

GEAR TECHNOLOGY

The Journal of Gear Manufacturing

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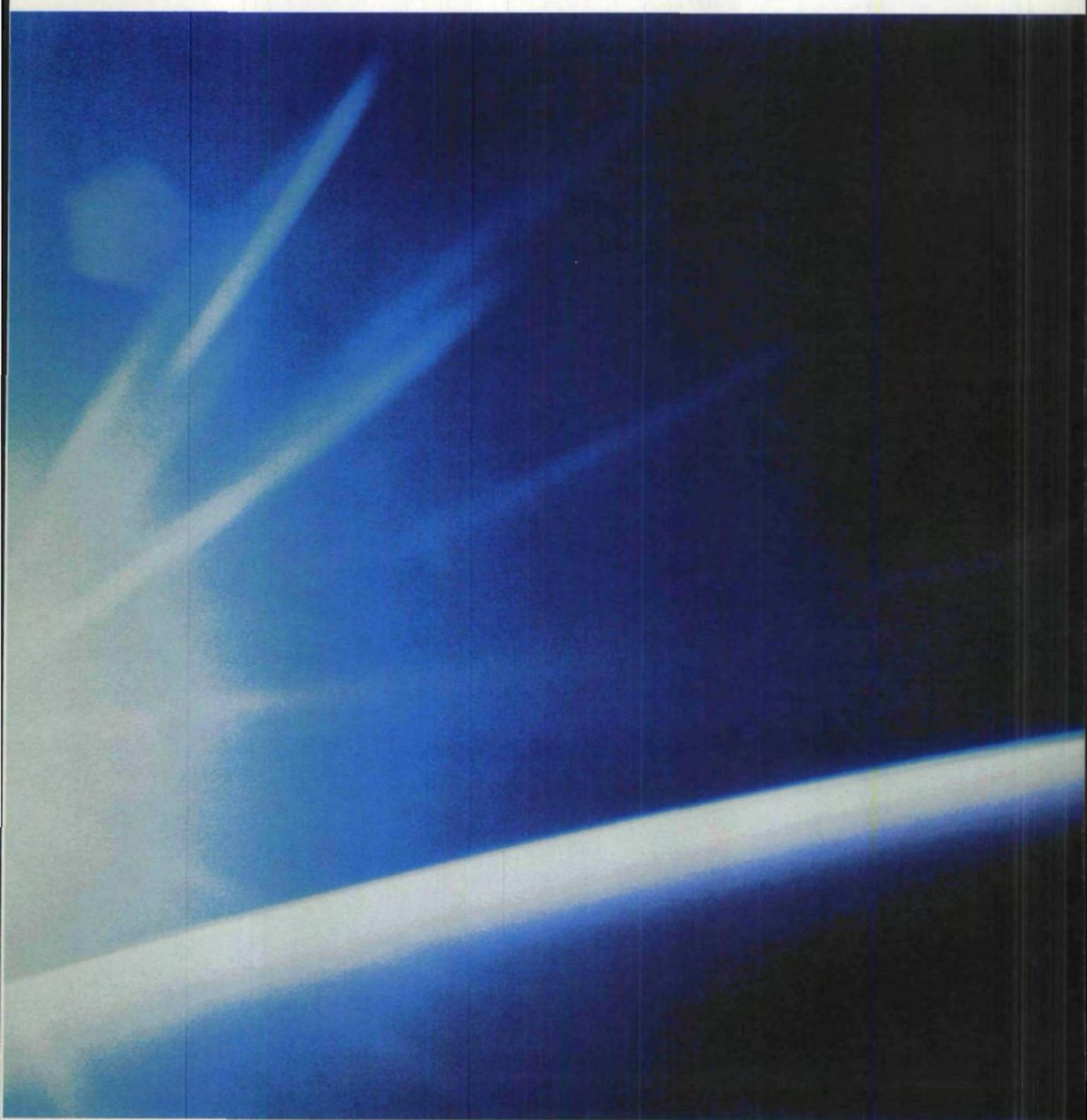
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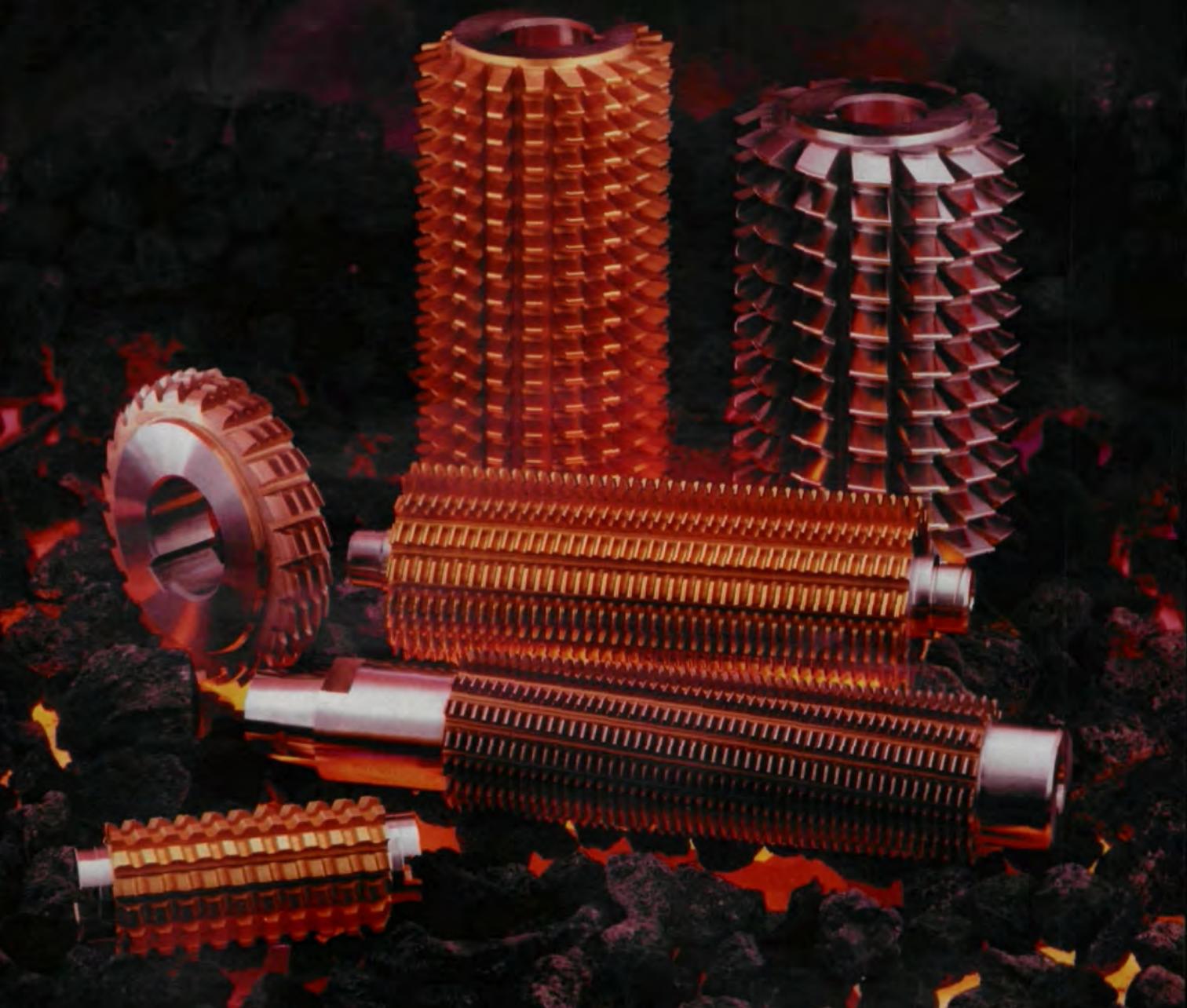
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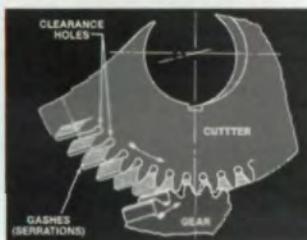
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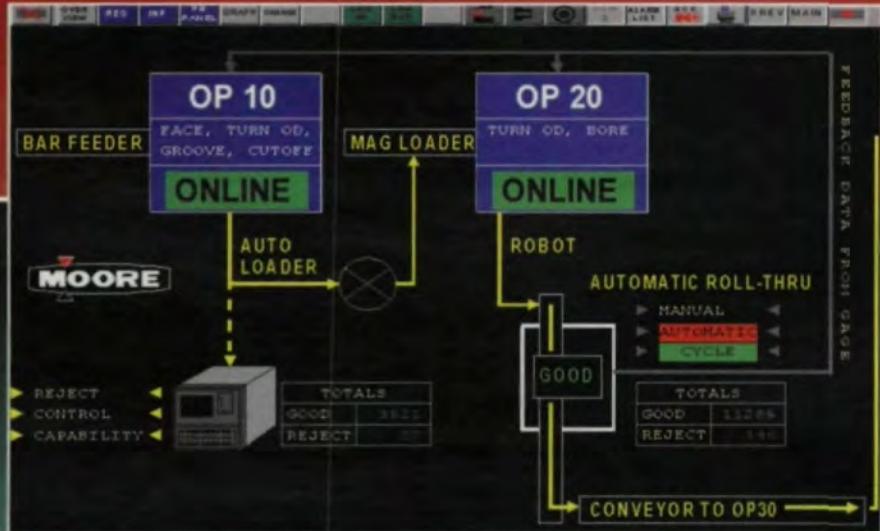
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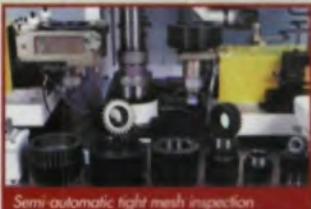
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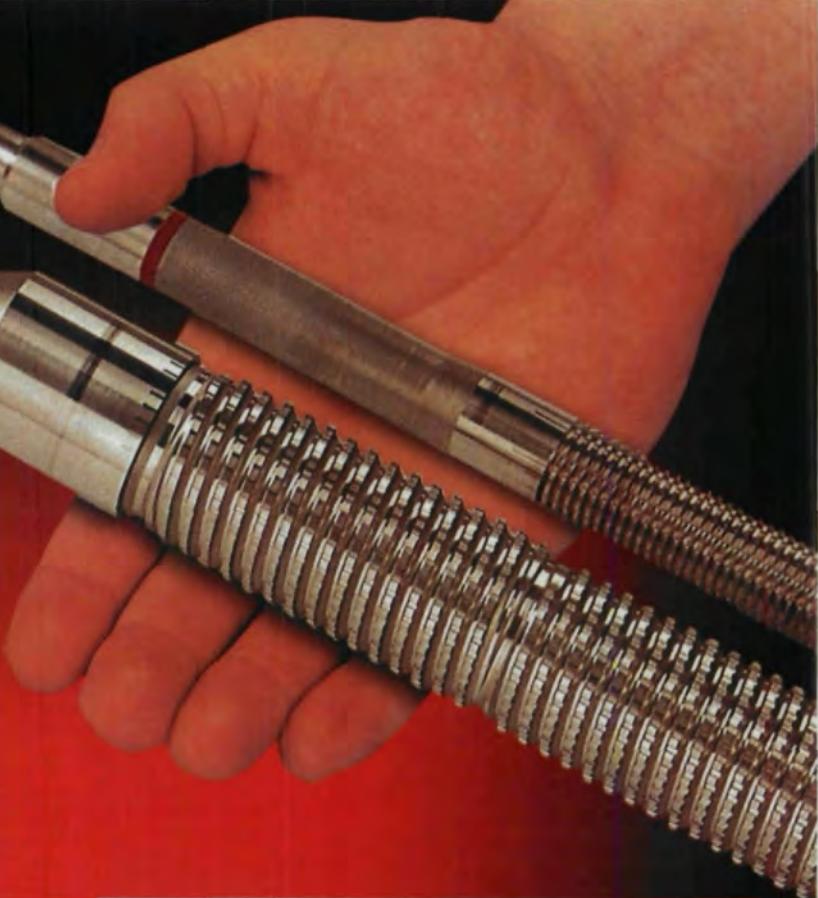
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Good-Bye, Dad

Harold Goldstein, 1917–1997

I sat down to write this editorial about my father, Harold Goldstein, as he approached his 80th birthday in October. I had meant it to be a celebration of his nearly 65 years in the machine tool business. Unfortunately, on August 26, as I was working on it, my father passed away after a long battle with emphysema. This editorial has now become a memorial as well as a celebration.

In many ways, my father's story was that of his generation. He entered his teenage years at the beginning of the Depression and spent his young manhood in a world shattered by war. He had to leave high school in his second year to earn money to help support his family and never knew the easy security that comes from having (or at least believing one has) a guaranteed lock on one's fair share of the good things in life.

But these early experiences strengthened him. Along the way, he made sure his own children had some of the important things he'd missed in the formative stages of his life; not so much material things, although he took care of that as well, but a strong sense of the importance of family, togetherness, love and caring.

He was self-taught. He turned himself into a very well-read, articulate individual, and his knowledge of accounting, business law, sales and marketing came on the job. In 1950, he struck out on his own from the business he ran with his father and founded Cadillac Machinery.

Dad also earned the trust and respect of his colleagues. Along with his father, he was one of the founding members of the Machinery Dealers National Association (MDNA) and became its national president in 1967-8. Later, in 1971 he was awarded the organization's Randolph K. Vinson Award for outstanding contributions to the industry. But he was particularly proud that he, with no formal education, was selected to represent the machine tool industry and the MDNA to give testimony before the House Ways and Means Commission with respect to the Investment Tax Credit.

He placed a tremendous importance on education as a tool to help us move through our lives, and he always stressed that importance to his children.

And it wasn't just "book learning" he impressed on my brothers and sister and me. In spite of all his early disadvantages and the hardships he faced during his formative years, there were certain admirable personal truths he lived out and taught his children, lessons which have helped to give my life some focus and direction...

. . . Your Word Is Your Bond. . . Be Scrupulously Honest. . . Don't Be Just A Taker In Life; Give Back As Well. . . It's Easy to Write a Check to a Charity; It's Harder, But More Useful, to Give Your Time, Experience and Talent. . . Fight For What You Believe and Stand Up For What You Think Is Right, Even If It's Not Popular. . . You Can't Be Successful If You Work Only 40 Hours a Week. . . Your Company Doesn't Pay Your Salary; Your Customers Do. Without Them, You Don't Have A Job or A Business. . .

To help his children to have a wider vision of any given situation, my dad would constantly tell us, "You don't know what you don't know."

Throughout my life, I have found this last statement to be particularly insightful. It's taught me to look beneath the surface of situations; to assume that, most of the time, there's more going on than first meets the eye; that things are generally deeper and more complex than they first appear. It's helped me to avoid making superficial judgments, not to be too cocky too early in the game and to do my homework.



Harold and his wife, Susan.

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Working with and for my dad, I learned about industriousness, leadership, tenacity, ambition, self-confidence and perseverance. Dad could be a tough boss, but he was a fair one, and I was fortunate to have mostly his praise and admiration as I went through my own career.

He provided a tower of strength for our companies, Cadillac Machinery and Randall Publishing. Even after he was no longer strong enough to come into the office, he had a seemingly inexhaustible supply of interest and enthusiasm for the business. I spoke to him nearly every day, and he always had the same questions: What did we buy today? What did we sell? What new projects were we working on?

And he had the same kind of interest and concern for the larger industry and for both our immediate and extended families. He was a patriarch in the truest and best sense of the word.

The end of his life, like the beginning, was not easy, but even when he was quite ill, he continued to teach us by example. He put his affairs in order quietly and efficiently so his family would be spared the burden of tying up the loose ends. He called those close to him together to say his good-byes, an act of closure that's been deeply meaningful to me these past few weeks. He met his end with a courage, grace and dignity that made me even prouder to be his son. His job was done, he was rightfully proud of what he accomplished, and he went in peace.

Once this summer, reflecting on the number of his family and friends throughout the world who called or came to visit with him, he said, "I guess I did something right."

Dad, you did so many, many things right. We're going to miss you.



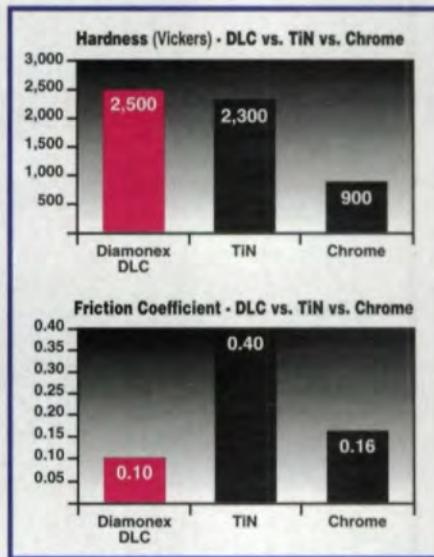
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INDUSTRY NEWS

Rock Valley Apprenticeship Program To Graduate First Class

The first group of seven students will complete their training in the Rock Valley College Manufacturing Youth Apprenticeship Program next spring. Upon graduation, they will have earned their Associate of Arts degrees from Rock Valley College or their journeyman's card from the Rockford Tooling and Machine Association.

