whether the process condition is stable, has an excessive variation or is off-target. Furthermore, SPC can offer clues to strategies for correcting

these conditions. Additional statistical tools can help us establish relationships between problematic process conditions and suspect variables.

1. Multivariate (T^2) Charts are useful in understanding and controlling correlated performance characteristics. The performance characteristics of assemblies, such as noise, durability, ease of maneuverability, etc., are likely to be correlated. That means, for example, that trying to reduce the noise may result in losing maneuverability, or improvement of maneuverability may result in a reduced durability, and so on. The problems associated with correlated characteristics can only be defined with the use of a multivariate chart (see Fig. 1).

2. Multivariate (T^2) Charts are also useful in understanding and controlling input gear characteristics. Gear characteristics are most likely to be correlative because they are generated simultaneously. In practical terms, we can state that when characteristics are correlated, each individual characteristic can be within specification, and yet jointly they constitute a statistical instability.

3. Multi-vari Charts are useful in analyzing size as well as shape problems. For example, four teeth on a gear measured by conventional means may all individually be within specification, and yet differences among them may be the root cause of a problem. A proper way to define a problem that takes into account characteristics of each tooth individually as well as differences among the four teeth is a multi-vari chart (See Fig. 2).

Multi-vari and multivariate charts are different. Multi-vari charts analyze variations within a given characteristic, whereas multivariate charts analyze

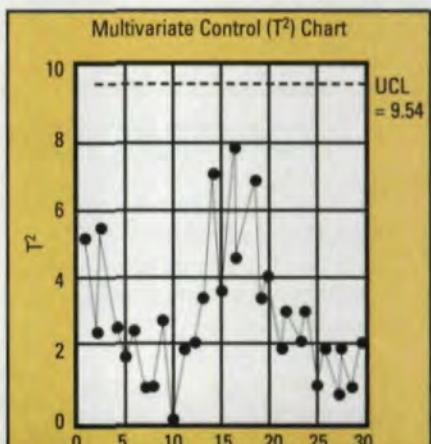


Fig. 1 — This T^2 chart combines 3 characteristics—tip, form and high point—in a single entity.

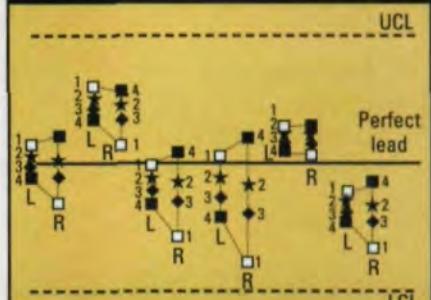
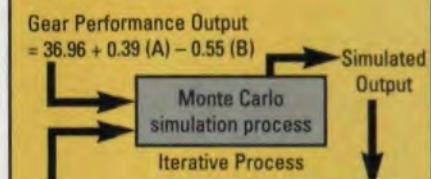


Fig. 2 — A multi-vari chart showing lead variation on 4 left and 4 right teeth simultaneously.

Equation Derived From Multiple Regression Analysis



Distributions of Random Variables A and B
 Random Variables: Gear Characteristic A
 Gear Characteristic B

Fig. 3 — A Monte Carlo simulation.

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relation and variation between two or more characteristics.

4. Multivariate Analysis is useful in analyzing process instabilities and relating them to process variables. An instability is characterized by an abnormal condition on a control chart. To understand the source of unstable behavior, we generally analyze process variables. If process variables are stable, then we look for the explanation elsewhere. Multivariate analysis captures the

missed opportunities in analyzing process variables that we have prematurely concluded to be noncontributory. For example, (A) incoming material condition, (B) workpiece speed and (C) tool feed may all appear to be within normal range when analyzing an instability visible on a control chart. Conventional wisdom leads us to look elsewhere for the root cause. A multivariate chart will offer additional help by analyzing T^2_{AB} , T^2_{AC} , T^2_{BC} and T^2_{ABC} . If this aid is not

utilized, it is possible that the instability may remain a mystery.

5. Multiple Regression Analysis is useful in establishing relationships between gear performance characteristics and gear characteristics. Neither worst-case tolerancing nor statistical tolerancing alone are sufficient to fully understand how gear characteristics affect the performance of assemblies containing gears. Such understanding can only be developed through probabilistic relationships based on actual data rather than any theoretical considerations. Multiple regression analysis helps develop this relationship.