The Rock Valley Apprenticeship Program is part of the nationwide Tech Prep program. It is modeled on the German apprenticeship program, which combines academic study with on-the-job training.

Students begin their training in their junior year of high school. The program is a combination of classroom and on-the-job training, including an extensive summer school program between the junior and senior high school years. After com-

pleting high school, students go on to a four-year apprenticeship program.

The apprenticeship training facility is located at the Pfauter-Maag Cutting Tools facility in Loves Park, IL, and Pfauter-Maag was one of the original sponsoring companies of the program.

Twenty-eight manufacturing companies in the Rock Valley/Rockford area are involved. Since 1993, some 140 students have participated in the program, which boasts a 70% retention rate.

M & M Precision Systems Acquires New Product Line

M & M Precision Systems Corp., manufacturer of gear inspection systems, has acquired the product lines of Apeiron, Inc. of Bloomington, MN. M & M will manufacture these laser dimensional measurement systems and market them worldwide under the M & M name. These non-contact laser measurement systems can accurately and rapidly identify dimensions on surfaces that cannot be measured by traditional contact methods.

Bison Gear Opens New Facility

Bison Gear and Engineering has officially opened its new world headquarters and gear motor manufacturing plant in St. Charles, IL. The 115,000 sq. ft. facility on 9.7 acres brings all the Bison operations under one roof.

The new building, designed and built to Bison's specifications, houses administration, finance, sales and marketing, research and development, warehousing and manufacturing. Special amenities include a gear technology center, a fitness center for employees and training facilities for professional and personal advancement. It has high technology equipment for hobbing, machining, gear inspection and assembly and testing.

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Capitalizing on Your Human Capital

Skill levels, productivity and labor availability all affect your bottom line.

Dr. Michael D. Bradley

A fundamental characteristic of the gear industry is that it is capital intensive. In the last decade, the gear manufacturing industry has been undergoing an intense drive toward improving and modernizing its capital equipment base. The Department of Commerce reports that annual sales of gear cutting equipment have increased nearly 60% since 1990. While this effort has paid off in increased competitiveness for the American gear industry, it is important to remember that there is another capital crucial to manufacturing success—"human capital."

Human capital is the set of skills, knowledge and abilities that makes an individual productive. The higher an individual's skill level, the more productive he will be and the more he will earn. This is exactly parallel to a new machine generating a higher rate of return than an older, less productive machine. Human capital is generally acquired through education and training. An engineer, for example, dramatically increases his or her human capital by going to college.

A gear manufacturer's human capital stock is mea-

sured by adding together the individual human capital of all its workers. Just as the total productive capacity of the physical capital stock is measured by adding up the physical capacities of the individual pieces of equipment, so too is the human capital stock measured.

Unfortunately, this sometimes doesn't get done. For one reason, acquisition of human capital doesn't typically require the outlay of a single huge pile of cash; a gear company makes payments gradually to workers through time. These gradual payments take away a natural point of focus in analyzing the human capital stock.

Another reason the human capital stock is less closely monitored may be that the state of human capital is more difficult to assess than that of machinery. Finding standards that measure and describe the status of human capital in an industry is often hard.

Fortunately, this latter problem is being remedied in the gear industry. The American Gear Manufacturers Association annually produces a comprehensive study of the state of human capital in the gear industry, called "Wage and Benefit Survey."

This survey provides insight

into the three important aspects of human capital stock which gear manufacturers should be monitoring. These are the expense of hiring the labor, the training and skill level of the labor force and the availability of skilled labor, both in the present and future.

The expense of hiring labor shows up in the quarterly bottom line, and it is this aspect of human capital that gets the most attention. According to the AGMA study, the average hourly wage paid to a direct worker in the gear industry is \$12.65. Adding average hourly benefits of \$7.20 per hour gives an average total

hourly compensation of \$19.85, or an average cost of \$40,000 per year or \$1.2 million during the worker's potential employment. Moreover, this represents the average direct employee's wages, including both low and high skilled employees. When just skilled workers, like tool makers or CNC machinists are considered, the lifetime compensation cost can climb to more than \$1.5 million. Viewed in this way, it is clear that gear manufacturers make a substantial investment in their workers.

The average gear manu-

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facturer is small—less than half have more than 100 direct workers—but even with just 100 employees, the annual cost of compensation can exceed \$4 million. Moreover, this sum does not include additional indirect labor costs like training, administration and other non-direct human resource activities. It also does not include selling costs, engineering costs or management costs. In addition, compensation is even higher at unionized gear manufacturers, with between one quarter

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and one third of gear firms being unionized. Compensation is about 30% higher at unionized firms, so the compensation cost at a unionized, 100-worker gear company can exceed \$5 million a year.

Given the size of these costs, it is important for gear manufacturers to control their growth. One area in which they have been successful is in health care costs. The AGMA study shows that, after years of rapid growth, the annual average health care cost per employee has grown little in recent years. In fact, annual employee health care cost has grown by only 3% over the last two years, a rate that is less than that of inflation. Gear firms have achieved this success by aggressively pursuing cost-saving strategies, such as by switching to managed care, switching carriers, increasing employee contributions to premiums and increasing deductibles.

Worker's compensation is another example. After several years of sharp increase in premiums, about half of gear firms have undertaken safety plans that reduce accidents. This has two benefits: It reduces worker's compensation premiums, and it reduces the lost productive output from injured workers. The point is, when a human capital issue comes to the attention of gear manufacturers, they can take successful steps to address it.

The worker's compensation issue also helps to reveal the dual nature of the human capital issue for gear manufacturers. While the level of compensation is obviously important, it is only half of the human capital story.

High wages by themselves are not necessarily a burden for a firm. In fact, some firms that pay the highest wages are the most profitable.

The other half of the human capital story is the productivity of the labor. The higher the human capital content of the labor force, the greater its skills and abilities, and the more productive it will be. A useful summary of the important relationship between a firm's compensation cost and the productivity of its labor is given by a measure called "unit labor costs." Like the internal rate of return to physical capital, this is a measure that helps a gear firm figure out how well it is managing its labor force.

The unit labor cost measure recognizes the two parts of labor costs. It accounts for both the rate of compensation to workers and the amount of labor required to produce output. In this sense, it is the mirror image of productivity. When productivity rises, output-per-labor-hour rises. When productivity rises, the labor hours required to produce a single unit of output falls. This mirror image of productivity is called the labor content of output, and it falls as productivity rises.

Unit labor cost is derived by multiplying this measure of labor content by the rate of average hourly compensation, and is, therefore, a dollar measure of the labor cost of producing a unit of output. When unit labor costs are falling, productivity is rising faster than wages, indicating that the gear manufacturer is doing a good job managing its human capital. Falling

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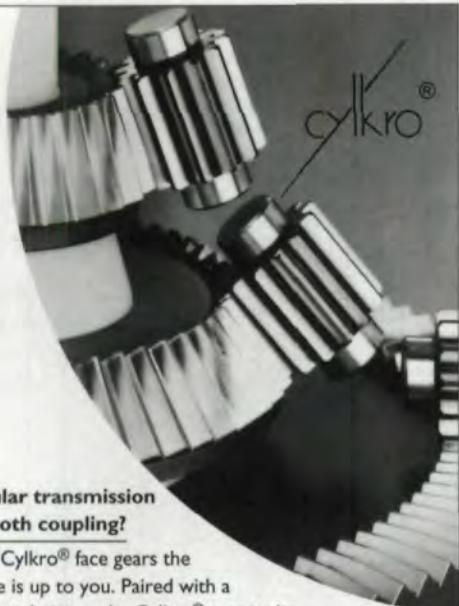


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CIRCLE 126

THE GEAR BUSINESS

unit labor costs also help profitability because declining unit labor costs mean that profits will rise without an increase in prices. This is crucial during a period of intense competition.

While unit labor costs measure how quickly labor productivity is rising relative to compensation, it tells us nothing about efforts to improve labor productivity. Even in an economy with modest inflation, wages tend to rise every year, and without an increase in productivity, higher wages mean higher unit labor costs and lower profitability. Therefore gear manufacturers must try to continuously improve the productivity of their work force.

The primary way gear manufacturers accomplish this for direct workers is through training. While there are some bright spots, this is an area in which the American gear industry is not particularly strong. For example, less than a quarter of gear manufacturers have apprenticeship programs. These programs are the fundamental way in which relatively new workers can rapidly increase their productivity through organized programs of skill transfer. This lack of apprenticeship programs stands in marked contrast to gear industries in other countries that tend to have well-established and successful apprenticeship programs.

It is true that several gear manufacturers have started partnerships with local community colleges. These programs include donations of old equipment, the establishment of scholarships for studying gear manufacturing

and the creation of coordinate work/study programs. Unfortunately, these programs are still the exception rather than the rule.

Gear manufacturers have begun to offer incentives for workers to get skills and become more productive. For example, the AGMA study reveals over the last three years a dramatic increase in the number of gear firms that "pay for knowledge." In 1994, less than 10% of the gear firms offered this incentive plan, but by 1996 more than 25% were offering it. Pay-for-knowledge programs provide financial compensation for the acquisition of additional skills. For example, some gear firms pay a premium to workers who can operate multiple machines. To be effective, this premium must be substantial, and it is averaging about 85 cents per hour among the gear manufacturers that use them.

Another incentive for workers to increase their productivity is through profit-sharing plans. In these plans, a worker's total compensation is linked to the performance of the firm. Usually, the firm's contribution to the worker's pension program depends upon firm performance, but 17% of

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THE GEAR BUSINESS

gear manufacturers have profit-sharing programs in which workers' current pay depends upon current profits.

Of course, no incentive plan will work unless the gear manufacturer has the employees to work. The third important aspect of human capital in the gear industry is the availability of skilled workers. Given the rapid economic expansion in the gear industry in the last five years and the paucity of training programs, it is not surprising that many gear firms are having difficulty finding and hiring skilled workers. Some gear firms have reported that a shortage of skilled labor is currently limiting their capacity to produce. In other words, these firms have the machinery available to expand production, but simply cannot find the additional skilled workers to run the equipment.

The AGMA study tracks labor scarcity, and this problem has clearly become more severe in recent years. As recently as 1994, over a quarter of gear firms reported that grinder machinists were readily available, but by 1996, this percentage has fallen to just over 11%. Similarly 93% of gear companies reported that in 1996, toolmakers were scarce and difficult to hire.

This problem is unlikely to improve as time passes. The industry work force is relatively old, and as older skilled workers retire, finding the new workers to replace them will be difficult. Forty-three percent of gear manufacturing workers are more than 45 years old, and 82% are more than 30 years old. In an industry where a

current shortage of skilled labor already exists, this age profile foreshadows a continuing problem over the next two decades. Tight labor markets imply rising wages that will drive up unit labor costs. Unless productivity rises continuously, the labor shortage could provide an ongoing drag on the industry's profitability.

The American gear industry has made impressive strides in the last ten years to recapitalize itself and become world-class. However, not forgetting the "other" capital, human capital, is important. Labor costs remain a substantial part of gear firms' total costs, and the pressure to improve labor productivity continues. When we combine these factors with the current, and probable future shortages of skilled labor, the human capital dimension of gear manufacturing presents a persistent challenge for the future. ◊

Michael D. Bradley

is Professor of Economics at the George Washington University in Washington, D.C. He has been a consultant to the gear industry for twelve years, and in 1996 he won AGMA's Executive Committee Award for "his efforts to enhance the art of management in the gear industry."

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VIEWPOINT

Cyclo System Also New Technology

As always, I enjoyed reading your magazine. It was interesting and enjoyable to read your article about Mr. E. K. Buckingham, who I highly regard as an exceptional authority in the field of gearing in the U.S. His views sometimes do not conform with mainstream practices, opinions and standards as represented by AGMA. I strongly believe it is important to have individuals like him to avoid viewing things too one-sidedly.

I was somewhat disappointed that, according to your article, Mr. Buckingham says "only two new technologies come directly from the gear industry in the last 50 years," namely the Spiroid system and Novikov-Wildhaber gearing.

These two developments are certainly significant. However, I feel that the CYCLO gear system is a much more important new technology. Next to the numerous unique technical and practical advantages of this gear system, no other could achieve a real, economic success in the last 50 years. The CYCLO system, however, became the backbone of close to a billion-dollar gearbox/gear motor industry and is the only significant competitive system to classical involute spur/helical gears.

It is also odd that AGMA is not interested in devoting attention to this system. It seems to me sometimes that the classical gear manufacturers hope: "If we ignore the CYCLO system, it will go away." However, the CYCLO system is being continuously updated, refined and is gaining market share worldwide.

Gerhard Antony, PhD.
Vice President,
Sumitomo Machinery Corp. of America

The Kish Hunting Mesh Method

The Kish method for determination of hunting mesh, (Vol. 14, No.4) looks remarkably like Euclid's algorithm for finding the greatest common divisor of two numbers. Euclid invented his algorithm some 2,300 or so years ago, and here it is in your latest issue, still being useful.

Jules Kish is an estimable engineer, and I am more than glad to call it, as you do, the Kish method, but I think that Euclid deserves at least a nod and, from me, a wink when I do so.

Ron Mosier
Applied Mathematician
Chrysler Corp.

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Gear Crack Propagation Investigations

David G. Lewicki and Roberto Ballarini

Introduction

A common design goal for gears in helicopter or turboprop power transmissions is reduced weight. To help meet this goal, some gear designs use thin rims. Rims that are too thin, however, may lead to bending fatigue problems and cracks. The most common methods of gear design and analysis are based on standards published by the American Gear Manufacturers Association. Included in the standards are rating formulas for gear tooth bending to prevent crack initiation (Ref. 1). These standards can include the effect of rim thickness on tooth bending fatigue (Ref. 2). The standards, however, do not indicate the crack propagation path or the remaining life once a crack has started. Fracture mechanics has developed into a useful discipline for predicting strength and life of cracked structures.

Ahmad and Loo (Ref. 3) applied fracture mechanics to gear teeth to illustrate the procedure and estimate crack propagation direction. Honda and Conway (Ref. 4) also applied fracture mechanics to simulate tooth crack propagation, compute threshold loads and calculate tooth life. Flaske and Jezernik (Ref. 5) applied fracture mechanics to gear teeth to estimate stress intensity factors and gear life. Researchers at Tohoku University in Japan performed a series of analyses and experiments to determine the effect of residual stress on crack initiation and propagation (Refs. 6, 7). Also, Daniewicz et al. (Ref. 8) developed a comprehensive, self-contained analysis package to refine the spur gear bending fatigue theory using fracture mechanics. Lastly, Flaske and Pehan (Ref. 9) described their method for calculating crack propagation in gear teeth using fracture mechanics. Much of the work of the above references considered only an initial crack, and propagation paths were not considered. Many of the references that did consider crack propagation assumed the propagation occurred in a straight path. In addition, experimental validation of the cited analyses was sparse. Finally, no work using fracture

mechanics was performed for thin-rim gears.

The objective of this study was to determine the effect of gear rim thickness on crack propagation life. From an extensive study (Ref. 10), linear elastic fracture mechanics was used to analyze gear tooth bending fatigue in standard and thin-rimmed gears. Finite element computer programs were used to determine stress distributions, estimate stress intensity factors and model crack propagation. Various fatigue crack growth models were used to estimate crack propagation life. Experimental tests were performed to validate predicted crack propagation results.

Fatigue Crack Growth

Many machine elements, such as gear teeth, are cyclically loaded in application. The overall fatigue life of such components may be represented by three distinct phases: 1) crack initiation, 2) crack propagation and 3) final failure. Once crack initiation has occurred, fracture mechanics may be used to estimate crack propagation fatigue growth rate and time to final failure.

The most universally used method to calculate crack propagation crack growth was postulated by Paris and Erdogan (Ref. 11). Purely Mode I loaded specimens subjected to cyclic load were considered. Unstable crack growth such that the stress intensity factor grew with increasing crack size was also considered. Paris postulated that the rate of crack growth with respect to number of stress cycles was a logarithmic relationship with the stress intensity factor range as

$$\frac{da}{dN} = C(\Delta K)^n \quad (1)$$

where da is the change in crack length for dN number of stress cycles, ΔK is the range of the Mode I stress intensity factor at a given time and C and n are material constants. The material constants C and n must be determined by some experimental means.

Further research of fatigue crack growth has shown three important factors not considered in the Paris model. First was the

effect of load ratio R on crack growth ($R =$ minimum cyclic load/maximum cyclic load). Second was the instability of crack growth observed when the stress intensity factor range approached the material's fracture toughness index, K_{IC} . Third was the presence of a stress intensity threshold factor ΔK_{th} . The stress intensity threshold factor is the highest stress intensity factor in which no crack growth would occur. The Collipriest crack growth model (Ref. 12) accounts for these effects where

$$\frac{da}{dN} = C(K_{IC}\Delta K_{th})^{n/2} \cdot$$

$$\exp \left\{ \ln \left(\frac{K_{IC}}{\Delta K_{th}} \right)^{n/2} \cdot \tanh^{-1} \left[\frac{\ln \left(\frac{\Delta K^2}{(1-R)K_{IC}\Delta K_{th}} \right)}{\ln \left(\frac{(1-R)K_{IC}}{\Delta K_{th}} \right)} \right] \right\} \quad (2)$$

In addressing applications to gears, Inoue et al. (Ref. 7) describe fatigue crack growth of gear bending fatigue tests. Here, crack growth equations were derived as a function of crack depth through a gear tooth. The expression derived for crack growth rate da/dN , as a function of stress intensity range ΔK was

$$\frac{da}{dN} = \begin{cases} \frac{\lambda}{(1-\alpha^n)} (\Delta K^n - \Delta K_{th}^n) & \text{for } \Delta K_{th} \leq \Delta K \leq \Delta K_C \\ \frac{\lambda}{(1-\alpha^n)} \frac{\Delta K^n K_{IC}^{-n}}{(K_{IC}^{-n} - \Delta K^n)} & \text{for } \Delta K_C < \Delta K < \Delta K_{IC} \end{cases} \quad (3)$$

where the parameters K_{IC} , α , ΔK_C , ΔK_{th} , η and λ were all estimated as a function of tooth hardness (Ref. 7).

Crack Propagation Simulation

The analysis of the current study used the FRANC (Fracture Analysis Code) computer program described by Wawrzynek (Ref. 13). FRANC is a general purpose finite element code for the static analysis of cracked structures. FRANC is designed for two-dimensional problems and is capable of analyzing plane strain, plane stress or axisymmetric problems.

Among the variety of capabilities, a unique feature of FRANC is the ability to

model a crack in a structure. FRANC uses a method called "delete and fill" to accomplish this. To illustrate, the user would first define an initial crack by identifying the node of the crack mouth and coordinates of the crack tip. FRANC will then delete the elements in the vicinity of the crack tip. FRANC will next insert a rosette of quarter-point, six-node triangular elements around the crack tip to model the inverse square-root stress singularity (Refs. 14, 15). Finally, FRANC will fill the remaining area between the rosette and original mesh with conventional six-node triangular elements. The user can then run the finite element equation solver to determine nodal displacements, forces, stresses and strains.

A further unique feature of FRANC is the automatic crack propagation capability. After an initial crack is inserted in a mesh, FRANC models a propagated crack as a number of straight line segments. For each segment, FRANC models the crack tip using a rosette of quarter-point elements. FRANC then solves the finite element equations, calculates the stress intensity factors and calculates the crack propagation angle. After the crack propagation angle is determined, FRANC then places the new crack tip at the calculated angle and at a user-defined crack increment length. The model is then remeshed using the "delete and fill" method described above. The procedure is repeated a specific number of times as specified by the user. In the current study, the stress intensity factors were determined from the calculated nodal displacements using the displacement correlation method (Ref. 16). The method of Erdogan and Sih (Ref. 17) was used in the current study to determine the crack propagation angle.

Once the stress intensity factors are determined for each segment, the predicted number of crack propagation cycles can be estimated using the fatigue crack growth models. Regardless of the model used, the crack growth rates da/dN , were of the form

$$\frac{da}{dN} = g(\Delta K) \quad (4)$$

where $g(\Delta K)$ is given by Eq. 1 for the Paris relationship, Eq. 2 for the Collipriest relationship or Eq. 3 for Inoue's method. The predicted number of crack propagation cycles for the i_{th} crack segment, N_p , was estimated by

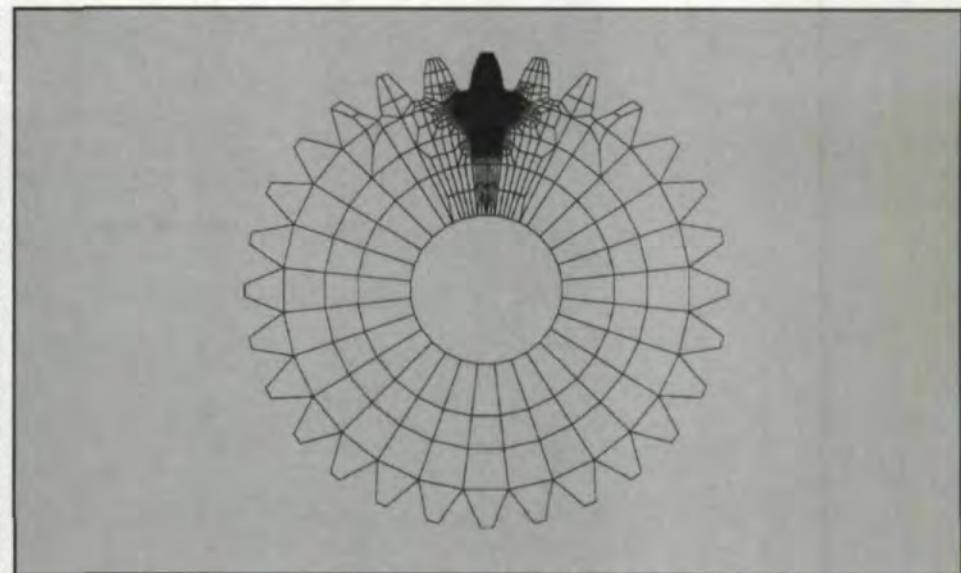


Fig. 1 — Finite element model of gears used in crack propagation studies, solid model, $m_B = 3.3$.

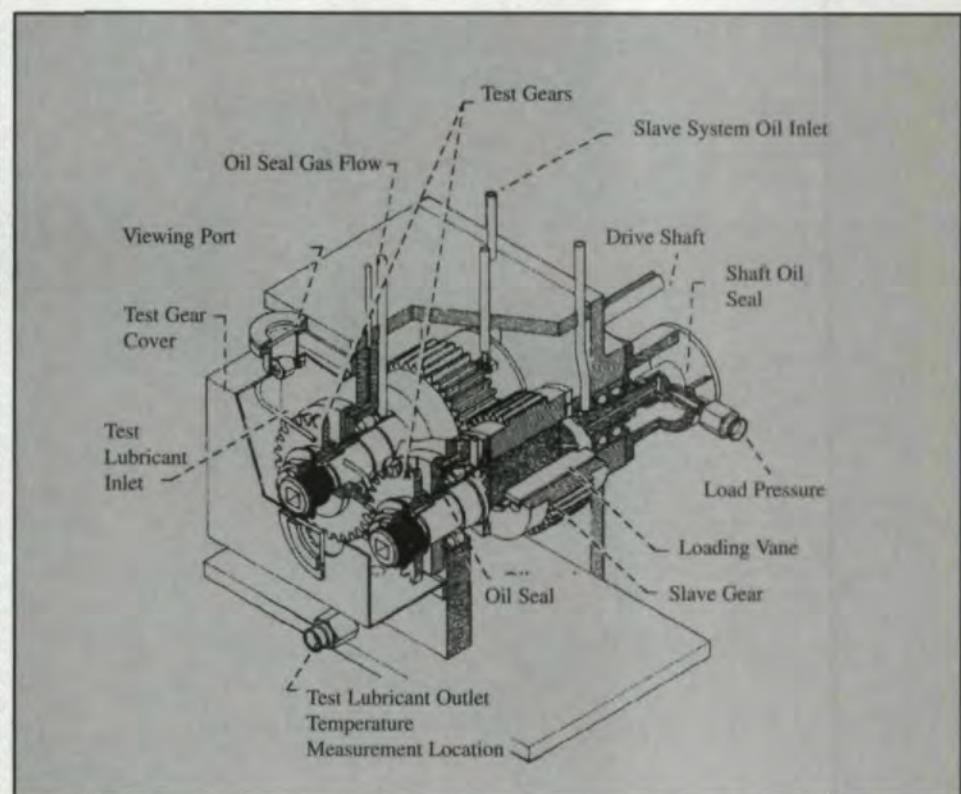


Fig. 2 — NASA Lewis Spur Gear Fatigue Rig.

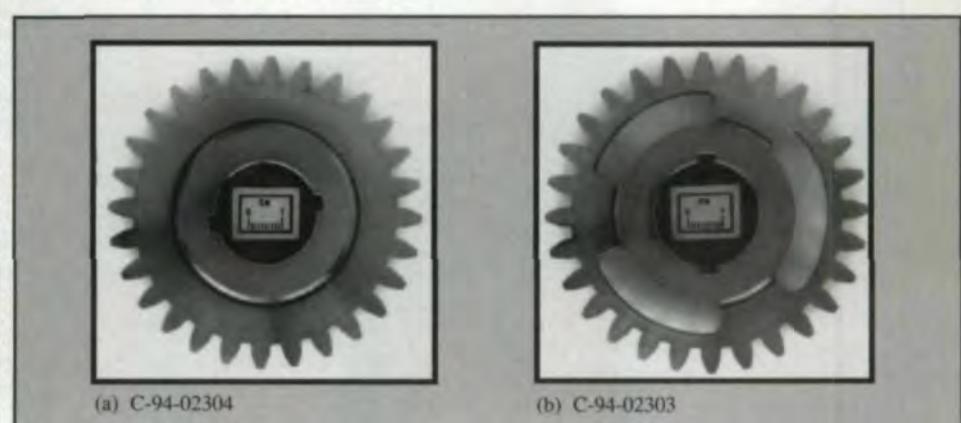


Fig. 3 — Test gears used to determine effect of rim thickness on crack propagation.
(a) $m_B = 3.3$. (b) $m_B = 0.3$.

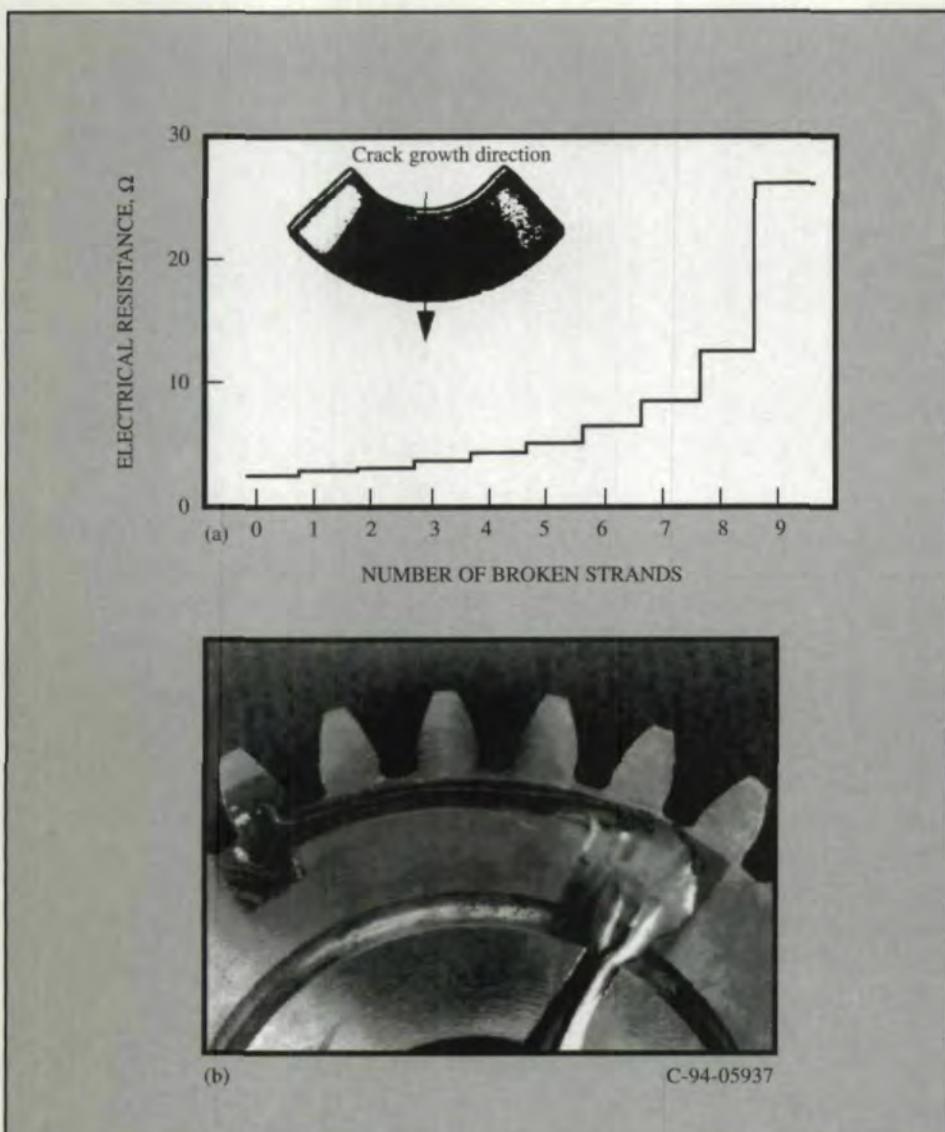


Fig. 4 — Specialized crack propagation gages for gear tooth crack growth measurements. (a) Increase in gage electrical resistance as the number of broken strands increases. (b) Installation of crack propagation gage on test gear.

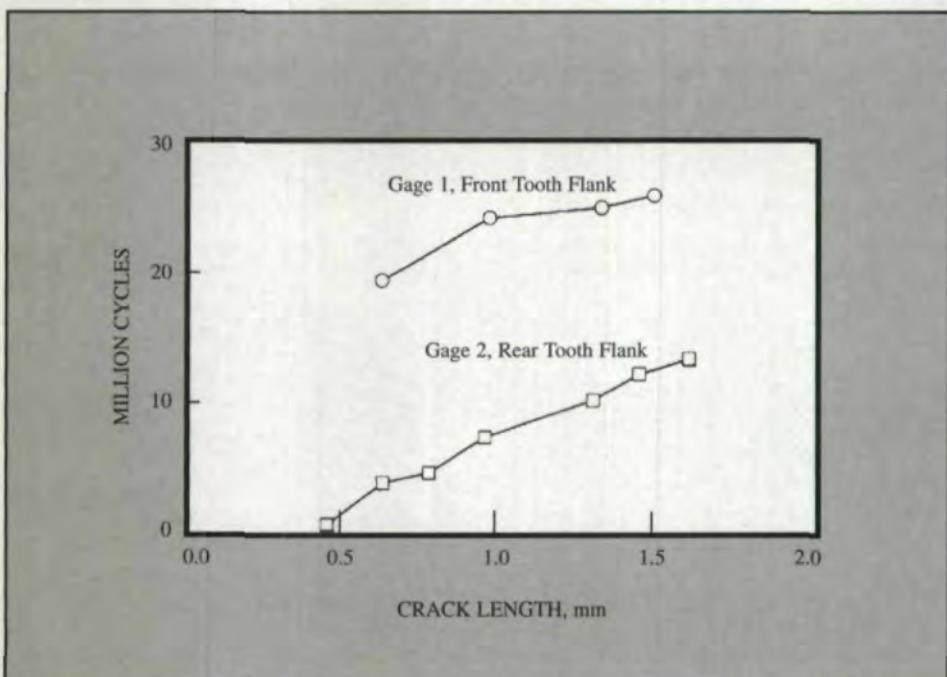


Fig. 5 — Crack propagation fatigue growth for Test 1, $m_B = 0.3$.

$$N_i = \frac{a_i - a_{i-1}}{g(\Delta K_i)} + N_{i-1} \quad (5)$$

where a_i was the crack length of the i_{th} segment, a_{i-1} was the crack length of the $(i-1)_{th}$ segment, N_{i-1} was the number of cycles of the $(i-1)_{th}$ segment and $g(\Delta K_i)$ was the average crack growth rate of the i_{th} and $(i-1)_{th}$ segments. Note that a_1 was the initial crack length, and $N_1 = 0$ and i varied from 2 to the total number of segments.

Gear Finite Element Modeling

Basic gear tooth geometry data was input to a tooth coordinate generation computer program. The tooth coordinate generator program used the method of Hefeng et al. (Ref. 18) to determine the tooth coordinates. The output was tooth coordinate and rim coordinate data which defined a single tooth sector of a gear. This output was used by a commercially available pre- and post-processing finite element analysis software package (Ref. 19). This package created the finite element mesh of the complete gear. FRANC then used this mesh and performed crack propagation simulations.