6. Monte Carlo Simulations are computer-based, iterative statistical procedures wherein we determine targets and ranges of critical gear characteristics to match targets and ranges of performance. The inputs to the simulation processes are probabilistic equations and targets and ranges of gear characteristics. The output from the simulation processes are the target and range of performance (see Fig. 3).

Six Applications for SPC in Gear Manufacturing

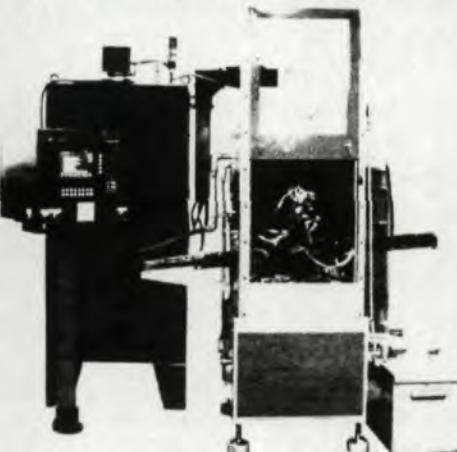
1. Acceptable as well as unacceptable production of gears can best be characterized by using SPC. Gear characteristics that fall within specifications are not in themselves indications of the quality of the processes that produced them. For example, an acceptable gear profile is judged by a specified envelope. However, the process that created the envelope is a multivariate process; that is, three characteristics that make up the gear profile—tip, form and high point—are produced simultaneously. A correct judgment about the process condition responsible for these characteristics can only be made with a T^2 chart. Any decisions regarding process actions based on specifications tend to produce either overreactions or underreactions. While gear metrology is very advanced, it does not go far enough in integrating SPC for process actions.

2. Effects of design and production of gear characteristics on gear performance can best be characterized by using SPC. Gear characteristics are simultaneously

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GEAR FUNDAMENTALS

generated and therefore, we must judge their acceptability together, rather than discretely. The issue of joint acceptability does not get enough coverage either in standards or at gear design and manufacturing conferences.

3. Output performance characteristics of assemblies containing gears, such as durability, noise, ease of transmission under quickly changing inputs and smoothness of transmission, are correlated to one another. Knowledge of these correlations is critical to the SPC of assemblies. These correlations can be quantified using statistical methods.

4. Suspect gear characteristics that contribute to poor performance of assemblies are most likely correlated to one another. Knowledge of these correlations is critical to the SPC of gear manufacturing processes. These correlations can be quantified by using statistical methods.

5. Manufacturing precision of gear characteristics is uneconomical until statistical relationships between gear characteristics and assembly performance are first established. In one example, a lead variation was found to be almost 95% out of specification, and yet assemblies containing the gears with such excessive variation only suffered 5% reject rate. If we rush to solve the lead variation problem at great expense, there is no guarantee that the 5% assembly reject rate will go down. How a 95% out of spec gear characteristic can cause only a 5% assembly fallout can be explained only through statistical relationships.

6. Without the use of statistical methods, it is almost impossible to separate the effects of machining and heat treating on manufacturing variation. Without such clear separation, fully resolving variation problems is impossible.

Recommended Sequence for Deploying SPC & Statistical Methods

1. Establish a statistical relationship between assembly performance and gear characteristics. Then select eight assemblies with acceptable performance and eight assemblies with borderline or unacceptable performance. It may not be easy to find 16 assemblies if you are in the

prototype stage. In that case, select the following alternate route to generating 16 assemblies. Take two assemblies. Any gear assemblies will have a minimum of four parts. By swapping these four parts between two assemblies, you can generate 16 assemblies for purposes of statistical analysis. Use multiple regression to analyze the data and generate an equation between performance characteristics and gear characteristics.

2. Use Monte Carlo simulations to establish targets and ranges of gear characteristics to match performance targets and ranges.