Fig. 1 shows a sample finite element mesh of an uncracked gear. The tooth geometry used modeled that of the test gears of the NASA Lewis Spur Gear Fatigue Rig (described in the following section). The analysis used 8-node, plane stress, quadrilateral finite elements. The mesh was refined in the region of the loaded tooth for improved accuracy. The model of Fig. 1 had 2,353 elements and 7,295 nodes. Material properties used were that of AISI 9310 steel. The tooth load was placed at the highest point of single tooth contact. For boundary conditions, four hub nodes were fixed. In addition, gears with various rim thicknesses were modeled. The parameter describing the rim thickness was the backup ratio m_B , where

$$m_B = \frac{b}{h} \quad (6)$$

where b was the rim thickness, and h was the tooth whole depth. Gears with various backup ratios were modeled by incorporating slots in the model. All cases used the same finite element mesh for the loaded tooth.

Test Facility

Crack propagation experiments were performed in the NASA Lewis Spur Gear Fatigue Rig (Fig. 2). The test stand operated on a torque regenerative principle in which

torque was circulated in a loop of test gears and slave gears. Oil pressure was supplied to load vanes in one slave gear which displaced the gear with respect to its shaft. This produced a torque on the test gears, slave gears and connecting shafts proportional to the amount of applied oil pressure. A 19 KW (25 hp), variable-speed motor provided speed to the drive shaft using a belt and pulley. The lubricant used for the gears, bearings and loading systems was a synthetic paraffinic oil. The test gear lubricant was filtered through a 5-micron fiberglass filter.

Test Gears

The test gears were 28-tooth, 8-pitch, 20° pressure angle external spur gears with a face width of 6.35 mm (0.25"). The teeth had involute profiles with linear tip relief starting at the highest point of single tooth contact and ending at the tooth tip at an amount of 0.013 mm (0.0005"). All test gears used in the experiments were fabricated and machined from a single batch of material. The test gear material was vacuum-melted, consumable-electrode AISI 9310 steel. The gears were case carburized and ground. The teeth were hardened to a case hardness of R_c 61 and a core hardness of R_c 38. The effective case depth (depth at a hardness of R_c 50) was 0.81 mm (0.032"). Two different test gear designs were considered. The first was a thick-rimmed gear with a backup ratio of $m_B = 3.3$ (Fig. 3a). The second was a thin-rimmed gear which incorporated slots (Fig. 3b). The backup ratio of the thin-rimmed gear was $m_B = 0.3$.

It was believed that tooth bending fatigue cracks would be difficult to initiate based on the load capacity of the test rig. Due to this, notches were fabricated in the fillet region (loaded side) on one tooth of each of the test gears to promote crack initiation. The notches were fabricated using electrical discharge machining (EDM) with a 0.10 mm (0.004") diameter wire electrode. The nominal notch dimensions were 0.20 mm (0.008") in length and 0.13 mm (0.005") in width along the full face width of the tooth. The notches were located at the same location for both test gears. This location was at a radius of 40.49 mm (1.594") on the fillet, which was the position of the greatest tensile stress for the solid gear ($m_B = 3.30$). The notches produced a stress concentration factor of approximately three as determined using a finite element analysis.

Instrumentation

The standard test rig instrumentation monitored test gear speed, oil load pressure, test gear and slave gear oil pressure and oil temperatures. Also, overall test stand vibration was monitored using an accelerometer mounted on the top housing. In addition to the standard facility vibration sensor, an advanced vibration processing diagnostic system was installed in the test stand to help assist in crack detection. Crack propagation gages were used in the experiments to determine fatigue crack growth. Special gages were fabricated for installation in the tooth fillet region of the test gears. The gages had ten circular strands with an inner radius of 1.52 mm (0.060") and an outer radius of 3.05 mm (0.120") (Fig. 4). The strands were designed to break as the crack propagated through them, which in turn increased the electrical resistance of the gage (Fig. 4a). Fig. 4b shows the installation of a gage in the fillet region of a notched tooth. A gage was installed on each side of the tooth flank for each gear instrumented with crack gages. The electrical resistance of the crack gages was monitored along with the load cycle count to estimate cycles as a function of crack length. The information from the rotating crack gages was transferred through brush-type slip rings. Also, an infrared tach sensor was used to measure number of load cycles.

Measured Gear Fatigue Crack Growth

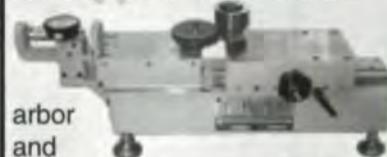
The thin-rimmed gear was used in Test 1. The test was run at 89 Nm (786 in/lb) torque and 10,000 rpm speed for 6.5 hrs., at which time rim fracture occurred. Fig. 5 plots the number of load cycles as a function of the measured crack length. The crack gage results indicated the crack growth was non-uniform throughout the tooth face width. A crack started on the rear flank of the tooth at the tip of the notch and reached an initial size of 0.46 mm (0.018") at 1,060,000 cycles. The crack continued to propagate through the rear flank, but did not reach the front flank until approximately 2,680,000 cycles. At 2,910,000 cycles, the crack reached a size of 0.64 mm (0.025") on the front flank, but completed propagation through the rear gage by this time. Even though the crack initiation time was not uniform throughout the tooth face width, the crack propagation rate was uniform. This was indicated by the similarity in slopes of the curves in Fig. 5 for Gages 1 and 2.

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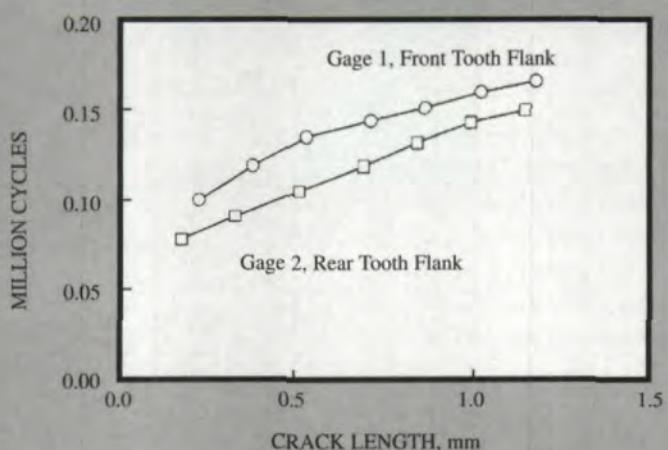


Fig. 6 — Crack propagation fatigue growth for Test 2, $m_B = 3.3$.

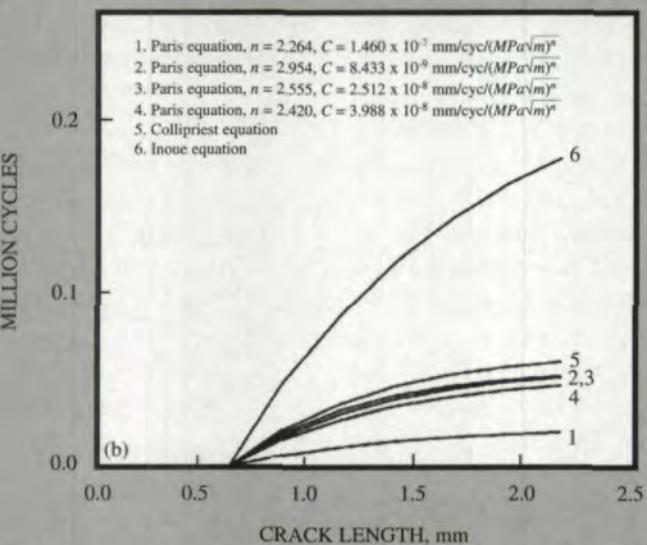
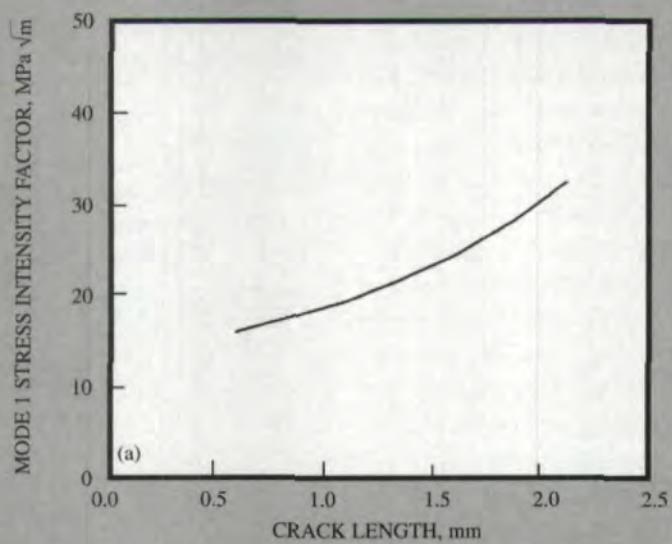


Fig. 7 — Comparison of predicted crack propagation cycles using Paris, Collipriest and Inoue equations. Model for $m_B = 0.3$. (a) Mode I stress intensity factor. (b) Life comparison.

The thick-rimmed gear was used in Test 2. This gear was run at 136 Nm (1200 in/lb) torque and 10,000 rpm speed for 15 minutes, at which time tooth fracture occurred. Fig. 6 gives the processed crack propagation results for Test 2. Note that the crack initiation and crack propagation was fairly uniform throughout the tooth face width for this test.

Comparison of Predicted and Measured Crack Growth

The FRANC computer program was used to simulate crack propagation and calculate Mode I stress intensity factors as a function of crack length. The predicted stress intensity factors were then used with three different fatigue crack growth models (Paris, Collipriest and Inoue) to estimate crack propagation.

A comparison of predicted crack propagation cycles using the Paris, Collipriest and Inoue methods is shown in Fig. 7. For this, the thin-rimmed model ($m_B = 0.3$) was used to simulate the test gear of Fig. 3b. An initial crack of 0.64 mm (0.025") was placed in the tooth fillet at the location of the maximum tensile stress. Crack propagation was then simulated, and the Mode I stress intensity factor as a function of crack length is given in Fig. 7a. From this, six different fatigue growth cases were considered. The first four cases used the Paris equation and material constants of AISI 9310 specimens from experiments of Au and Ke (Ref. 20). The fifth case used the Collipriest equation and AISI 9310 material constants from Forman and Hu (Ref. 21). The load ratio used was $R = 2.6$, as determined from the finite element analysis. The sixth case used Inoue's method and the material constants of the SCM 415 material (SCM 415 is a high-strength Japanese steel with properties similar to AISI 9310). The predicted number of cycles per crack length varied significantly among the cases studied (Fig. 7b). Note that the cycles were defined as the number of crack propagation cycles after an initial crack of 0.64 mm (0.025").

Predicted crack growth for the $m_B = 0.3$ and 3.3 gears was compared to the measured crack growth from the experiments. Again, the six different prediction schemes mentioned above were used. The predicted number of crack propagation cycles using the sixth schemes were, for the most part, extremely low compared to the measured number of cycles from the experiments. To

account for this, the concept of fatigue crack closure was investigated. Elber (Ref. 22) performed crack experiments on aluminum alloys and deduced that residual compressive stresses existed near the crack tip region because of plastic deformation. These residual stresses reduced the effective stress intensity factor range (and thus, increased crack propagation life) and provided a better fit to experimental data than other empirical expressions. Elber proposed an effective stress intensity range ratio U such that

$$\Delta K_{\text{eff}} = U(\Delta K) \quad (7)$$

where ΔK_{eff} was the effective stress intensity factor range. Elber then used the effective stress intensity factor range in the Paris fatigue crack growth model. In addition, Elber defined U through experimental studies as a linear function of the load ratio R .

The concept of fatigue crack closure was applied to the current gear crack experiments and predictions. A study was conducted to estimate the effective stress intensity factor range ratio for the experiments. The predicted number of crack propagation cycles using the same six schemes were plotted versus crack length at a variety of arbitrarily chosen U ratios. For the Paris equation and material constants $n = 2.954$ and $C = 8.433 \times 10^{-9} \text{ mm/cyc/(MPa}\sqrt{\text{m}})^n$, good correlation between predicted crack cycles and the experiments occurred when: 1) $U = 0.4$ for $R = 2.6$, and 2) $U = 0.8$ for $R = 0.1$. Assuming a linear relation between U and R produced

$$= 0.82 + 0.16(R) \quad (8)$$

Fig. 8 shows a sample comparison of predicted and measured crack growth when the fatigue crack closure concept was used. The cycles were defined as the number of crack propagation cycles after an initial crack of 0.64 mm (0.025"). It should be noted that good correlation was also achieved when the Collipriest equation was used with certain U values. This produced a relationship similar to Eq. 8, but with different coefficients (Ref. 10).

Fig. 9 displays the effect of rim thickness on predicted Mode I stress intensity factors and predicted crack propagation cycles. The stress intensity factors were determined from FRANC using the appropriate finite

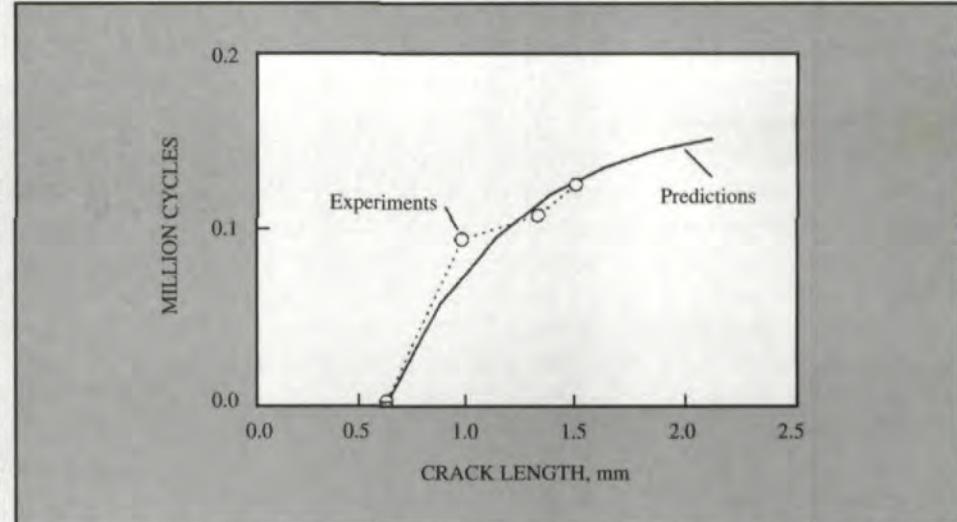


Fig. 8 — Comparison of predicted crack propagation cycles to experiments. Paris fatigue crack growth model, $n = 2.954$, $C = 8.433 \times 10^{-9} \text{ mm/cyc/(MPa}\sqrt{\text{m}})^n$, $R = -2.6$, $U = 0.4$, used for predictions. Test 1, Gage 1, front flank, for experiments.

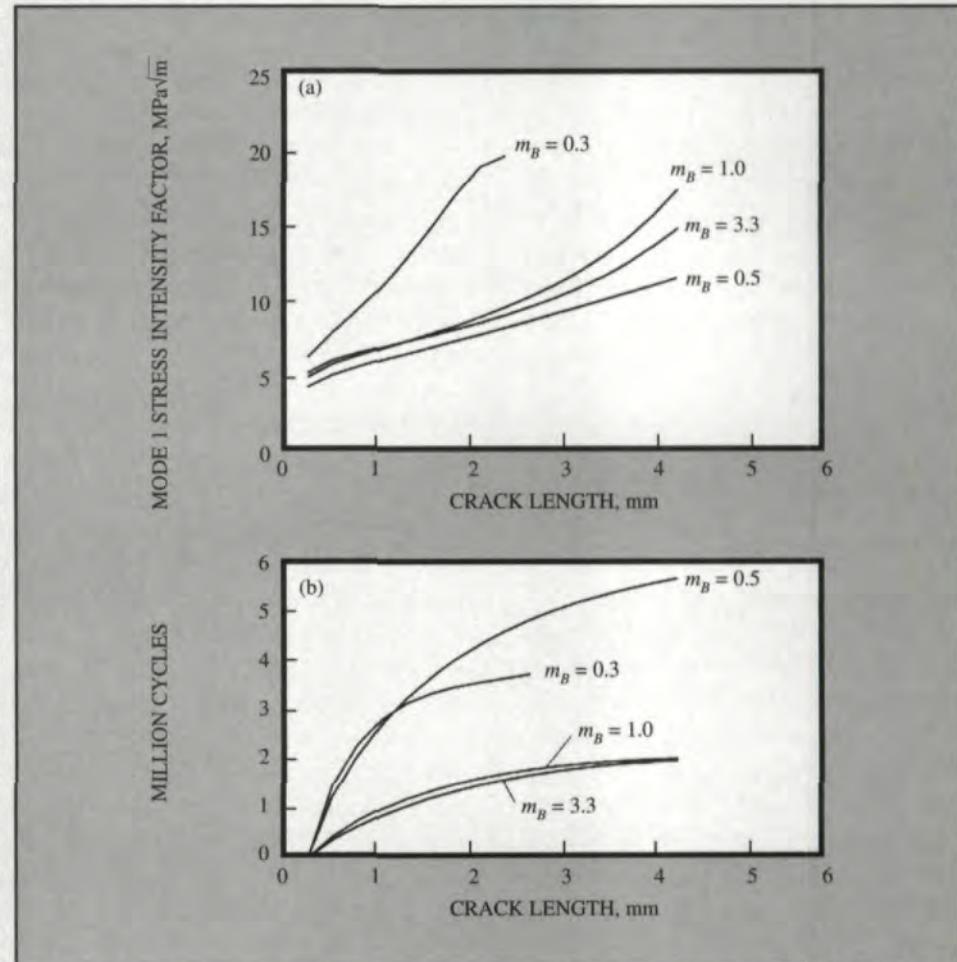


Fig. 9 — Effect of backup ratio on stress intensity factors and crack propagation cycles. (a) Mode I stress intensity factors. (b) Crack propagation cycles, Paris fatigue crack growth model, $n = 2.954$, $C = 8.433 \times 10^{-9} \text{ mm/cyc/(MPa}\sqrt{\text{m}})^n$, $U = 0.82 + 0.16R$.

element models. The Paris equation was used along with the effective stress intensity range ratios of Eq. 8. The initial cracks of the various models were placed at the location of the maximum tensile stress in the tooth fillet. The stress intensity factors were lowest for the $m_B = 0.5$ case. This gave the

highest predicted number of cycles for the cases studied. The cycles were all defined as the number of crack propagation cycles after an initial crack of 0.28 mm (0.011"). The stress intensity factors were highest for the $m_B = 0.3$ case. However, the predicted life for this was somewhere between the case of

$m_B = 0.5$ and 1.0 due to the fatigue crack closure effect. The cases of $m_B = 3.3$ and 1.0 gave nearly the same predicted life.

Conclusions

Based on these analytical and experimental studies, the following conclusions were made: 1) Good correlation between predicted and measured gear crack growth was achieved when the predictions used the Paris crack growth equation and the concept of fatigue crack closure. 2) For thin rims, a decrease in rim thickness caused an increase in both the stress intensity factor and the compressive cyclic stress in the gear tooth fillet region. The increase in stress intensity factor promoted crack growth, while the increase in cyclic compressive stress tended to retard crack growth and increase the number of propagation cycles to failure.

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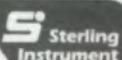


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Gear Shaving Basics – Part I

John P. Dugas

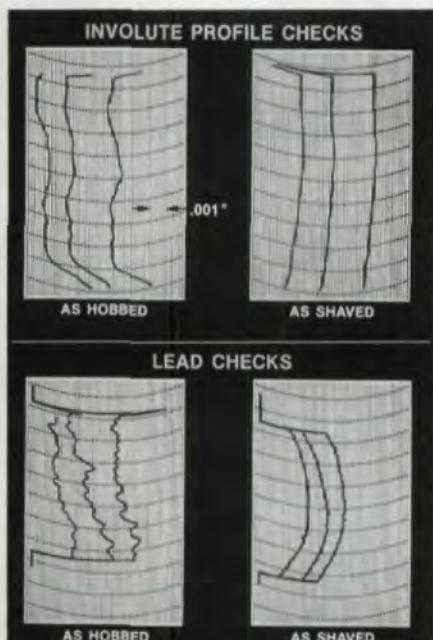


Fig. 1 — Charts showing improvement in profile and lead, 5.7 NPD, 20°, NPA, 3.85" P.D., crowned shaved with stock removal of 0.011" over pins.

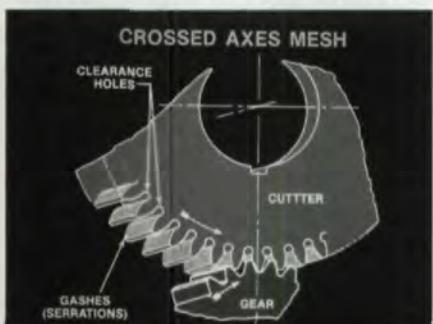


Fig. 2 — Work gear in crossed-axes mesh with rotary shaving cutter mounted above.

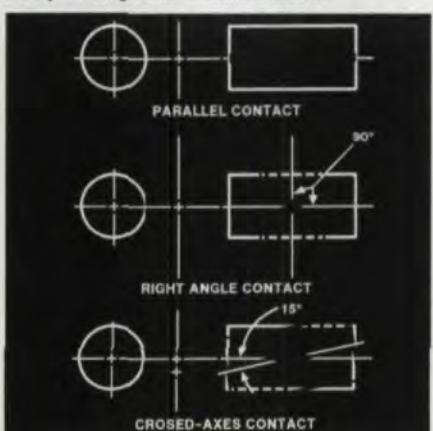


Fig. 3 — Contact between cylinders change as crossed axes are varied.

Gear shaving is a free cutting gear finishing operation which removes small amounts of metal from the working surfaces of gear teeth. Its purpose is to correct errors in index, helix angle, tooth profile and eccentricity (Fig. 1). The process also improves tooth surface finish and eliminates by means of crowned tooth forms the danger of tooth end load concentrations in service. Shaving provides for profile modifications that reduce gear noise, increase a gear's load carrying capacity, its factor of safety and its service life. Gear finishing (shaving) is not to be confused with gear cutting (roughing). They are essentially different. Any machine designed primarily for one cannot be expected to do both with equal effectiveness or with equal economy.

Gear shaving is the logical remedy for the inaccuracies inherent in gear cutting. It is equally effective as a control for those troublesome distortions caused by heat treatment.

The form of the shaving cutter can be reground to make profile allowance for different heat treat movements caused by varying heats of steel. The shaving machine can also be reset to make allowance for lead change in heat treatment.

Rotary gear shaving is a production process that utilizes a high speed, hardened and ground, ultra-precision steel shaving cutter. The cutter is made in the form of a helical gear. It has gashes in the flanks of the teeth which act as the cutting edges.

The cutter is meshed with the work gear in a crossed-axes relationship (Fig. 2) and rotated in both directions during the work cycle while the center distance is reduced in small increments. Simultaneously the work is traversed back and forth across the width of the cutter. The traverse path can either be parallel or

diagonal to the work gear axis, depending on the type of work gear, the production rate and finish requirements. The gear shaving process can be performed at high production rates. It removes material in the form of fine hair-like chips.

Machines are available to shave external spur and helical gears up to 200" in diameter. Other machines are also available for shaving internal spur and helical gears. For best results with shaving, the hardness of the gear teeth should not exceed 30 Rockwell C scale. If stock removal is kept to recommended limits, and the gears are properly qualified, the shaving process will finish gear teeth in the 7 to 20 pitch range to the following accuracies: involute profile, 0.0002"; tooth-to-tooth spacing, 0.0003" and lead or parallelism, 0.0002".

In any event, it should be remembered that gear shaving can remove 65–80% of the errors in a hobbed or shaped gear. It will make a good gear better. The final quality of the shaved gear is dependent to a large degree upon having good hobbed or shaped gear teeth.

Excellent surface finish is achieved with gear shaving. A value of approximately 25° is the normal finish obtained with production gear shaving, although much finer finishes are possible by slowing the process. In some cases, shaving cutters will finish up to 80,000 gears before they need sharpening. They may generally be sharpened from four to ten times.

To a gear designer, the shaving process offers attractive advantages in the ability to modify the tooth form. If a crowned tooth form or a tapered tooth form are desired to avoid end bearing conditions, these can be easily provided by shaving.

If modifications are desired in the involute profile, these can be made by suitable modifications in the ground cutter tooth form. If heat treatment distorts

GEAR FUNDAMENTALS

tions can be kept to a minimum, the most inexpensive way to produce an accurate, quiet, high-performance gear is to specify hobbing followed by gear shaving. The shaving process uses a variety of standardized production equipment ranging from hand loading to fully automatic loading and unloading.

Basic Principles

The rotary gear shaving process is based on fundamental principles. This process uses a gashed rotary cutter in the form of a helical gear having a helix angle different from that of the gear to be shaved. The axes of the cutter and the gear are crossed at a predetermined angle during the shaving operation. When the cutter and the work gear are rotated in close mesh, the edge of each cutter gash shaves a fine hair-like chip as it moves over the surface of a work gear tooth. The finer the cut, the less the pressure required between tool and work, eliminating the tendency to cold-work the surface metal of the work gear teeth.

This process is performed in a shaving machine, which has a motor-driven cutter head and a reciprocating work table. The cutter head is adjustable to obtain the desired crossed axis relationship with the work. The work carried between live centers is driven by the cutter. During the shaving cycle, the work is reciprocated parallel to its axis across the face of the cutter and upfed an increment into the cutter with each stroke of the table. This conventional shaving cycle is one of several methods.

The Crossed-Axis Principle

To visualize the crossed-axis principle, consider two parallel cylinders of the same diameter (Fig. 3). When brought together under pressure, their common contact surface is a rectangle having the length of a cylinder and width which varies with contact pressure and cylinder diameter.

When one of these cylinders is swung around so that the angle between its axis and that of the other cylinder is increased up to 90°, their common plane remains a parallelogram, but its area steadily decreases as the axial angle increases. The same conditions prevail when instead of the two plain cylinders, a shav-

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ing cutter and a work gear are meshed together. When the angle between their axes is from 10° to 15° , tooth surface contact is reduced, and the pressure required for cutting is small. As the work gear is moved away axially from the point of intersection of the axes, backlash develops. Conversely, as it is returned to the point of axial intersection, backlash decreases until the two members engage in tight mesh with the teeth of the cutter wedging between those of the work gear. Thus, each succeeding cutting edge sinks deeper into the work gear tooth until the point of axial intersection is reached.

For shaving, the cutter and work gear axes are crossed at an angle usually in the

range of 10° to 15° or approximately equal to the difference in their angles.

Crossing the axes produces reasonably uniform diagonal sliding action from the tip of the teeth to the root. This not only compensates for the nonuniform involute action typical of gears in mesh on parallel axes, but provides the necessary shearing action for stock removal.

Relationship Between Cutting & Guiding Action

Increasing the angle between the cutter and work axes increases cutting action, but, as this reduces the width of the contact zone, guiding action is sacrificed. Conversely, guiding action can be increased by reducing the angle of

crossed axes, but at the expense of cutting action.

Preparation Prior to Shaving

The first consideration in manufacturing a gear is to select the locating surfaces and use them throughout the process sequence. Close relationship between the locating surface and the face of the gear itself must be held. Otherwise, when the teeth are cut and finished with tooling that necessarily contacts the gear faces, the teeth will be in an improper relationship with the locating or related surface on which the gear operates. Gears that locate on round diameters or spline teeth must fit the work arbors closely or these critical hole-to-face relationships will be destroyed.

Typical manufacturing tolerances for gear blanks prior to cutting of the teeth are shown in Table 1.

Once the gear blank has been manufactured, it is necessary to cut the gear teeth. The most common methods today for rough-cutting gear teeth are hobbing and shaper cutting. Of primary concern to the shaving cutter manufacturer is the fillet produced by the roughing operation. The tips of the shaving cutter teeth must not contact the gear root fillet during the shaving operation. If such contact does occur, excessive wear of the cutter results, and the accuracy of the involute profile is affected.

The shaving cutter just finishes the gear tooth below its active profile. Thus, the height of the fillet should not exceed the lowest point of contact between the shaving cutter teeth and the teeth on the work gear.

Protuberance type hobs and shaper cutters are often used prior to shaving to produce a slight undercut or relief near the base of the gear tooth. This method assures a smooth blending of the shaved tooth profile and the unshaved tooth fillet, as well as reducing shaving cutter tooth tip wear (Fig. 4). The amount of undercut produced by the protuberance type tool should be made for the thin end of the tooth. The position of the undercut should be such that its upper margin meets the involute profile at a point below its contact diameter.

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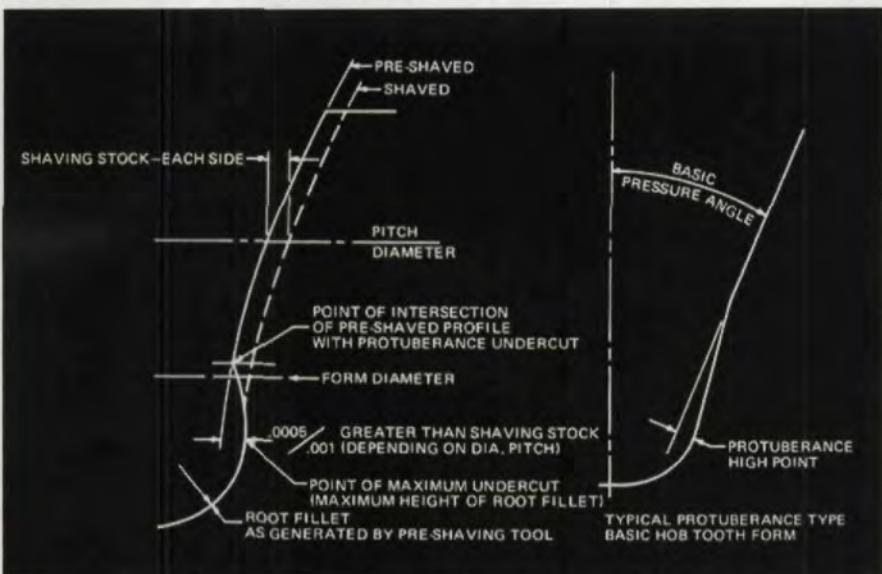


Fig. 4 — Undercut produced by protuberance hob and basic hob tooth form.

TABLE 1 — TYPICAL GEAR BLANK TOLERANCE

Blank Dia. In.	Face Runout In.	Hole Size In.	Hole Tape In./In.	Hole Roundness In.-Max.	O.D. In.-Max.	O.D. Runout In.
Up to 1 1-in Thick	0.0003— 0.0005	0.0003— 0.0006	0.0002— 0.0003	0.0002— 0.0003	0.003	0.003
1—4, up to 1 in. Thick	0.0004— 0.0008	0.0005— 0.001	0.0002— 0.0003	0.0003— 0.0005	0.005	0.005
4 to 8	0.0006— 0.0012	0.0008— 0.0012	0.0002— 0.0003	0.0004— 0.0006	0.005	0.007
8 to 12	0.001— 0.002	0.001— 0.0015	0.0002— 0.0003	0.0005— 0.0007	0.005	0.008

TABLE 2 — RECOMMENDED SHAVING STOCK AND UNDERCUT FOR PRESHAVED GEARS.

Normal Diametral Pitch	Shaving Stock (In. per Side of Tooth)	Total Undercut (In. per Side of Tooth)
2—4	0.0015—0.0020	0.0025—0.0030
5—6	0.0012—0.0018	0.0023—0.0028
7—10	0.0010—0.0015	0.0015—0.0020
11—14	0.0008—0.0013	0.0012—0.0017
16—18	0.0005—0.0010	—
20—48	0.0003—0.0008	—
52—72	0.0001—0.0003	—

Shaving Stock

The amount of stock removed during the shaving process is a key to its successful application. Sufficient stock should be removed to permit correction of errors in the preshaved teeth. However, if too much stock is removed, cutter life and part accuracy are effectively reduced.

Table 2 shows the recommended amounts of stock to be removed during the shaving operations and the corresponding amount of undercut required. ☀

Acknowledgement: Presented by National Broach & Machine at the Society of Manufacturing Engineers 1st International Advanced Gear Processing & Manufacturing Conference, June, 1996.

The second half of this article, covering shaving methods and design, will appear in our Jan/Feb, 1998, issue.

John P. Dugas

for many years was the Chief Tool Engineer at National Broach & Machine. He is the author of numerous papers and presentations on gear subjects. He is now retired.