3. Investigate whether any correlations exist among critical gear characteristics. Use correlation analysis.

4. If correlations are high, use a multivariate (T^2) chart to monitor the output.

5. If correlations are low, use either average and range (X-R) charts (Fig. 4) or

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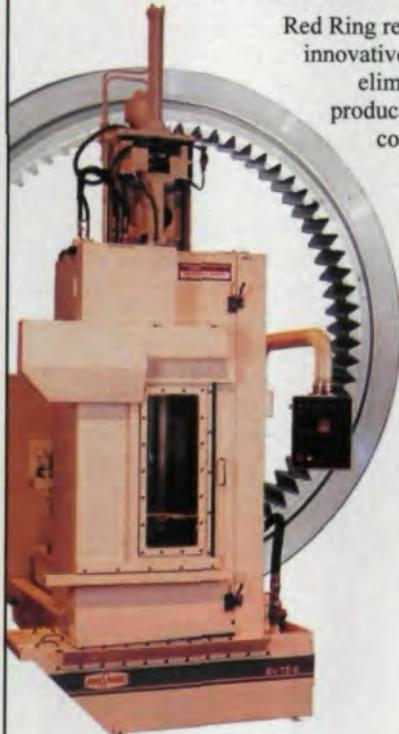
individuals and moving range (\bar{X} -MR) charts (Fig. 5) for monitoring each individual gear characteristic. To select either set of charts, first determine whether a process output is homogeneous or heterogeneous. Do this by taking a group of five consecutive pieces and examining its range. If the range is one-half of the specification range or lower, the process output is homogeneous. Otherwise it is heterogeneous. If the process is homogeneous, use X-MR charts for monitoring

process output. If the process is heterogeneous, use \bar{X} -R charts.

6. Because differences among teeth are contributing factors to ultimate gear performance, a multi-vari chart must accompany all the other charts to understand and control tooth-to-tooth variation within a gear.

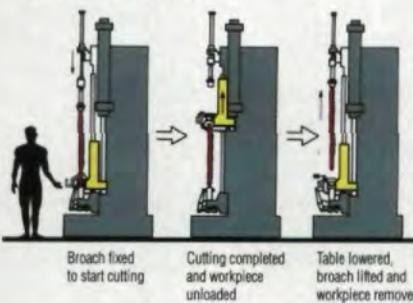
The above described sequence is an investigative use of SPC. If any problems are uncovered as a result of this exercise, we can begin the solution

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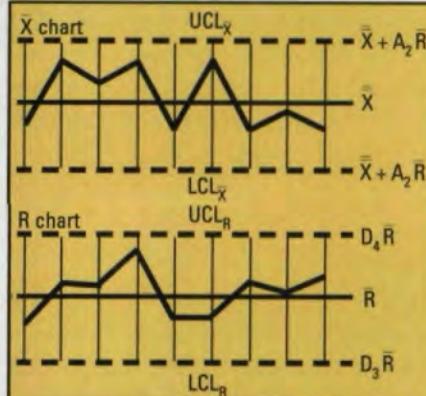


Fig. 4 — Data in the form of an X-R chart.

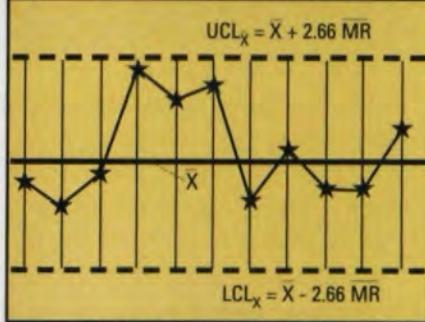


Fig. 5 — Data in the form of individuals (X).

process. If no problems are uncovered, we may choose to use SPC from this point on in the process for monitoring output. Inappropriate variations can then serve as a warning of incipient problem conditions.

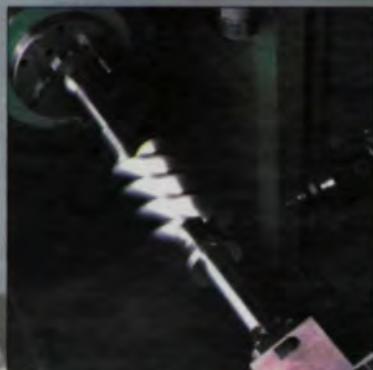
Statistical tools may come to the rescue when you are confronted with puzzling gear problems. SPC, a results-backward approach, is a complement to the more traditional knowledge-forward approaches to gear problem solving. Once you develop expertise in the use of these methods, you will find they also accelerate and improve the productivity of your knowledge-forward approaches as well. ☀