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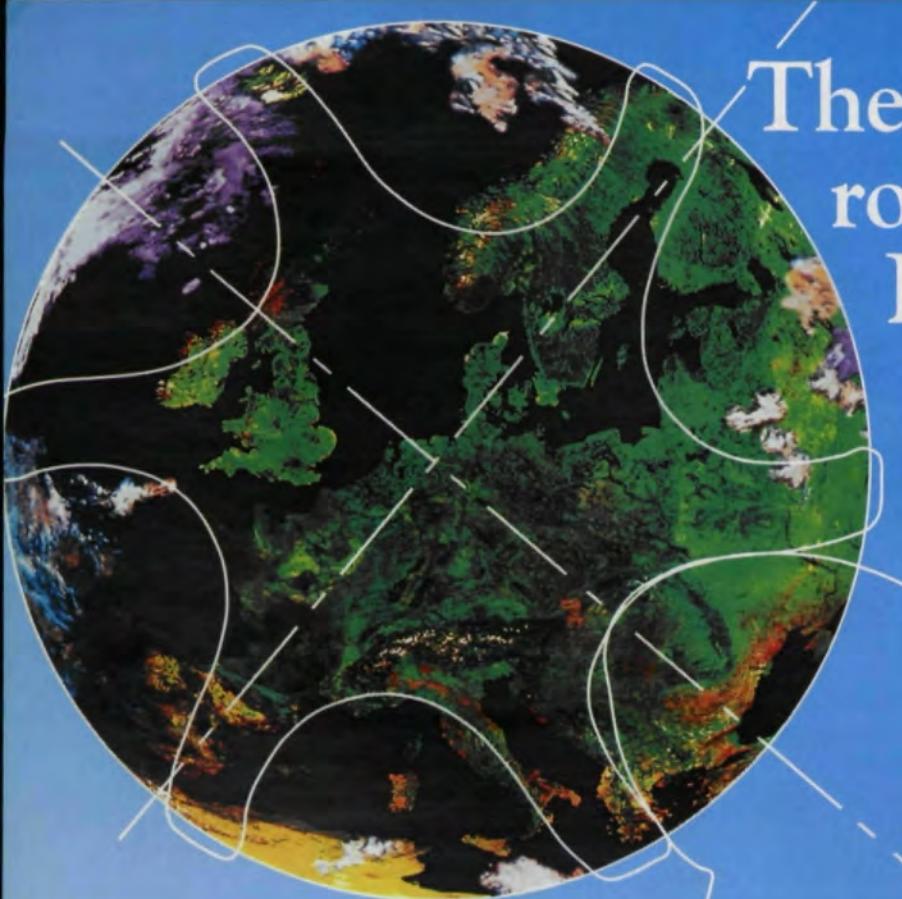
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PRODUCTS & SERVICES INDEX

Welcome to the 1998 *Gear Technology* Buyers Guide Product & Services Index. Use this index to locate the names of companies according to the products and services they provide. The complete mailing address, phone and fax numbers and e-mail and Web site addresses of each company are listed in the Company Index. *Gear Technology* advertisers are shown in boldface type. To find the pages on which their ads appear, see the Advertisers Index on page 68.

While we have made every effort to ensure that company names and addresses are correct, we cannot be held responsible for errors of fact or omission.

If your company is not listed and you would like to be included in next year's directory, e-mail people@geartechnology.com, call 847-437-6604, or fax 847-437-6618, and we will add you to our mailing list.

GEAR & DRIVE MANUFACTURERS

Differentials

Bevel Gears (India)
Engelhardt Gear Co.
Euclid Universal Corp.
Fleet Tools Ltd.
Gajra Gears Ltd.
Grupos Diferenciales
ITW Spiroid
Indiana Power
Transmission Systems
Nissei Corp. of America
Sri Venkateshwara Gear

Gear Boxes, Gear Drives & Speed Reducers

ACR Industries
ATA Gears Inc.
Adobe Precision Gear, Inc.
Advance Gear & Machine
Aero Gear, Inc.
Allied Devices Corp.
Alpha Gear Drives Inc.
Amarillo Gear
Co.-Amarillo
Amarillo Gear
Co.-Russellville
American Metric Corp.
Andantex USA
Anderson International
Aplus Engineering Inc.
Arrow Gear Co.
Ashot Ashkelon Indust.
Ashot USA Inc.
Axicon Technologies
Bevel Gears (India)
Bison Gear & Engineering
Blanchat Machine Co.
Bonfiglioli Riduttori
Bonfiglioli U.K.
Boston Gear
C-B Gear & Machine, Inc.
CMD (UK) Ltd.
Calicut Eng. Works Ltd.
Channel Power
Transmission, Inc.
Charles Bond Co.
Chicago Gear-D. O. James
Ciateq, A. C.
The Cincinnati Gear Co.
Circle Gear & Machine
Columbia Gear Corp.
Cone Drive Operations
Curtis Machine Co., Inc.
Cyclo Transmissions Ltd.
Davall Gear Co. Ltd.
Dayton Gear & Tool
Delroyd Worm Gear
Dynamic Tool Grinding
Electra-Gear
Engelhardt Gear Co.
Engranes Industriales
Rivera
Euclid Universal Corp.

Fairfield Mfg. Co.
Falk Corp.
Fleet Tools Ltd.
Flender Corporation
Flender-Graffenstaden
Foote-Jones/Illinois Gear
GW Plastics
Gajra Gears Ltd.
Gear Products Inc.
Gear Systems Inc.
The Gear Works-Seattle
Gears & Drive Systems
Geartronics Industries
Great Gear Co.
Greenspon Engineering
Works Ltd.
Grove Gear
Grupos Diferenciales
Hamilton Gear
Harder Precision
Components
Harmonic Drive
Technologies
Harmschfeger
Hico
Horsburgh & Scott
Hub City, Inc.
ITW Spiroid
Indiana Power
Transmission Systems
Indiana Tool/Indiana Gear
Inesco Corporation
Labeco
Lufkin Industries Gear
Repair
MO Star Gear & Machine
Maquinaria Ral, S.A.
Merit Gear Corp.
Micron Instrument Corp.
Milwaukee Gear Company
Mitrapak Power
Transmission Products
Moore Gear Mfg. Co.
Moore Machine & Gear
Nanchang Gear Works
Nissei Corp. of America
Nord Gear Corporation
Nuttall Gear Corp.
Ohio Gear
Ontario Drive & Gear
Overton Gear & Tool
PIC Design
Penn Machine Company
Pennsylvania Gear Corp.
Philadelphia Gear
Corp.-King of Prussia
Philadelphia Gear
Corp.-Houston
Power Eng. & Mfg. Ltd.
Precipart Corp.
Precision Gear Inc.
Precision Gears Inc.
The Purdy Corporation
R. Cushman & Associates
Rapid Gear
Reliance Gear Co. Ltd.
Reliance Gear Corp.

Renold Power
Transmission Corp.
Rexnord Corporation
RJ Link International
Rockwell Automation /
Dodge
Ronson Gears Pty. Ltd.
Santasalo Gears Service
Shin Shin Enterprises
Sri Venkateshwara Gear
Sterling Electric
Sumitomo Machinery
Sussex Gear Company
Torque Transmission
Trogetec Inc.
United States Gear
Von Ruden Mfg.
Walter Machine Co., Inc.
Wedin Int'l. Inc.
Wes-Tex Gear Inc.
Westech Gear
Westerner Companies
Weyers Bros (FT) Ltd.
Winsmith
ZF Industrial Drives
Zenith Sintered Products
Zero-Max, Inc.

Gear Couplings

Amarillo Gear
Co.-Russellville
Harmonic Drive
Technologies
Lovejoy Inc.
TB Wood's, Inc.

Gear Motors

Bison Gear & Engineering
Bonfiglioli Riduttori
C-B Gear & Machine, Inc.
Channel Power
Transmission, Inc.
Euclid Universal Corp.
Fleet Tools Ltd.
Greenspon Engineering
Works Ltd.
Groschopp
Grove Gear
Hub City, Inc.
Nissei Corp. of America
Nord Gear Corporation
Ohio Gear
Renold Power
Transmission Corp.
Rexnord Corporation
Ronson Gears Pty. Ltd.
Sri Venkateshwara Gear

Gear Reducers

American Metric Corp.
Andantex USA
Channel Power
Transmission Inc.

Gears-Helical

ACR Industries
Reliance Gear Co. Ltd.
Reliance Gear Corp.

The Adams Company
Adobe Precision Gear, Inc.
Advance Gear & Machine
Aero Gear, Inc.
Aerocon Industries Inc.
Allied Devices Corp.
Allied Gear Co.
Amarillo Gear
Co.-Amarillo
Amarillo Gear
Co.-Russellville
American Gear & Eng.
American Mach. & Gear
American Precision Gear
Andantex USA
Aplus Engineering Inc.
Arrow Gear Co.
Ashot Ashkelon Indust.
Ashot USA Inc.
Axicon Technologies
Barit International Corp.
Bengal Industries Inc.
Bevel Gears (India)
Bilgrami Gear Co.
Bonfiglioli Riduttori
Bonfiglioli U.K.
Boonville Mining Services
Boston Gear
Bourn & Koch
Boxx Gear Mfg.
Buckeye Gear Co.
Bucyrus International, Inc.
Burgess-Norton Mfg. Co.
C-B Gear & Machine, Inc.
CMD (UK) Ltd.
Calicut Eng. Works Ltd.
Capstan Atlantic
Carbon City Products
Caterpillar Industrial
Products Inc.
Channel Power
Transmission, Inc.
Chardam Gear Co.
Charles Bond Co.
Chicago Gear-D. O. James
Chicago Gear Works
Ciateq, A. C.
The Cincinnati Gear Co.
Circle Gear & Machine
Cloyes Gear & Products
Columbia Gear Co.
Commercial Gear &
Sprocket
Crown Gear B.V.
Curtis Machine Co. Inc.
Dabko Industries Inc.
Davall Gear Co. Ltd.
Dayton Gear & Tool
Dearborn Gear & Tool Co.
E.C. Machining, Inc.
EMCO Gears
Electra-Gear
Electrex Ltd. (India)
Engelhardt Gear Co.
Engranes Industriales
Rivera
Enrecon S.A.

Euclid Universal Corp.
Fairfield Mfg. Co.
Falk Corp.
Federal Gear Corp.
Fleet Tools Ltd.
Flender Corporation
Foote-Jones/Illinois Gear
Forest City Gear Co.
Franke Gear Works Inc.
GW Plastics
Gear Company of America
Gear Products Inc.
Gear Systems Inc.
The Gear Works-Seattle
Gears & Drive Systems
Geartronics Industries
General Gear Corporation
Generated Gear &
Machine
Global Gear
Globe Gear Co.
Great Gear Co.
Greenspon Engineering
Works Ltd.
HMC
Hamilton Gear
Hanover Gear Mfg. Co.
Harder Precision
Components
Harmschfeger
Hico
Holroyd Machine
Horsburgh & Scott
Hua Yang Machine
Hub City, Inc.
Inesco Corporation
Intech Corp.
Invo Spine Inc.
J&E Hofmann Eng.
Jackson Gear Co.
Jade Precision Gear Co.
KA-Wood Gear
Keller Machine Co.
Kreiter Geartech
Krupp Engineering Inc.
L + H Welding & Machine
Lawler Gear Corp.
Lufkin Industries Gear
Repair
Lyon Gear
M.J.H. Gear & Tool Co.
MO Star Gear & Machine
Maquinaria Ral, S.A.
Mascotech-Braun
Merit Gear Corp.
Micron Instrument Corp.
Midwest Gear
Midwest Gear & Tool
Milford Gear Works
Milwaukee Gear Company
Molon Gear & Shaft
Moore Gear Mfg. Co.
Moore Machine & Gear
Murray Brothers Mfg.
Nanchang Gear Works
National Broach
Niagara Gear Corp.

Nissei Corp. of America

Nixon Gear

Nord Gear Corporation

Nordberg Lokomo OY

Nuttall Gear Corp.

Oliver Gear

Omni Gear & Machine

O'Neill Gear

Ontario Drive & Gear

Overton Gear & Tool

PIC Design

Patterson Gear & Machine

Penn Machine Company

Pennsylvania Gear Corp.

Penntech

Perry Technology

Philadelphia Gear

Corp.-King of Prussia

Philadelphia Gear

Corp.-Houston

Poly Hi Solidur

Power Eng. & Mfg. Ltd.

Precipart Corp.

Precision Gear Co.

Precision Gear Inc.

Precision Gears Inc.

Presrite Corp.

Process Industries

Production Gear & Broach

Progressive Engineering

The Purdy Corporation

Qualicast Corp.

R.L. Wagner & Assoc.

Rapid Gear

Rawling Gear

Reliance Gear Co. Ltd.

Reliance Gear Corp.

Riley Gear Corp.

Riverside Spine & Gear

Rj Link International

Ronson Gears Pty. Ltd.

STD Precision Gear &

Instrument, Inc.

Santasalo Gears Service

Satellite Gear

Schafer Gear Works Inc.

Sri Venkateshwara Gear

Sterling Electric

Stock Drive Prod./Sterling

Instrument

Tech Sales Inc.

Textile Parts & Machine

Tifco Gage & Gear

Trojan Gear Inc.

United States Gear

Von Ruden Mfg.

Walter Machine Co., Inc.

Wedin Int'l. Inc.

Wes-Tex Gear Inc.

West Industries Inc.

Westech Gear

Western Spline Gage

Worcester Gear Works

Worrall Grinding Co.

Xtek Inc.

Zenith Sintered Products

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Gears—Herringbone

Adobe Precision Gear, Inc.
American Mach. & Gear
Anderson International
Aplus Engineering Inc.
Axicon Technologies
Bilgram Gear Co.
Boonville Mining Services
C-B Gear & Machine, Inc.
CMD (UK) Ltd.
Calicut Eng. Works Ltd.
Chicago Gear-D. O. James
Ciateq, A. C.
The Cincinnati Gear Co.
Circle Gear & Machine
Dayton Gear & Tool
Engelhardt Gear Co.
Energraves Industrielles

Rivera
Falk Corp.
Federal Gear Corp.
Foote-Jones/Illinois Gear
The Gear Works-Seattle
Gears & Drive Systems
Globe Gear Co.
Great Gear Co.
HMC
Hamer Gear
Horsburgh & Scott
Intech Corp.
J&E Hofmann Eng.
Kreiter Geartech
L + H Welding & Machine
Lufkin Industries Gear
Repair
Maquinaria Ral, S.A.
Midwest Gear
Moore Gear Mfg. Co.
Nordberg Lokomo OY
Oliver Gear
Penn Machine Company
Philadelphia Gear
Corp.-Houston
Precision Gear Inc.
Process Industries
Progressive Engineering
Qualicast Corp.
Rapid Gear
Santatalo Gears Service
Shin Shin Enterprises
Wes-Tex Gear Inc.
Westech Gear
Westerman Companies
Xtek Inc.

Gears—Hypoid

ACR Industries
ATA Gears Inc.
Aero Gear Inc.
Amarillo Gear
Co.-Amarillo
Amarillo Gear
Co.-Russellville
Arrow Gear Co.
Ashot Ashkelon Indust.
Ashot USA Inc.
Astron Midwestern Inc.
Bevel Gears (India)
Bonfiglioli Riduttori
Bonfiglioli U.K.
Caterpillar Industrial
Products Inc.
Channel Power
Transmission, Inc.
Davall Gear Co. Ltd.
Engelhardt Gear Co.
Engrecon S.A.
Fairfield Mfg. Co.

Foote-Jones/Illinois Gear

Globe Gear Co.
Great Gear Corp.
 Grupos Diferenciales
 Hamilton Gear
Midwest Gear & Tool
 Moore Gear Mfg. Co.
 Nissei Corp. of America
 Ohio Gear
Philadelphia Gear
 Corp.—King of Prussia
 Precision Gear Co.
Presrite Corp.
 Qualcast Corp.
 Rawling Gear
 Reliance Gear Corp.
 Santasalo Gears Service
 United States Gear
 Wedin Intl. Inc.
 West Industries Inc.
 Westech Gear

Gears—Internal
 ACR Industries
 Acme Gear Co.
 The Adams Company
 Adobe Precision Gear, Inc.
 Advance Gear & Machine
 Aero Gear, Inc.
 Aerocom Industries Inc.
 Allied Devices Corp.
Allied Gear Co.
 Amarillo Gear
 Co.—Russellville
 American Gear & Eng.
 American Mach. & Gear
 American Precision Gear
 Aplus Engineering Inc.
 Arrow Gear Co.
 Axicon Technologies
 Bengal Industries Inc.
 Bevel Gears (India)
 Bilgram Gear Co.
 Blanchat Machine Co.
 Boston Gear
 Boxx Gear Mfg.
 Buckeye Gear Co.
 CMD (UK) Ltd.
 Calicut Eng. Works Ltd.
 Carbon City Products
 Caterpillar Industrial
 Products Inc.
 Chardam Gear Co.
 Charles Bond Co.
 Chicago Gear-D. O. James
 Chicago Gear Works
 The Cincinnati Gear Co.
 Circle Gear & Machine
 Cloyes Gear & Products
 Columbia Gear Co.
 Commercial Gear &
 Sprocket
 Davall Gear Co., Ltd.
 Dayton Gear & Tool
 Dynamic Tool Grinding
 EMCO Gears
 Engelhardt Gear Co.
 Engranes Industriales
 Rivera
 Engrecon S.A.
Fairfield Mfg. Co.
 Federal Gear Corp.
 Fleet Tools Ltd.
 Foote-Jones/Illinois Gear
 Forest City Gear Co.
 Franke Gear Works Inc.
 Gear Company of America
 Gear Products Inc.