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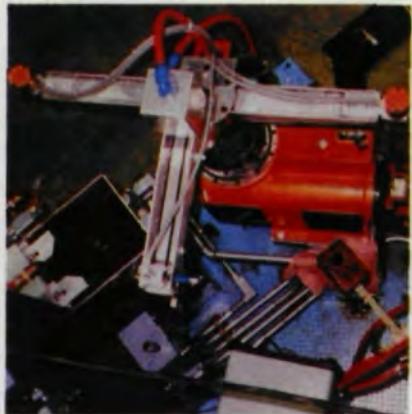
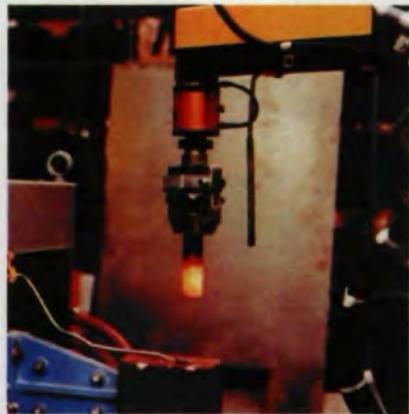
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PRODUCT NEWS

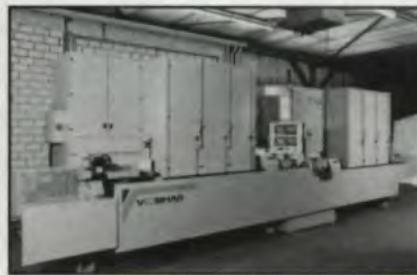
Welcome to our Product News page. Here we feature new products of interest to the gear and gear products markets. To get more information on these items, please circle the Reader Service Number shown.



Vertical Honing Machine

Sunnen's new CK-21 computerized vertical honing machine is designed for precision honing of 3/4" (19 mm) to 8" (203 mm) bores in applications such as small engine blocks, air compressor cylinders, valve bodies and aircraft cylinders. The unit features a microprocessor based control system that enables the operator to control all aspects of the production cycle. The machine has a 3 hp (2.2 kW) spindle motor, and its new hone heads are designed for use with superabrasives. It has a real-time graphic display, will hold the geometry of the bore to within 2 tenths (6 microns), depending on the application, and allows for two different spindle speeds and multiple feed rates during a single honing cycle.

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Deburring Machines

Feintool Equipment Corp. is marketing the complete line of Vobhag deburring machines, which come equipped with optional PC-based process controls to compensate for brush or fleece wear automatically. All models let users fine-tune speeds of both head and brushes to "debug" the deburring process without hardware changes. The units all use linear guides to position the Rotex head to ensure the rigidity necessary for high-force fleece deburring. The control area and work zone are sealed and separate from one another for operator safety and to guard against drive contamination.

Circle 327

warning devices. The VC920 features a 4-20 mA output for system integration with a PLC and a buffered output for instant vibration analysis. It accepts all power supplies (115/230 V A/C, 24 V DC) and is easily mounted on rails or within a cabinet enclosure.

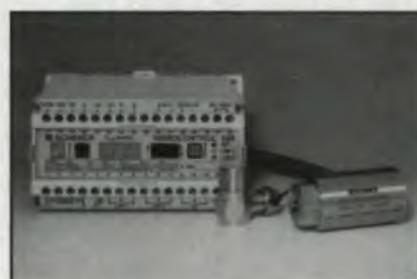
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Brinell Hardness Tester

NewAge Industries, Inc., announces the HB3000 Series Brinell hardness tester with motorized dead-weight load application and automatic readout options to reduce sources of error in Brinell testing. The basic tester operates in any Brinell range from 62.5 to 3000 kg loads and with 2.5, 5 or 10 mm ball indentors. The capacity is 9" vertical and 4.5" throat depth. The BOSS Automatic Readout Option uses a handheld scanning head that views the Brinell impression. The software measures the impression at many angles to derive the Brinell hardness and impression diameters. Outputs include histograms, X-Bar & R charts and RS 232 output to a printer, computer or data gathering system.

Circle 329



Digital AC Servomotors

Indramat introduces its line of rugged, low cost, MKD digital AC servomotors. The line offers peak motor power up to 12 kW, with peak torques ranging from 4 to 102 Nm (35 to 9000 lb-in) and speeds up to 9,000 rpm. They are available in five frame sizes and are available with an option integral multi-turn absolute resolver feedback, eliminating the need for axis homing routines. They are rated IP65, making them ideal for use in harsh environments in packaging, material handling, converting and printing.