The Gear Works-Salt Lake City
Geartronics Industries
Generated Gear & Machine
Globe Gear Co.
Greenspon Engineering Works Ltd.
HMC
Hamilton Gear
Hanover Gear Mfg. Co.
Harder Precision Components
Harmschfeger
Highway Machine Co.
Horsburgh & Scott
Hua Yang Machine
ITW Spiroid
Indiana Tool/Indiana Gear
Intech Corp.
Invo Spline Inc.
J&E Hofmann Eng.
Jackson Gear Co.
Jade Precision Gear Co.
KA-Wood Gear & Machine
Kreiter Geartech
Krupp Engineering Inc.
L + H Welding & Machine
Lawler Gear Corp.
Lyon Gear
M.J.H. Gear & Tool Co.
MO Star Gear & Machine
Maquinaria Ral, S.A.
Mascotech-Braun
Micron Instrument Corp.
Midwest Gear
Midwest Gear & Tool
Milford Gear Works
Milwaukee Gear Company
Modified Gear & Spine
Moore Gear Mfg. Co.
Moore Machine & Gear
Nanchang Gear Works
Nissei Corp. of America
Nixon Gear
Nordberg Lokomo OY
Oliver Gear
Omni Gear & Machine
O'Neill Gear
Ontario Drive & Gear
Orlandi Gear Company
Overton Gear & Tool
Patterson Gear & Machine
Penn Machine Company
Pennsylvania Gear Corp.
Penntech
Perry Technology
Philadelphia Gear Corp.-Houston
Philadelphia Gear Corp.-King of Prussia
Power Eng. & Mfg.
Precipart Corp.
Precision Gear Co.
Precision Gear Inc.
Precision Gears Inc.
Process Industries
Production Gear & Broach
Progressive Engineering
The Purdy Corporation
Rapid Gear
Rawling Gear
Reliance Gear Co. Ltd.
Reliance Gear Corp.
Riley Gear Corp.
Riverside Spline & Gear
RJ Link International
Ronson Gears Pty. Ltd.

STD Precision Gear
Santasalo Gears Service
Satellite Gear
Schafer Gear Works Inc.
Shin Shin Enterprises
Sri Venkateshwara Gear
Textile Parts & Machine
Tifco Gage & Gear
Trogetec Inc.
Trojan Gear Inc.
United States Gear
Von Ruden Mfg.
Wedit Int'l. Inc.
West Industries Inc.
Westech Gear
Winzeler Gear
Worcester Gear Works
Xtek Inc.

Gears-Master
ACR Industries
Amarillo Gear
Co.-Russellville
American Mach. & Gear
Arrow Gear Co.
Barit International Corp.
Boston Gear
CMD (UK) Ltd.
The Cincinnati Gear Co.
Davall Gear Co. Ltd.
Dayton Gear & Tool
Delroyd Worm Gear
Engelhardt Gear Co.
Engranes Industrielles
Rivera
Fairfield Mfg. Co.
Fellows Corp.
Fleet Tools Ltd.
Forest City Gear Co.
The Gear Works-Seattle
Generated Gear &
Machine
Holroyd Machine
ITW Heartland
ITW Spiroid
Invo Spline Inc.
M&M Precision System
Mahr Corporation
Modified Gear & Spline
Nanchang Gear Works
National Broach
Nixon Gear
Perry Technology
Philadelphia Gear
Corp.-Houston
Philadelphia Gear
Corp.-King of Prussia
Precision Gage Co.
Precision Gear Inc.
The Purdy Corporation
Russell, Holbrook &
Henderson
SRP Tools Ltd.
SU America Inc.
Santasalo Gears Service
Shin Shin Enterprises
Spline Gauges Ltd.
Tifco Gage & Gear
Trogetec Inc.
Westerman Companies
Western Spline Gage

Gears—Non-Circular

Advance Gear & Machine
 Bengal Industries Inc.
 Bilgram Gear Co.
 Calicut Eng. Works Ltd.
 Cunningham Industries
 GW Plastics
 Gear Company of America
 Generated Gear &
Machine
 Globe Gear Co.
 Horsburgh & Scott
 J&E Hofmann Eng.
 Krupp Engineering Inc.
 Merit Gear Corp.
Midwest Gear & Tool
Perry Technology
 Precision Gear Inc.
 Trogetec Inc.
 Wedin Intl. Inc.
 Worcester Gear Works

Gears—Planetary
 Acme Gear Co.
 Adobe Precision Gear, Inc.
 Amarillo Gear
 Co.—Russellville
 American Gear & Eng.
 American Precision Gear
 CMD (UK) Ltd.
 Capitol Stamping Corp.
 Greenspon Engineering
 Works Ltd.
 Rapid Gear
 STD Precision Gear
 Santasalo Gears Service

Gears—Plastic
 Acme Gear Co.
 Allied Devices Corp.
 American Gear & Eng.
 American Mach. & Gear
 American Precision Gear
 Andantex USA
 Arrow Gear Co.
 Bengal Industries Inc.
 Bilgram Gear Co.
 Boston Gear
 Buckeye Gear Co.
 Calicut Eng. Works Ltd.
 Capitol Stamping Corp.
 Chicago Gear-D. O. James
 Chicago Gear Works
 Commercial Gear &
 Sprocket
 Dabko Industries Inc.
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 Engranes Industriales
 Rivera
 Forest City Gear Co.
 GW Plastics
 Gear Company of America
 Gear Systems Inc.
 The Gear Works—Seattle
 Gears & Drive Systems
 Geartronics Industries
 Generated Gear &
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 Globe Gear Co.
Great Gear Corp.
 Intech Corp.
 J&E Hofmann Eng.
 KA-Wood Gear &
Machine
 Keller Machine Co.
 M.J.H. Gear & Tool Co.
 Martin Sprocket & Gear
Midwest Gear

Midwest Gear & Tool

Moore Gear Mfg. Co.
 Moore Machine & Gear
 Murray Brothers Mfg.
 Omni Gear & Machine
 PIC Design
Perry Technology
 Philadelphia Gear
 Corp.—Houston
 Precision Gear Co.
 Precision Gears Inc.
 Process Industries
 Progressive Engineering
 Putnam Precision
 Molding, Inc.
 R.L. Wagner & Assoc.
 Rapid Gear
 Reliance Gear Corp.
 Riley Gear Corp.
Shin Shin Enterprises
 Textile Parts & Machine
 Tifco Gage & Gear
 Trogetec Inc.
 Trojion Gear Inc.
 Wedin Intl. Inc.
 Winzeler Gear
 Worcester Gear Works

Gears—Powder Metal

Aplus Engineering Inc.
 Asco Sintering Co.
 Ashot USA Inc.
 BestMetal Corp.
 Burgess-Norton Mfg. Co.
 Capstan Atlantic
 Carbon City Products
 Cloyes Gear & Products
 Dabko Industries Inc.
 The Gear Works—Seattle
Great Gear Corp.
 ITW Spiroid
 Keystone Powdered Metal
 Lyon Gear
M&M Precision Systems
 Martin Sprocket & Gear
 Metal Powder
 Components
 Moore Gear Mfg. Co.
 Pennsylvania Pressed
 Metal Inc.
 Precision Gear Co.
 St. Marys Carbon Co.
Shin Shin Enterprises
 Tifco Gage & Gear
 Trogetec Inc.
 Zenith Sintered Products

Gears—Racks

ACR Industries
 Allied Devices Corp.
 American Mach. & Gear
 American Metric Corp.
 American Precision Gear
 Andantex USA
 Anderson International
 Aplus Engineering Inc.
 Asco Sintering Co.
 Bevel Gears (India)
 Bonville Mining Services
 Boston Gear
 C-B Gear & Machine, Inc.
 Capstan Atlantic
 Carbon City Products
 Charles Bond Co.
 The Cincinnati Gear Co.
 Circle Gear & Machine
 Commercial Gear &
 Sprocket

Cornell Forge Co.
Dabko Industries Inc.
Davall Gear Co. Ltd.
Dayton Gear & Tool
EMCO Gears
Engelhardt Gear Co.
Engranes Industrielles
Rivera
Federal Gear Corp.
Fellows Corp.
Fleet Tools Ltd.
Foote-Jones/Illinois Gear
Franke Gear Works Inc.
GW Plastics
Gear Company of America
The Gear Works-Seattle
Gears & Drive Systems
Geartronics Industries
Generated Gear &
Machine
Globe Gear Co.
HMC
Harder Precision
Components
Harnischfeger
Highway Machine Co.
Hua Yang Machine
Intech Corp.
J&E Hofmann Eng.
Jade Precision Gear Co.
Keystone Powdered Metal
Krupp Engineering Inc.
Lawler Gear Corp.
MO Star Gear & Machine
Maquinaria Ral, S.A.
Martin Sprocket & Gear
Modified Gear & Spline
Moore Gear Mfg. Co.
Moore Machine & Gear
National Broach
Nixon Gear
Oliver Gear
Patterson Gear & Machine
Perry Technology
Pitch Templates, Inc.
Ply-Mar Tool Co.
Poly Hi Solidur
Precipart Corp.
Progressive Engineering
Pulley Manufacturers Inc.
Qualicast Corp.
Rapid Gear
Reliance Gear Co. Ltd.
Riley Gear Corp.
Riverside Spline & Gear
Ronson Gears Pty. Ltd.
STD Precision Gear
Satellite Gear
Shin Shin Enterprises
Sri Venkateshwara Gear
Trogetec Inc.
Troyon Gear Inc.
Wedin Intl. Inc.
Worcester Gear Works
Xtek Inc.

Gears-Ring

Acme Gear Co.
Amarillo Gear
Co.-Russellville
American Gear & Eng.
American Precision Gear
Boonville Mining Services
C-B Gear & Machine, Inc.
Circle Gear & Machine
Davall Gear Co. Ltd.
Delroyd Worm Gear
Engelhardt Gear Co.

Hamilton Gear
Indiana Tool/Indiana Gear
Inesco Corporation
Jade Precision Gear Co.
MO Star Gear & Machine
Nissei Corp. of America
Overton Gear & Tool
Production Gear & Broach
Rapid Gear
Rawling Gear
Reliance Gear Co. Ltd.
Ronson Gears Pty. Ltd.
STD Precision Gear
Santasalo Gears Service
Sri Venkateshwara Gear

Gears-Segment

Acme Gear Co.
Amarillo Gear
Co.-Russellville
American Precision Gear
C-B Gear & Machine, Inc.
Circle Gear & Machine
Davall Gear Co. Ltd.
Delroyd Worm Gear
Engelhardt Gear Co.
Euclid Universal Corp.
Hamilton Gear
ITW Spiroid
Nissei Corp. of America
Production Gear & Broach
Rapid Gear
Rawling Gear
Ronson Gears Pty. Ltd.
STD Precision Gear
Sri Venkateshwara Gear

Gears-Spiral Bevel

ACR Industries
ATA Gears Inc.
Advance Gear & Machine
Aero Gear, Inc.
Amarillo Gear
Co.-Amarillo
Amarillo Gear
Co.-Russellville
Arrow Gear Co.
Asco Sintering Co.
Ashot Ashkelon Indust.
Astron Midwestern Inc.
Blanchat Machine Co.
Bonfiglioli Riduttori
Bonfiglioli U.K.
Boston Gear
Bourn & Koch
Burgess-Norton Mfg. Co.
CMD (UK) Ltd.
Carbon City Products
Caterpillar Industrial
Products Inc.
Channel Power
Transmission, Inc.
Chicago Gear-D. O. James
Ciateq, A. C.
The Cincinnati Gear Co.
Curtis Machine Co. Inc.
Davall Gear Co. Ltd.
Electrex Ltd. (India)
Engelhardt Gear Co.
Engranes Industrielles
Rivera
Engrecon S.A.
Fairfield Mfg. Co.
Falk Corp.
Foote-Jones/Illinois Gear
The Gear Works-Seattle
Gears & Drive Systems
Globe Gear Co.