Circle 326

Vibration Monitor

Schenck Trebel introduces the Vibrocontrol 920, a single channel monitor, which the company says is flexible, dependable and provides maximum protection for motors, fans, pumps and other equipment critical to operations. It accepts virtually any type pickup, including velocity sensors and 2-, 3- or 4-wire accelerometers. A program provides password protection and allows pre-programming of limits for

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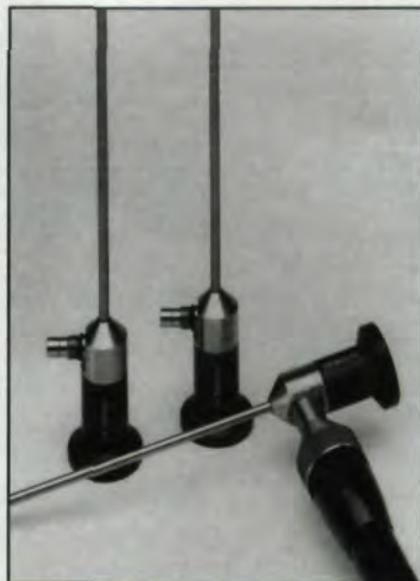
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Gears on Film

Gear Technology's bimonthly aberration — gear trivia, humor, weirdness and oddments for the edification and amusement of our readers. Contributions are welcome.

In our unceasing attempt to further educate our readers—and find new and creative ways to waste time at work—the Addendum staff has spent many long hours (and many dollars on popcorn) to bring you our latest research on gears in film.

We'll be assigning ratings (1 gear = pretty awful; 4 gears = terrific) to the movies based on the following qualities: impressiveness of the gears, relevance to the plot, prominence in the film, star quality and dramatic interpretation.

Modern Times (1936). Our nominee in the Classic Gear Movie category is Charlie Chaplin's last film without dialogue (or almost without it anyway), and may be one of his finest. In it Chaplin plays a hapless victim of modern factory life, while a very young Paulette Goddard plays his love interest, known only as "The Gamin."

The plot, which might have been co-written by Charles Dickens, Victor Hugo, Scott Adams and the Monty Python gang, is a darkly comedic look at the Depression-era struggles of ordinary people trying to survive in an industrialized society.

We're sorry to say that the gears play metaphorical villains, but they're nasty in the grand tradition of movie bad guys. If not quite as evil as Olivier's Richard III or as funny as Alan Rickman's Sheriff of Nottingham, they make worthy symbolic opponents, and they're considerably more obvious as symbols than Charles Foster Kane's Rosebud. They're also very sexy, as gears go, and they film wonderfully in black-and-white.

Our only quibble is that in a couple of crucial scenes, some of the gears are

running backwards. But then maybe it's not fair to expect someone to be both a directorial genius and a gear engineer. Rating: **●●●●**.

The Rock (1996). An action/adventure flick with Nicolas Cage as an FBI biochemical weapons specialist and Sean Connery as the only man ever to have escaped from Alcatraz.

The gears—or in this case, gear segments—come into play after terrorists steal some chemical weapons and take over "The Rock." Connery, Cage and a small band of Navy SEALS must sneak into Alcatraz, disarm the weapons and save San Francisco from total destruction.

At a crucial point in the plot, Connery must roll underneath a series of giant pendulums with gear teeth on their bottoms while avoiding spouts of flame shooting up from the floor. We're not entirely sure what this contraption is supposed to be. The gear teeth don't

appear to mesh with anything, and we don't know why flames are shooting up from the floor, but it's really cool and scary-looking. Rating: **●●●●**.

The Metaphysics of Gears

To answer the question, what is a real gear, we have consulted no less an authority than Eliot K. Buckingham. Mr. Buckingham comes down on the side of the stationary objects. He says, "... to my mind, a single gear is a piece of metal with projections on it. A gear is designed to be operated with another gear or gears. You do not design a single gear ...

"If a gear has to be moving to be a gear, what are all those things in planetaries, and often differentials, that don't move, but are absolutely necessary to proper performance, and have all the appearance of being gears, with teeth and all?"

He approaches the "Biggest Gear in the World Question" using the same logic: "Actually, the largest gear in the world is a cog railroad, since the rail is a rack, which is a segment of a gear of infinite diameter."

Since no discussion of either philosophy or movies is complete without a dissenting point of view, Addendum is waiting for yours. If you have nominations for our Gear Movie Hall of Fame or another philosophical viewpoint on the ontology of gears, let us know. We have a new referee's whistle we'd love to try out. **●**



The Addendometer: If you've read this far on the page and enjoyed it, please circle 225.

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