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Hamilton Gear	Products Inc.	Krupp Engineering Inc.	Stock Drive Prod/Sterling	Federal Gear Corp.	Acme Gear Co.
Hico	Channel Power	L + H Welding & Machine	Instrument	Fleet Tools Ltd.	The Adams Company
Horsburgh & Scott	Transmission, Inc.	Lampin Corporation	Tech Sales Inc.	Foot-Jones/Illinois Gear	Adobe Precision Gear, Inc.
Hua Yang Machine	Chardam Gear Co.	Lawler Gear Corp.	Textile Parts & Machine	GW Plastics	Advance Gear & Machine
Hub City, Inc.	Charles Bond Co.	Lufkin Industries Gear	Tifco Gage & Gear	Gear Company of America	Aero Gear, Inc.
Intech Corp.	Chicago Gear-D. O. James	Repair	Trogetec Inc.	The Gear Works-Seattle	Allied Devices Corp.
Keystone Powdered Metal	Chicago Gear Works	Lyon Gear	Trojan Gear Inc.	Gears & Drive Systems	Allied Gear Co.
Krupp Engineering Inc.	Ciateq, A. C.	M.J.H. Gear & Tool Co.	United States Gear	Geartronics Industries	Amarillo Gear
Micron Instrument Corp.	The Cincinnati Gear Co.	MO Star Gear & Machine	Von Ruden Mfg.	Generated Gear &	Co.-Russellville
Midwest Gear & Tool	Circle Gear & Machine	Maquinaria Ral, S.A.	Walter Machine Co., Inc.	Machine	American Gear & Eng.
Milford Gear Works	Cloyes Gear & Products	Martin Sprocket & Gear	Wedin Int'l. Inc.	Globe Gear Co.	American Mach. & Gear
Moore Gear Mfg. Co.	Columbia Gear Co.	Merit Gear Corp.	West Industries Inc.	Great Gear Corp.	American Precision Gear
Nanchang Gear Works	Commercial Gear &	Micron Instrument Corp.	Westech Gear	Grupos Diferenciales	Aplus Engineering Inc.
Nissei Corp. of America	Sprocket	Midwest Gear	Westerman Companies	Hamilton Gear	Bengal Industries Inc.
Ohio Gear	Cornell Forge Co.	Midwest Gear & Tool	Western Spline Gage	Hua Yang Machine	Bevel Gears (India)
PIC Design	Crown Gear B.V.	Milford Gear Works	Windsor Gear Co.	Hub City, Inc.	Bilgram Gear Co.
Philadelphia Gear	Cunningham Industries	Milwaukee Gear Company	Winzeler Gear	Intech Corp.	Blanchat Machine Co.
Corp.-Houston	Curtis Machine Co. Inc.	Mobil Pulley & Machine	Wohlert Corp.	J&E Hofmann Eng.	Bonfiglioli Riduttori
Philadelphia Gear	Cyclo Transmissions Ltd.	Modified Gear & Spline	Worcester Gear Works	Jackson Gear Co.	Bonfiglioli U.K.
Corp.-King of Prussia	Dabko Industries Inc.	Molon Gear & Shaft	Worrall Grinding Co.	Keystone Powdered Metal	Boston Gear
Precision Gear Co.	Davall Gear Co. Ltd.	Moore Gear Mfg. Co.	Xtek Inc.	Krupp Engineering Inc.	Bourn & Koch
Presrite Corp.	Dayton Gear & Tool	Moore Machine & Gear	Zhuhai Intercontinental	Lawler Gear Corp.	Boxx Gear Mfg.
The Purdy Corporation	Dearborn Gear & Tool Co.	Murray Brothers Mfg.	Pulleys Ltd.	M.J.H. Gear & Tool Co.	Buckeye Gear Co.
Rawling Gear	Dynamic Tool Grinding	Nanchang Gear Works	Gears-Straight Bevel	MO Star Gear & Machine	C-B Gear & Machine, Inc.
Reliance Gear Corp.	E.C. Machining, Inc.	Niagara Gear Corp.	ACR Industries	Maquinaria Ral, S.A.	CMD (UK) Ltd.
Riverside Spline & Gear	EMCO Gears	Nissei Corp. of America	The Adams Company	Martin Sprocket & Gear	Calicut Eng. Works Ltd.
Santasalo Gears Service	Electrex Ltd. (India)	Nixon Gear	Adobe Precision Gear, Inc.	Mascotech-Braun	Channel Power
Shin Shin Enterprises	Engelhardt Gear Co.	Nordberg Lokomo OY	Advance Gear & Machine	Midwest Gear & Tool	Transmission, Inc.
Tech Sales Inc.	Engranes Industriales	Oliver Gear	Aero Gear, Inc.	Milford Gear Works	Charles Bond Co.
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Von Ruden Mfg.	Engrecon S.A.	O'Neill Gear	Allied Gear Co.	Transmission Products	Commercial Gear &
Wedin Int'l. Inc.	Euclid Universal Corp.	Ontario Drive & Gear	Amarillo Gear	Moore Gear Mfg. Co.	Sprocket
West Industries Inc.	Fairfield Mfg. Co.	Orlandi Gear Company	Co.-Russellville	Moore Machine & Gear	Cone Drive Operations
Westech Gear	Falk Corp.	Overton Gear & Tool	American Gear & Eng.	Nanchang Gear Works	Davall Gear Co. Ltd.
Winzeler Gear	Federal Gear Corp.	PIC Design	American Mach. & Gear	Nissei Corp. of America	Dayton Gear & Tool
	Fleet Tools Ltd.	Patterson Gear & Machine	American Metric Corp.	Nixon Gear	Delroy Worm Gear
	Foot-Jones/Illinois Gear	Penn Machine Company	American Precision Gear	Nord Gear Corporation	EMCO Gears
	Forest City Gear Co.	Pennsylvania Gear Corp.	Arrow Gear Co.	Ohio Gear	Electra-Gear
	Franke Gear Works Inc.	Pennsylvania Pressed	Asco Sintering Co.	Oliver Gear	Engelhardt Gear Co.
	GW Plastics	Metal Inc.	Ashot Ashkelon Indust.	PIC Design	Engranes Industriales
	Gear Company of America	Penntech	Ashot USA Inc.	Penn Machine Company	Rivera
	Gear Products Inc.	Perry Technology	Astron Midwestern Inc.	Perry Technology	Euclid Universal Corp.
	Gear Systems Inc.	Philadelphia Gear	Bengal Industries Inc.	Philadelphia Gear	Falk Corp.
	The Gear Works-Seattle	Corp.-Houston	Bevel Gears (India)	Corp.-King of Prussia	Federal Gear Corp.
	Gears & Drive Systems	Corp.-King of Prussia	Bilgram Gear Co.	Preicipart Corp.	Fleet Tools Ltd.
	Geartronics Industries	Philadelphie Gear	Bonfiglioli Riduttori	Precision Gear Co.	Flender Corporation
	General Gear Corporation	Corp.-King of Prussia	Bonfiglioli U.K.	Presrite Corp.	Foot-Jones/Illinois Gear
	Generated Gear &	Poly Hi Solidur	Boston Gear	Process Industries	Forest City Gear Co.
	Machine	Power Eng. & Mfg.	Boxx Gear Mfg.	Progressive Engineering	Gear Company of America
Global Gear	Global Gear	Precipart Corp.	Burgess-Norton Mfg. Co.	The Purdy Corporation	Gear Products Inc.
American Gear & Eng.	Globe Gear Co.	Precision Gear Co.	C-B Gear & Machine, Inc.	Rawling Gear	Gear Systems Inc.
American Mach. & Gear	Great Lakes Industry, Inc.	Precision Gear Inc.	CMD (UK) Ltd.	Reliance Gear Co. Ltd.	The Gear Works-Seattle
American Metric Corp.	Greenspon Engineering	Precision Gears Inc.	Calicut Eng. Works Ltd.	Reliance Gear Corp.	Gears & Drive Systems
American Precision Gear	Works Ltd.	Presrite Corp.	Carbon City Products	Caterpillar Industrial	Geartronics Industries
Aplus Engineering Inc.	HMC	Process Industries	Products Inc.	Products Inc.	General Gear Corporation
Arrow Gear Co.	Hamilton Gear	Production Gear & Broach	Channel Power	Reliance Gear Power	Generated Gear &
Asco Sintering Co.	Hand Screw Machine	Progressive Engineering	Transmission, Inc.	Transmission Inc.	Machine
Ashot Ashkelon Indust.	Hanover Gear Mfg. Co.	Pulley Manufacturers Inc.	Chardam Gear Co.	Chardam Gear Co.	Globe Gear Co.
Ashot USA Inc.	Harder Precision	The Purdy Corporation	Charles Bond Co.	Charles Bond Co.	Great Gear Corp.
Axonix Technologies	Components	Putnam Precision	Chicago Gear-D. O. James	Chicago Gear-D. O. James	Greenspon Engineering
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Bengal Industries Inc.	Horsburgh & Scott	Qualicast Corp.	Ciateq, A. C.	Ciateq, A. C.	
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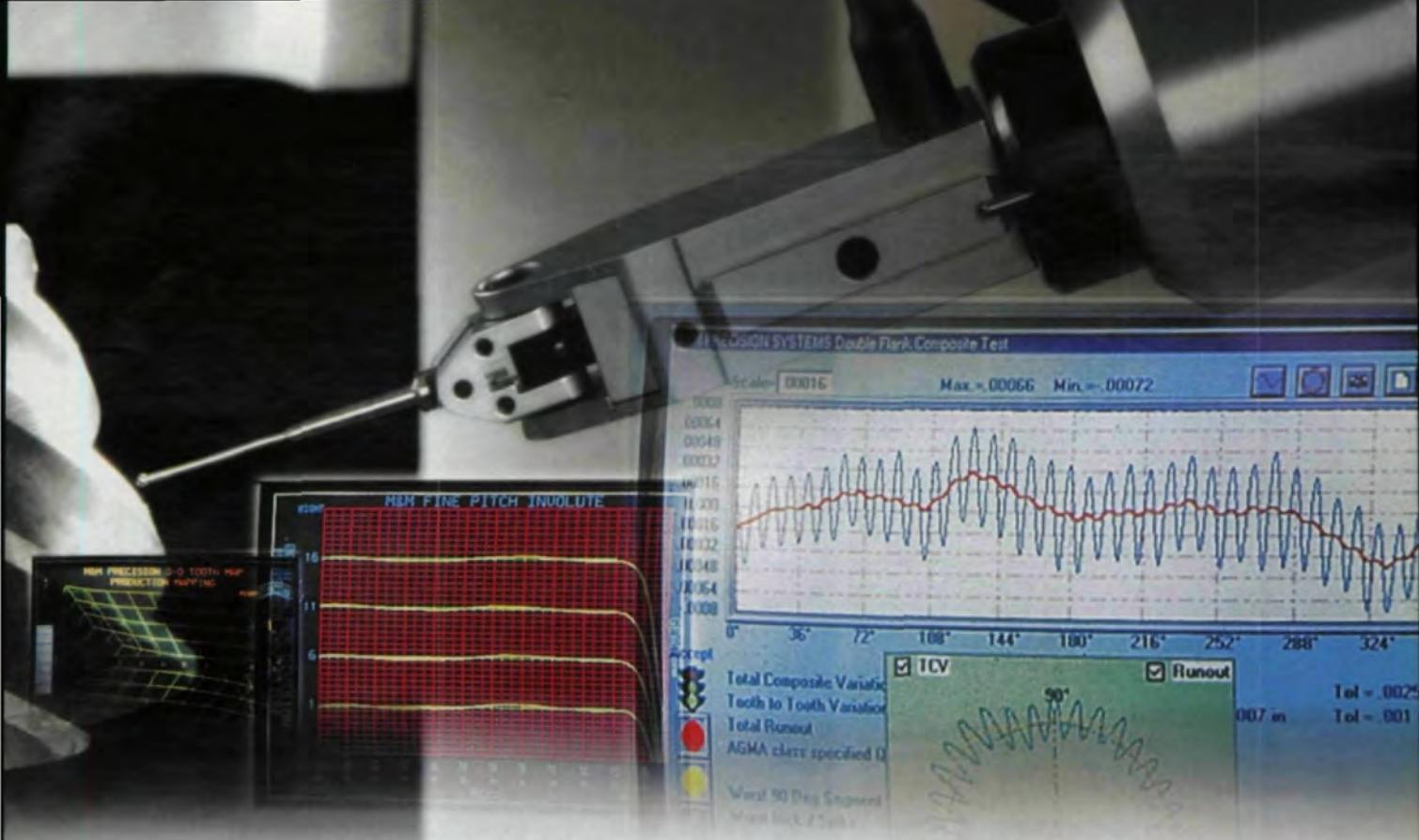
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Company-Charlotte,
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Streetsboro,
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Best Engineering Co., Inc.
Bourn & Koch
C-Dot Engineering
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Drive Systems Technology
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Richter Precision Inc.				
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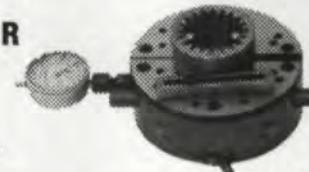
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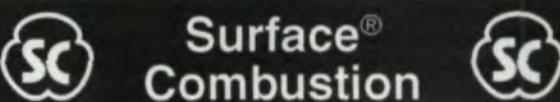
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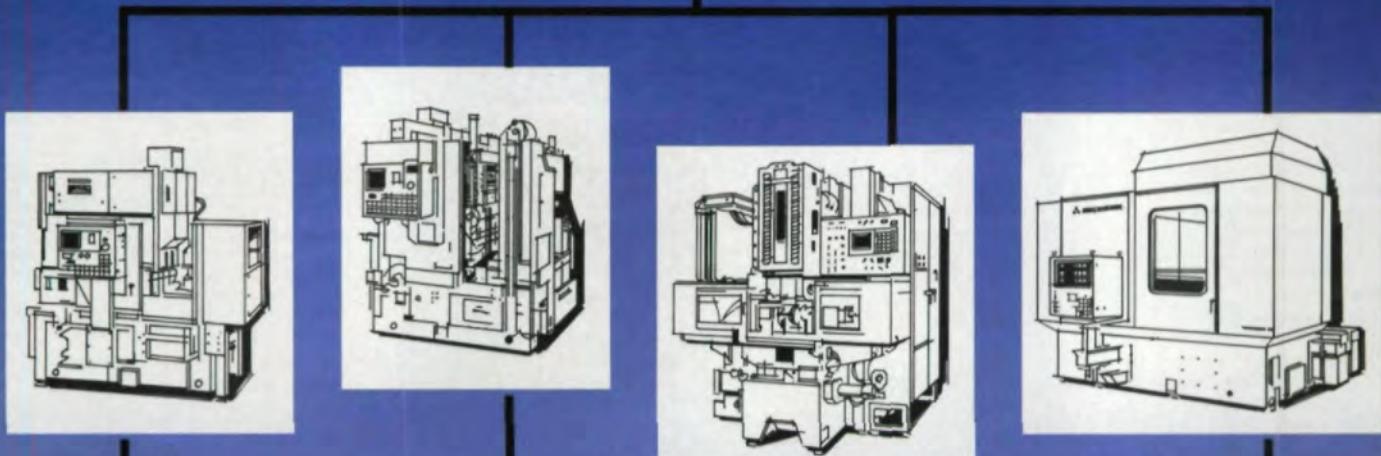
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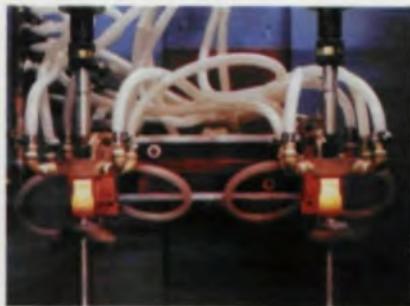
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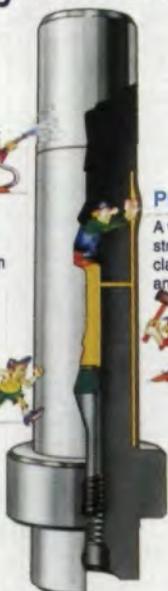
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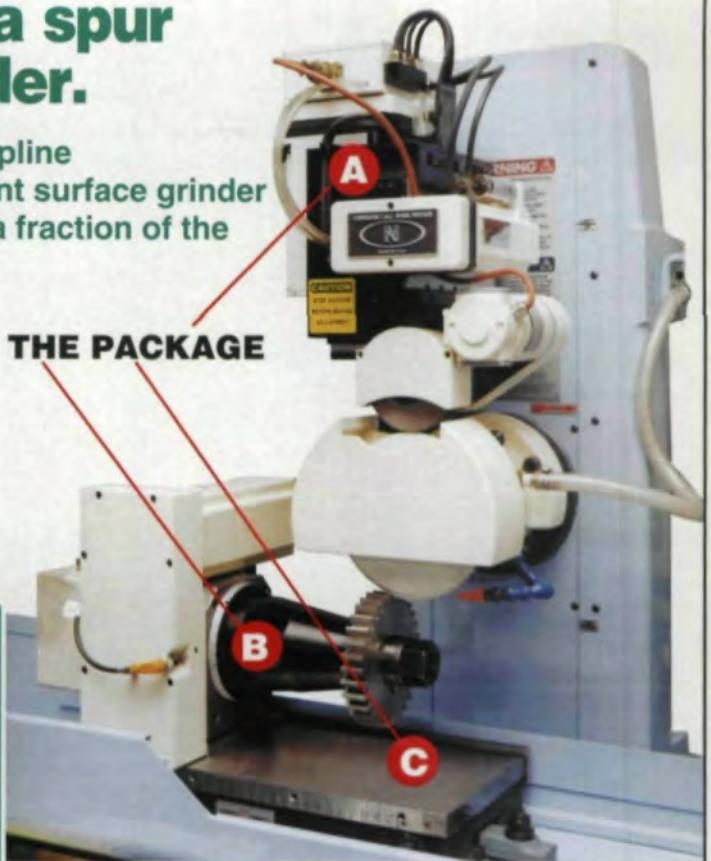
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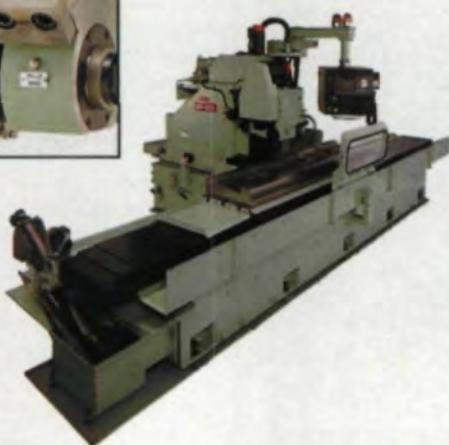
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Guide for Gear Giving

Gear Technology's bimonthly aberration — gear trivia, humor, weirdness and oddments for the edification and amusement of our readers. Contributions are welcome.

The Addendum team hates to admit it, but we're coming up hard on the holiday season again, and that means straining the old brain cells to come up with a good gift list. Once you've taken Aunt Maude's fruit cake brick out of the freezer to recycle it to the least-favorite person on your list, things start to get tricky. Then there's the concern that you're going to end up getting yet another ugly sweater, body-of-steel home exercise gadget (special TV offer; three payments of \$29.95; no CODs, please) or commemorative Elvis plate.

But never fear. As a public service, the Addendum Shopping Team has been scouring the landscape for the season's "must-have" items for gear giving and receiving. Put these items on your list, or circle your favorites and leave the column where your own personal Santa will find it.

For the serious-minded among you (and who's not serious about gears, besides the Addendum Team, that is?), there's the *Maag Gear Book*. This staple of the gear engineering library is in print and available from Global Engineering Documents for \$95.00. (Call 800-854-7179.) If that's not serious enough for you, remember that major technical

societies like AGMA, SME and ASM have big catalogs of all sorts of engineering books, CD-ROMs and software. ASM is offering four volumes of its massive metals *Handbook*® on CD for \$443.00. The entire twenty volumes will be available by December of next year.

For a bit less strenuous reading, our book review editor recommends a little gem called *Longitude* by Dava Sobel (Walker & Company, New York). This is the true story of John Harrison, the self-taught carpenter, clock-maker, mechanic and engineer who solved the problem of calculating longitude, one that had stumped such luminaries as Galileo, Edmund Halley, Christiaan Huygens and Robert Hooke. The crux of the problem is that to calculate longitude, you need to be able to tell time precisely in two places at once, no mean feat in a time before electronic communications and satellites. The story is not just one of engineering ingenuity, but politics, professional jealousy, idealism, class struggle and lots of money.

If your tastes run to the more unusual (like the Addendum staff's), you will want to check out the catalog from American Science & Surplus (847-982-0870 or www.sciplus.com). Here you can order everything from a tabletop-sized dry pellet steam plant to a "talking duck faucet," which apparently is just what it sounds like, an animal-shaped plastic spout to be attached to your regular faucet to make "more or less appropriate" animal sounds when the water flows through. Other must-have items include neon-colored sand paper, make-your-own slime & ooze kits, small motors and gearboxes, French Foreign Legion uniform buttons, army-green "pocket spittoons" and your very own Archimedes pump (for pumping up dead Greek scientists?). Many items are sold in quantity and are remarkably



inexpensive. Lots of good educational kits and toys for your budding engineers, plus odd, but useful, office and lab supplies. This place could solve your stocking stuffer problems.

What would the holidays be without toys? And what's the point of buying stuff for the kids you wouldn't want to play with? For example, Hasbro is relaunching a few of the original Tonka trucks in its Classic Edition series. The 1949 Dump Truck and the 1956 Pickup are back in real metal with real heft, just right for dropping on Grandma's foot, floor-and-furniture scratching and other fun stuff. Then there's the Mercury Astronaut doll, 12" high, complete with spacesuit, helmet, gloves and dog tags. The astronaut's compatriots include a Tuskegee Fighter Pilot, General Patton and, for your own G.I. Jane, the U.S. Army Helicopter Pilot, who just happens to be a girl.

Finally, our staff doesn't want to make your shopping any harder than it has to be. Just send us money. One size fits all, and the color's always right. ☺

The Addendometer: If you've read this far on the page and enjoyed it, please circle 225.



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